

Non-noble metal catalysts for oxygen reduction reaction in low temperature fuel cells

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POLITECNICO DI TORINO  
SCUOLA DI DOTTORATO

Dottorato di Ricerca in Ingegneria Chimica – XXVIII Ciclo



PhD Thesis

**Non-Noble Metal Catalysts  
for Oxygen Reduction Reaction  
in Low Temperature Fuel Cells**

Dissertation

Presented in partial fulfillment of the requirements for the Degree of Doctor of Philosophy in  
Chemical Engineering

**Supervisor**

Prof. Stefania Specchia

**Candidate**

Luigi Osmieri

Torino, March 2016



*Ai miei genitori*





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## ABSTRACT

Polymer electrolyte membrane fuel cells (PEMFC) are electrochemical devices which can directly convert the chemical energy of a fuel (such as hydrogen or a low-molecular weight alcohol) and an oxidant (i.e. oxygen) into electrical energy with high efficiency. Moreover, due their low operating temperature, they are suitable for automotive or portable applications. However, the slow kinetics of oxygen reduction reaction (ORR) requires the use of costly Pt-based catalysts at the cathode in order to obtain the desired power density values. Nevertheless, the cathode is still responsible for the main voltage loss in the cell.

The overall objective of the research carried out in this Ph.D. thesis was the development of Pt-free ORR catalysts starting from different carbon, nitrogen and transition metals precursors. Different synthesis approaches were used in order to obtain an improvement of the activity, and to understand the influence of the synthesis process variables. In particular, the influence of carbon supports (commercial and synthesized in the lab), nitrogen and transition metals precursors, templating agents, number and temperature of pyrolysis were examined. The catalysts produced were characterized by means of several instrumental techniques such as N<sub>2</sub> physisorption, XRD, XPS, EDX, SEM, FESEM, TEM, Raman and FTIR. The effect of the presence of different transition metals on the pyrolysis process was investigated by TGA coupled with a mass spectroscopy analysis, in order to have an insight on their influence in the formation of ORR active sites. The activity toward ORR was assessed by RDE-RRDE (rotating disk electrode - rotating ring disk electrode) analysis and by gas-diffusion electrode in a 3-electrodes electrochemical cell configuration. The electrochemical techniques used were cyclic voltammetry (CV), linear sweep voltammetry (LSV), staircase voltammetry (SV), chronoamperometry and electrochemical impedance spectroscopy (EIS). These electrochemical tests were performed in both acid and alkaline conditions, with reference to the potential applications in both H<sup>+</sup> and OH<sup>-</sup> conducting polymer electrolyte membrane fuel cells. This first part of research was carried out in the laboratories of the Gre.En<sup>2</sup> (Green Energy and Engineering) Group in the Department of Applied Science and Technology (DISAT) at Politecnico di Torino.

Then, in the second part, some of the most promising electrocatalysts in terms of ORR activity were in different types of single PEMFC. In particular, using acidic electrolyte membrane, the tests were performed using H<sub>2</sub> or methanol as fuels. In the case of direct methanol fuel cell (DMFC) tests, short-term durability tests were done in order to compare the durability performance of our catalysts with

a standard Pt-based catalysts. The tests with alkaline electrolyte membrane were performed using ethanol as fuel. This second part of research was carried out at the Universidad Autonoma de Madrid in the laboratories of the Department of Applied Physical-Chemistry.

Here the structure of the thesis:

Chapter 1 is a general introduction about the PEMFC fuel cell technology, particularly focusing on the non-noble metal catalysts for ORR as potential alternative to Pt.

Chapter 2 is focused on the use of different types of reduced graphene oxide as support for the synthesis of Fe-N/C catalysts.

In Chapter 3, a complex between Co ions and a N-containing ligand molecule is impregnated on multi walled carbon nanotubes and pyrolyzed one or two times for producing a Co-N-C catalyst, and the influence of the second pyrolysis on the activity improvement was investigated.

Chapter 4 deals the optimization of the synthesis process of a Fe-N-C catalyst using polypyrrole as N source and mesoporous carbon as C-support.

In Chapter 5 the study of the influence of different silica templates on the morphology on the ORR activity of a Fe-N-C catalyst synthesized using Fe-phthalocyanine as precursor is presented.

In Chapter 6, different Me-phthalocyanines (Me = Fe, Co, Cu, Zn) were used as precursor for the synthesis of Me-N-C catalysts using SBA-15 silica as hard template. The influence of the different transition metals on the pyrolysis process and on the ORR activity and selectivity toward a complete 4 e<sup>-</sup> oxygen reduction was investigated in both acid and alkaline conditions. A detailed kinetic analysis in acid conditions is also presented. The most active catalyst was tested in different types of PEMFCs.

Finally, in Chapter 7, the influence of four different carbon supports on the ORR activity of Fe-N/C catalysts in acid and alkaline conditions as well as the performance in single PEMFC is examined.

The general conclusions of the thesis are presented in Chapter 8.

## CHAPTER 1. Introduction.

### 1.1. Renewable Energy, Hydrogen & Fuel Cells: towards a sustainable development.

One of the targets of the United Nations 2030 Agenda for a Sustainable Development (Goal 7) is to “Ensure access to affordable, reliable, sustainable and modern energy for all”. In particular, this target is subdivided into the following points:

- By 2030, ensure universal access to affordable, reliable and modern energy services.
- By 2030, increase substantially the share of renewable energy in the global energy mix.
- By 2030, double the global rate of improvement in energy efficiency.
- By 2030, enhance international cooperation to facilitate access to clean energy research and technology, including renewable energy, energy efficiency and advanced and cleaner fossil-fuel technology, and promote investment in energy infrastructure and clean energy technology.
- By 2030, expand infrastructure and upgrade technology for supplying modern and sustainable energy services for all in developing countries, in particular least developed countries, small island developing States, and land-locked developing countries, in accordance with their respective programs of support. [1]

In this context, to reduce the dependence on non-renewable energy sources like oil, gas and coal, and favor the transition to an emissions-free way to produce energy, the implementation of a “Hydrogen Economy” worldwide is essential [2]. Hydrogen is a sustainable, non-polluting source of power that can be used in mobile and stationary applications, usable as an ideal energy carrier.

It is an alternative to hydrocarbon fuels such as gasoline. It has many potential uses, and it is environmentally friendly. Today many available technologies can use hydrogen to power cars, trucks, electrical plants, and buildings. However, the absence of an infrastructure for producing, transporting, and storing large quantities of hydrogen have prevent until now its practical use.

Hydrogen cannot be found by itself in nature in the form of  $H_2$ , because the chemical element H always combines with other elements such as oxygen and carbon. Therefore,  $H_2$  needs to be produced, and this requires energy. If this energy comes from renewable sources, the “Hydrogen Economy” is completely clean and sustainable. Nowadays, however, the most common  $H_2$  production method is the steam reforming of methane (from natural gas). Steam reforming is a chemical process that converts hydrocarbons into hydrogen and carbon monoxide by reaction with water steam [3].

Another method of producing hydrogen is the water electrolysis: it consists in splitting water ( $H_2O$ ) into its component parts of hydrogen ( $H_2$ ) and oxygen ( $O_2$ ) using electrical current. If this electricity



is produced by renewable energy sources, this process would be completely emission-free and sustainable, and hydrogen production and use can be part of a clean natural cycle [4].

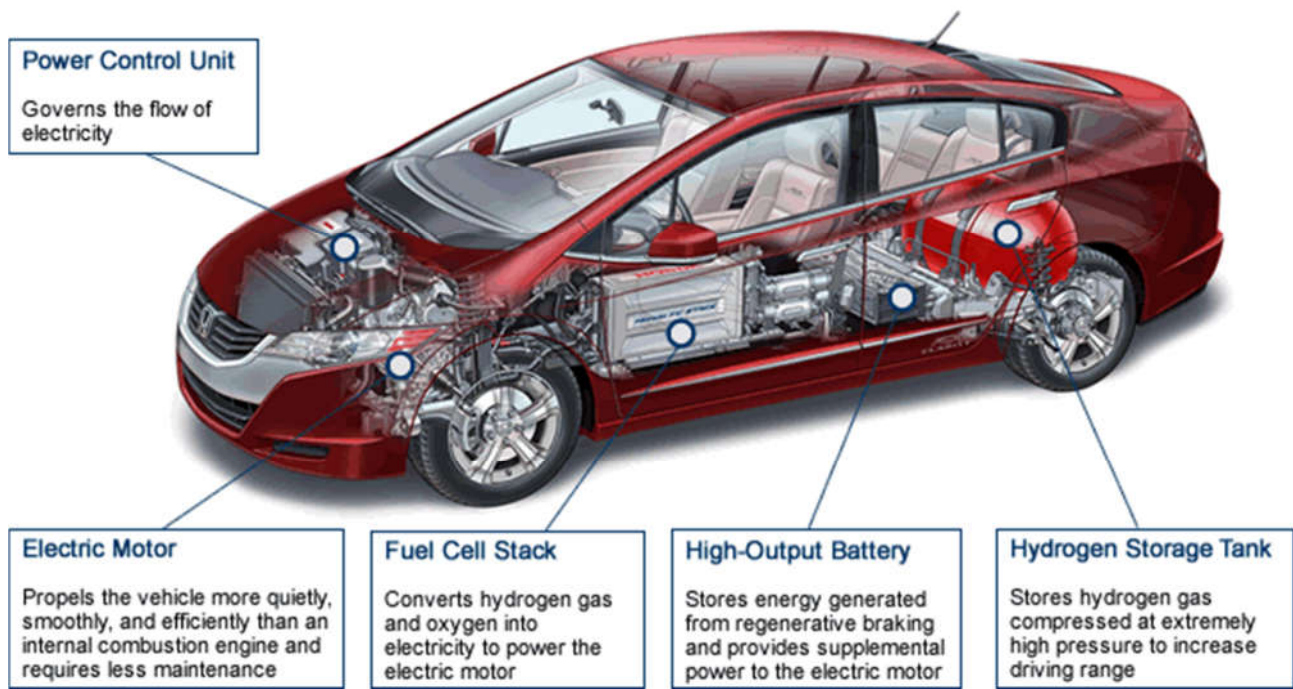
After production, if not immediately consumed, hydrogen needs to be stored in some way. The available hydrogen storage technologies are listed below [5].

- Gaseous storage in C-fibre composite vessels at pressure 350-700 bar. This technology is commercially available but costly. The main R&D issues to be overcome are mechanical resistance to fracture, safety, compression energy, and reduction of volume.
- Liquid storage in cryogenic insulated dewars (at 1 bar and  $-253\text{ }^{\circ}\text{C}$ ). This technology is also commercially available, but costly. The main R&D issues to be overcome in this case are high liquefaction energy, dormant boil off, and safety.
- Solid storage. There are many potential options for hydrogen storage in a solid form. One possibility is the physisorption of molecular  $\text{H}_2$  on extremely high surface area carbon based materials (like carbon nanotubes or graphite nanofibers) or on other high surface area materials like MOF (metal-organic-frameworks) or zeolites. However, the most-developed technology is the storage in metal hydrides ( $\text{H}_2\text{O}$ -reactive chemical hydrides, thermal chemical hydrides and rechargeable hydrides). The problem of these solid storage technologies is that they are still in a very early development status and many R&D questions have to be addressed, some of them are: weight, low desorption temperatures, high desorption kinetics, high recharge time and pressure, heat management, cost, pyrophoricity, cyclic life and container compatibility.

Due to all these factors, cost is the biggest impediment to the wide use of hydrogen as a fuel. In fact, since electricity is required for hydrogen production by electrolysis, this makes hydrogen more expensive than the fuels it would replace. Moreover, many expensive changes should be made in the present energy infrastructure to accommodate hydrogen.

Another concern is flammability:  $\text{H}_2$  can ignite in low concentrations, meaning that any leak in transport and storage equipment could present a safety hazard. These facts highlight some of the many practical considerations to be addressed before wide-scale use of hydrogen becomes a reality. Researchers are developing new technologies in order to make the use of hydrogen cheaper and safer in the future.

A fundamental advance toward a hydrogen-based energy system that uses hydrogen as a fuel are the fuel-cell powered vehicles. This technology is already available and some car manufacturers have already put on the market a fuel-cell car model. However, only a few models are now available for sale or lease, and availability is limited to areas with hydrogen fueling stations, mostly in the USA (California and East Coast), Japan and Northern Europe. Nevertheless, several challenges must be overcome before fuel cell vehicles (FCVs) will be a successful, competitive alternative for consumers.



**Figure 1.** General scheme of the main components of a fuel-cell vehicle [6].

However, the clear advantages of reducing the dependence on fossil fuels, reducing the greenhouse gases emissions (mostly carbon dioxide,  $\text{CO}_2$ ) that contribute to global climate change, and other harmful air pollutants (like  $\text{NO}_x$ ,  $\text{SO}_x$ , unburned hydrocarbons, CO and particulate) in comparison with conventional gasoline- and diesel-powered vehicles cannot be neglected [7].

Another example of fuel cell powered device that is already available on the market are small scale power generator units that are suitable for off-grid stationary and portable applications. They could be based on Direct Methanol Fuel Cell (DMFC) systems, converting methanol directly into electrical energy. Other systems are based on Reformed Methanol Fuel Cell (RMFC), which first convert methanol into hydrogen via reforming, and then use the hydrogen as fuel in the fuel cell system.



**Figure 2.** An example of Reformed Methanol Fuel Cell power generator [8].



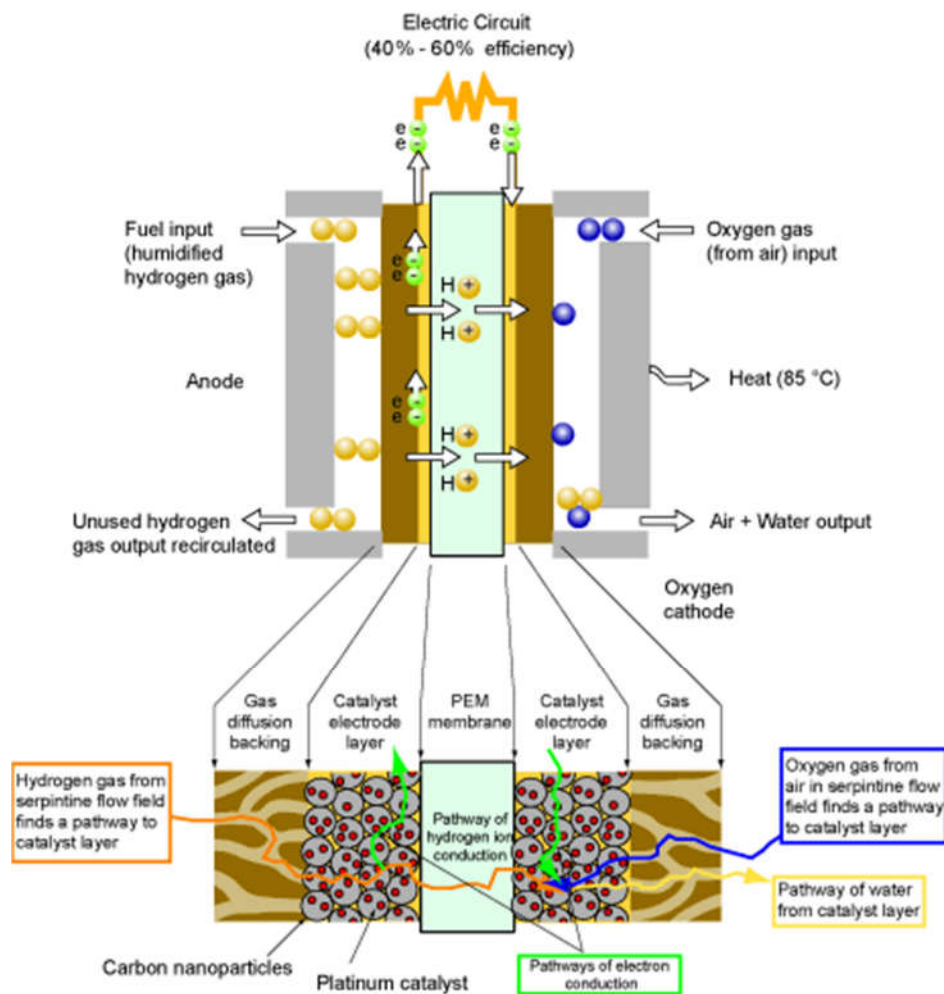
**Figure 3.** An example of Direct Methanol Fuel Cell portable power generator [9].

They are used to supply power in remote zones, where it is not possible to be connected to any electricity or hydrogen distribution grid. The use of a liquid fuel (methanol) increases the energy density, and facilitates the transport and the storage safety.

## 1.2. Fuel Cell systems.

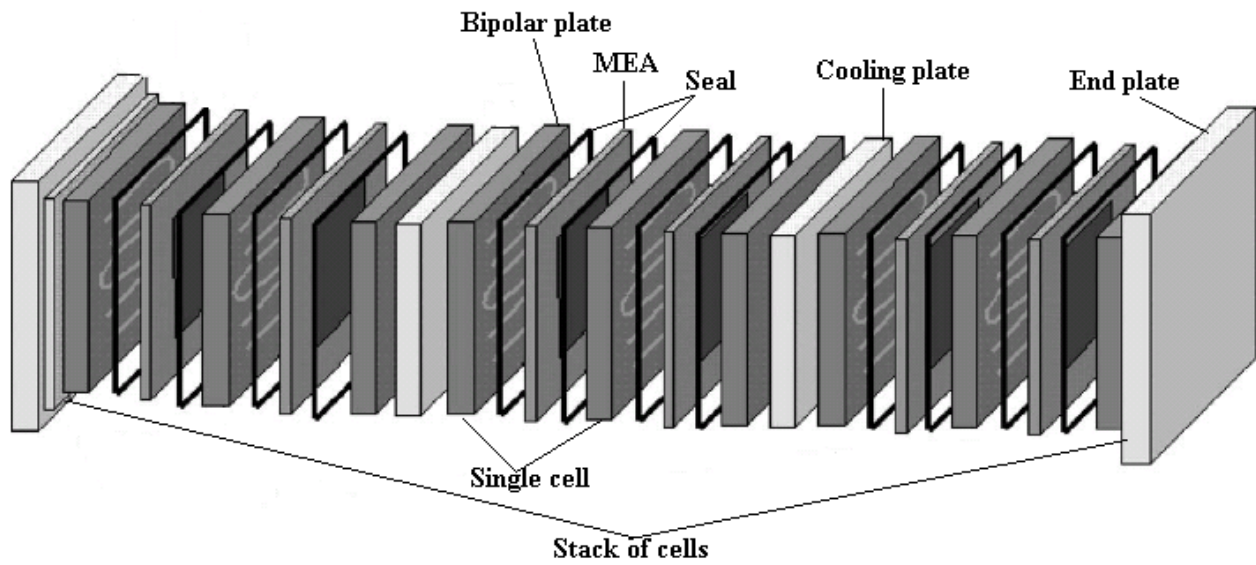
### 1.2.1. What is a fuel cell?

A fuel cell is a device that directly converts the chemical energy of a fuel (generally hydrogen or methanol) and an oxidant (oxygen from the air) into electrical energy. This happens by means of an electrochemical reaction that takes place at the electrodes (anode and cathode) of the fuel cell. The electrochemical reaction is the reverse of what occurs when electricity is used to produce hydrogen and oxygen by electrolysis [10]. The basic structure of a fuel cell consists of an electrolyte layer in contact with a porous anode and cathode on either side. A schematic representation of a single fuel cell with the reactant/product gases and the ion conduction flow directions through the cell is shown in Figure 3. There, the electrolyte is a polymeric membrane which conducts  $H^+$  ions, and the whole membrane and electrodes is called MEA (Membrane Electrode Assembly).



**Figure 3.** Scheme of an individual proton exchange membrane fuel cell (PEMFC) and detail of the MEA structure [11].

The electrochemical reaction occurs at a specific voltage, and the current density is a function of the real or active surface area of the electrode. Thus, electrical series/parallel configurations are necessary in order to get the desired amount of power. Series combinations are achieved by placing multiple single cells together to reach the desired voltage. This is named the fuel cell “stack”. Parallel combinations are achieved by placing multiple stacks together to achieve the desired current [12].



**Figure 4.** Scheme representing how the single MEAs are assembled together in a fuel cell “stack” [13].

The internal combustion engines in today’s cars convert less than 20% of the fuel energy into power that moves the car. Otherwise, fuel cells are highly efficient. They can capture 40 – 60 % or more of a fuel’s energy to power a car, depending on the fuel. However, before fuel cells can be widely used in vehicles, some important problems have to be overcome:

- reduce the size and weight of all the components of a fuel cell power system to improve overall efficiency;
- reduce the cost of producing the fuel cell stacks;
- help fuel cells start faster and respond better to rapid changes in power requirements;
- increase durability and reliability in extreme operating conditions;
- improve the processing systems for hydrogen production and distribution. [10]

### 1.2.2. Fuel cell efficiency.

The ideal performance of a fuel cell depends on the electrochemical reactions that occur with different fuels and oxygen. The efficiency is defined as the work output divided by the heat input. In an

electrochemical energy converter, the heat input is the enthalpy change of the reaction ( $\Delta H$ ), and the work output (if the system operates at the thermodynamic reversible potential of the cell) is the free-energy change of the reaction [14].

For a fuel cell, the energy input is equivalent to the enthalpy of reaction (combustion), and the useful energy output is the electrical energy produced. If all the Gibbs free energy produced is ideally converted to electricity, then the thermodynamic fuel cell efficiency ( $\varepsilon$ ) at 25 °C temperature and 1 atmosphere pressure is the ratio of the change in Gibbs free energy ( $\Delta G^\circ$ ) to the change in enthalpy ( $\Delta H^\circ$ ) of the fuel cell reaction (using the Higher Heating Value of hydrogen) [12]:

$$\varepsilon = \frac{\Delta G^\circ}{\Delta H^\circ} = \frac{237.1 \text{ kJ mol}^{-1}}{286.0 \text{ kJ mol}^{-1}} = 83\% \quad (1)$$

As the enthalpies and Gibbs free energies of reaction are temperature dependent, the thermodynamic efficiencies of a fuel cell is as a function of temperature at a given pressure.

The Gibbs free energy is related to the cell voltage ( $E_{\text{cell}}$ ) by the following relation:

$$\Delta G = -nFE_{\text{cell}} \quad (2)$$

And the ideal voltage of a cell is defined by the Nernst equation [1]:

$$E_{\text{cell}} = E_{\text{cell}}^0 + \frac{RT}{nF} \ln \left( \frac{C_O}{C_R} \right) \quad (3)$$

where:  $R$  is the gas constant,  $T$  is absolute temperature,  $n$  is the number of electrons transferred,  $C_O$  and  $C_R$  are the concentrations of the chemical species in the oxidized and reduced form, respectively. The Nernst equation provides a relationship between the ideal standard potential ( $E_{\text{cell}}^0$ ) for the cell reaction and the ideal equilibrium potential ( $E_{\text{cell}}$ ) at other temperatures and concentrations (or partial pressures in case of gases) of reactants and products. Once the ideal potential at standard conditions is known, the ideal voltage can be determined at other temperatures and pressures through the use of these equations.

Useful work in the form of electrical energy is obtained from a fuel cell only when a reasonable current is drawn. In these conditions, the actual cell potential is decreased from its equilibrium potential due to irreversible losses. Different factors contribute to irreversible losses in a fuel cell. These losses, usually called polarization or overpotential ( $\eta$ ), are due to different reasons.

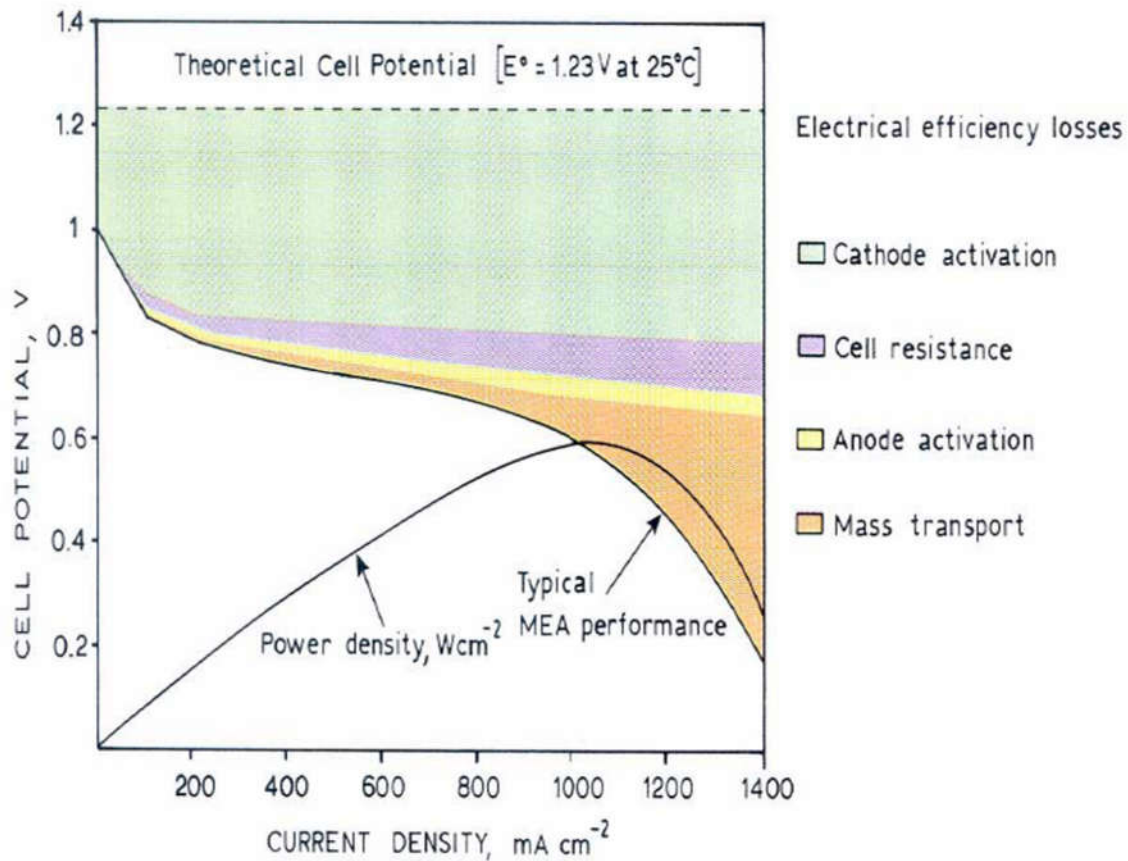
- Activation overpotential ( $\eta_{act}$ ): it is dominant at low current density, when the rate of an electrochemical reaction at an electrode surface is controlled by sluggish electrode kinetics. Therefore, the activation polarization is directly related to the rates of electrochemical reactions.
- Ohmic overpotential ( $\eta_{ohm}$ ): it is due to resistance to the flow of ions in the electrolyte and resistance to flow of electrons through the electrode materials. Both the electrolyte and fuel cell electrodes obey Ohm's law, therefore the ohmic losses can be expressed by the equation  $\eta_{ohm} = iR$  where  $i$  is the current flowing through the cell, and  $R$  is the total cell resistance (which includes electronic, ionic, and contact resistance).
- Concentration overpotential ( $\eta_{conc}$ ): it is important at high currents, where it becomes difficult to provide enough reactant flow to the reactive sites. In facts, as a reactant is consumed at the electrode at a high rate, there is a loss of potential due to the inability to maintain the initial concentration of the bulk fluid (a concentration gradient is formed). The slow transport of reactants/products to/from the electrochemical reaction site is the major contributor to concentration polarization.
- Other losses can be caused by fuel crossover from the anode through the electrolyte, resulting in a mixed potential at the cathode, and also by internal currents. Fuel crossover and internal currents have an effect on the voltage at open circuit ( $V_{ocv}$ ), which results to be lower than the ideal cell potential ( $E_{cell}$ ) [12,14].

The actual fuel cell voltage ( $V_{cell}$ ) is given by:

$$V_{cell} = V_{ocv} - \eta \quad (4)$$

Where:  $\eta = \eta_{act} + \eta_{ohm} + \eta_{conc}$



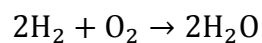


**Figure 5.** Typical PEM fuel cell polarization curve with the different losses [16].

The standard electrochemical technique for characterizing both single fuel cells and stacks is called polarization curve. Here, the cell voltage is plotted as a function of current density (see Fig. 5). However, polarization curves can only show the overall performance of the fuel cell. They cannot distinguish within the different polarization losses [12].

### 1.2.3. Different types of low-temperature fuel cells.

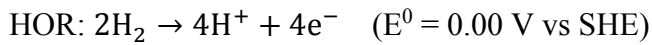
When hydrogen is used as fuel, two different configurations of fuel cell with a polymeric membrane electrolyte are possible. The first one is the PEMFC (Proton Exchange Membrane Fuel Cell), where the membrane is a conductor of H<sup>+</sup> ions. The second type is the AEMFC (Anion Exchange Membrane Fuel Cell) or APEFC (Alkaline Polymer Electrolyte Fuel Cell), where the membrane is a conductor of OH<sup>-</sup> ions. This substantial difference implies that, although the overall reaction between H<sub>2</sub> and O<sub>2</sub> is the same for both types of fuel cells:



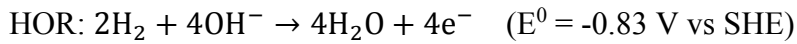


the half-reactions that take place at the two electrodes (hydrogen oxidation at the anode and oxygen reduction at the cathode) are different.

For a PEMFC (acidic conditions) we have:



For an AEMFC (alkaline conditions) we have:

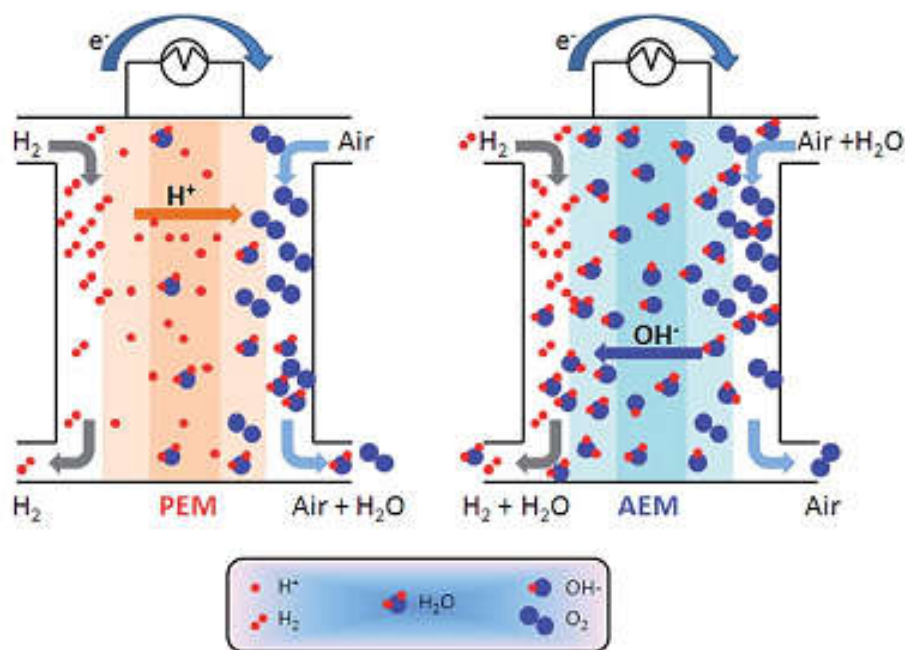


This implies that in the case of a PEMFC, the  $\text{H}^+$  cations are transported through the solid membrane from the anode to the cathode, while in the case of an AEMFC the  $\text{OH}^-$  anions are transported through the membrane in the opposite direction, from the cathode to the anode.

As evident in the half-reactions, and shown in the schemes of Figure 6, water is not a direct reactant in PEMFCs, while it is in APEFCs (it is consumed at the cathode). Moreover, water is generated at cathode side of PEMFCs, otherwise it is generated at the anode in APEFCs.

The advantages of the PEMFC are mainly related to the membrane. The most commonly used membrane material is a sulfonated tetrafluoroethylene based polymer (Nafion®), which has a relatively low cost, and good mechanical and chemical properties.

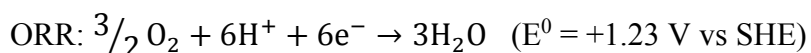
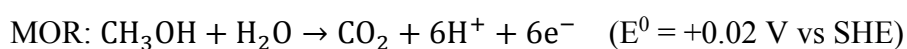
On the contrary, the advantages of the AEMFCs over PEMFCs are related to the alkaline pH cell environment. In these conditions the ORR catalysis is enhanced (allowing for the use of less expensive Pt-free catalysts), and the operative conditions for the cell and stack materials are less severe (allowing to use cheaper materials, and reducing corrosion problems of carbon based materials). The most critical concerns for APEFC technology are the low conductivities and the relatively poor stabilities of the alkaline polymer exchange membranes, and the carbonation problems due to the presence of  $\text{CO}_2$  in the air [17].



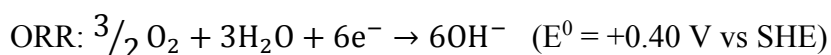
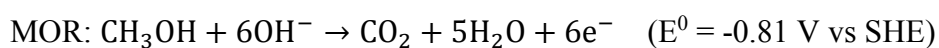
**Figure 6.** Schematic comparison of a proton exchange membrane fuel cell (PEMFC, left) and an alkaline polymer electrolyte fuel cell (APEFC, right) that use H<sub>2</sub> as fuel [17].

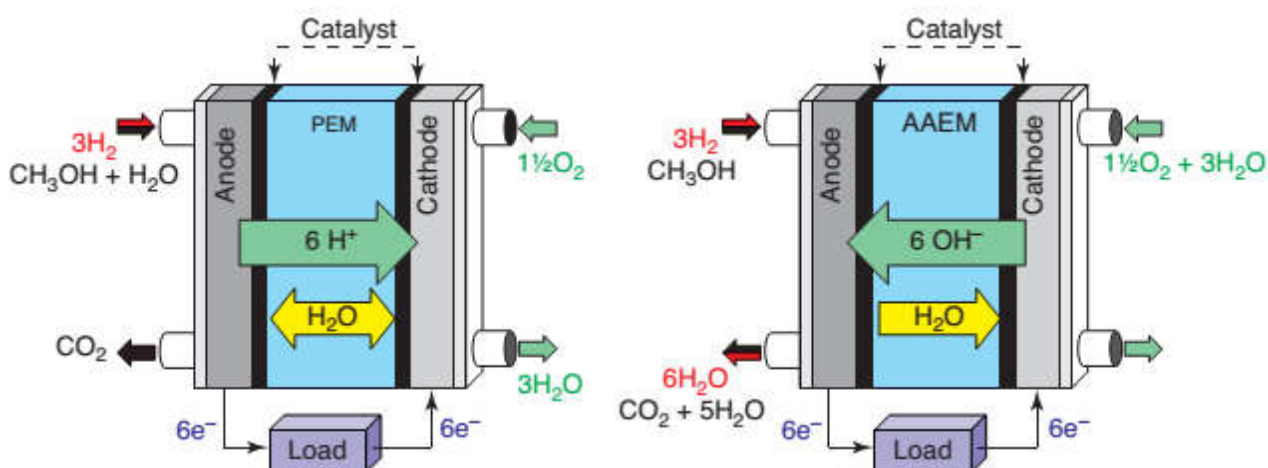
In alternative to H<sub>2</sub>, organic molecules like light alcohols can be directly used as fuels. In this case the fuel cell devices are called Direct Alcohol Fuel Cells. In particular, methanol and ethanol are the most commonly used alcohols due to their availability and low cost. Because of their simple chemical structure, they can be more easily oxidized. Other more complex alcohols like ethylene glycol, propanols and glycerol have also been tested, especially in direct alcohol AEMFC fuel cells [18].

In a direct methanol fuel cell (DMFC) working with a proton-conducting membrane (acidic conditions) the reactions are the followings:



If we operate with an OH<sup>-</sup>-conducting membrane (alkaline conditions) we have:





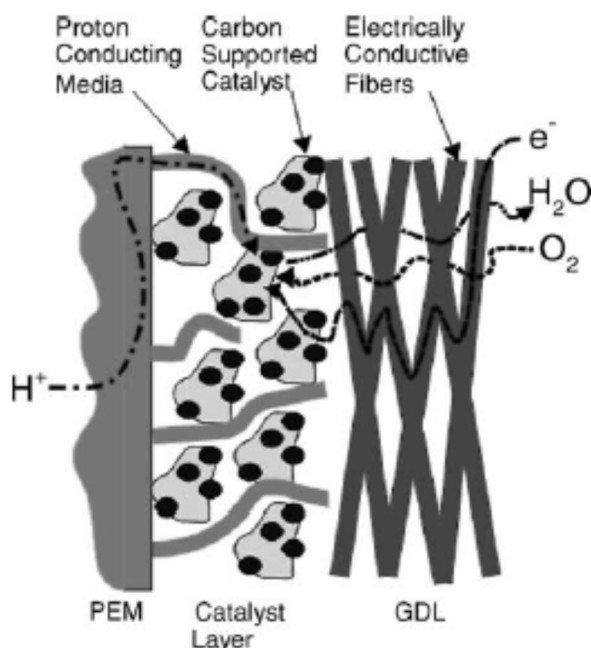
**Figure 7.** Schematic comparison between a hydrogen or methanol-fuelled proton exchange membrane fuel cell (PEMFC) and an alkaline anion exchange membrane fuel cell (AEMFC) [19].

To operate with direct alcohol fuel cells in alkaline conditions has many advantages in comparison with acid ones. In particular, alcohol oxidation is generally more facile at high pH. Therefore, it is potentially possible to use cheaper and more abundant anode catalysts. Also, the ORR is kinetically favored in alkaline conditions allowing to use Pt-free catalysts as stated before. In addition, the  $OH^-$  ions move through the membrane in the direction cathode  $\rightarrow$  anode, that is contrary to alcohol crossover (anode  $\rightarrow$  cathode). This may mitigate the effect of alcohol crossover, especially at higher currents. The crossover problem is particularly serious in acid DMFC when Nafion® material is used as electrolyte [19]. However, the production of  $CO_2$  could cause problems in the alkaline electrolyte due to the formation of carbonates.

#### 1.2.4. The MEA structure – Factors that affect the performance of the fuel cell.

The MEA is the “core” component of PEMFCs and APEFCs. It is the place where the electrochemical reactions occur. The MEA has a “sandwich” structure (as shown in the detail of Figure 3), consisting of a gas diffusion layer (GDL) made of porous carbon paper or carbon cloth, a microporous layer (generally carbon), a catalyst layer mixed with a certain quantity of ionomer (the same type of the membrane), and the polymer electrolyte membrane. The same components are repeated on the other side of the membrane, in reverse order. The MEA structure in the cathode side of a PEM is shown in Figure 8. Here it is also shown the complex mechanism of transport of  $H^+$  ions,  $O_2$  and electrons, which have to simultaneously be present in the catalytic active site, to give rise to the oxygen reduction reaction. After that,  $H_2O$  is generated as product, and has to be removed away from the catalytic site back through the GDL, and finally to the flow channels.

Due to this complexity, all of the MEA components play an important role in the fuel cell system operation. Therefore, to get a good performance, each one of them needs to be optimized.



**Figure 8.** Scheme of the transport of reactants (protons and gaseous  $O_2$ ), electrons and products ( $H_2O$ ) in a PEM fuel cell cathode [20].

Below we will analyze how the different parts of the MEA influence its operation.

**Catalyst:** its function is to catalyze the electrode reaction, so it must possess a good catalytic activity (for ORR at the cathode side and for HOR or MOR at the anode side). Moreover, it must also have a good electronic conductivity, to allow the electrons transport towards or away from the active sites. In addition, the catalyst must be capable to resist at the strong acidic (or alkaline) environment of the PEMFC (or AEMFC) for a reasonably long period, comparable to the life of the fuel cell.

So far, only noble metal-based catalysts, essentially Pt for ORR and HOR, and Pt-Ru alloys for MOR have reached satisfactory results in terms of electroactivity and durability demonstrated on a large scale. Due to Pt high cost, a high surface area per weight of catalyst is highly desirable. Therefore, to maximize platinum utilization and minimize cost, platinum is dispersed in the form of nanoparticles (2-10 nm diameter) on an electrically conducting, and relatively chemically inert support (generally a carbon black). In this way, one of the best state-of-the-art Pt-utilization efficiency of 60 –70 kW/g<sub>Pt</sub> was achieved for catalyst layers with Pt-loadings as low as 0.01 – 0.02 mg/cm<sup>2</sup> [21,22].

To make the electrodes, the two most common techniques are coating the catalyst ink on a gas diffusion layer (GDL), or directly onto the membrane to form a catalyst coated membrane (CCM) [12].

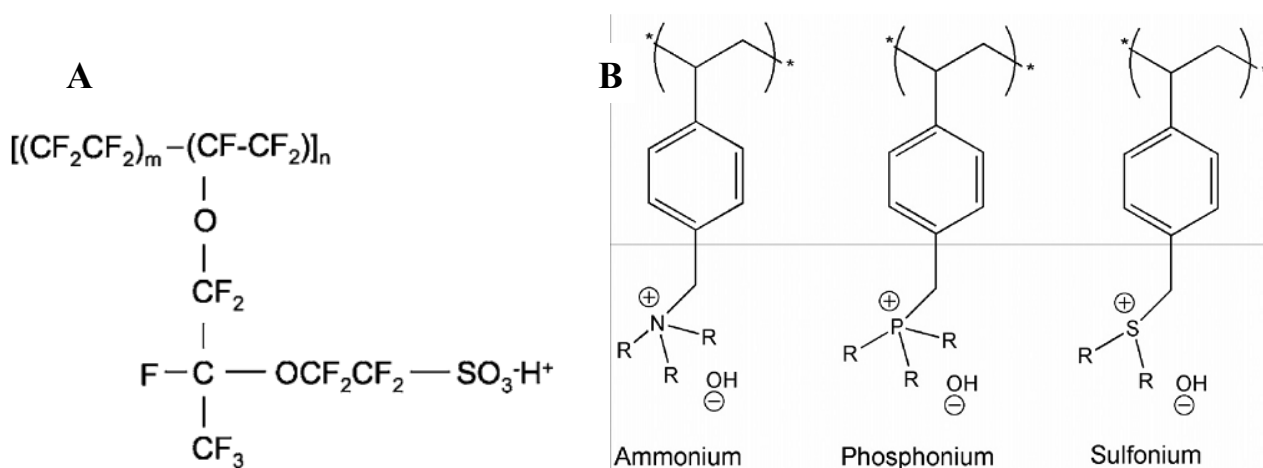
Another aspect of the catalyst that has to be considered is the selectivity. Pt is not a selective catalyst. This is not a problem if H<sub>2</sub> is used as fuel, due to its low permeation rate across the membrane. On the contrary, when the fuel is methanol, non-negligible quantities cross the membrane and are oxidized at the Pt cathode catalyst. This results in a lowered fuel cell performance and fuel utilization [23]. For this reason, the research toward very selective catalyst for ORR is important.

**Carbon electrode material (GDL, catalyst C support):** the GDL has the main function of homogeneously distribute the reactant gases inside the porous electrode, providing at the same time a good electronic conductivity. The GDL also plays an important role in water removal away from the catalyst layer. The GDL usually has a dual layer structure. The first layer (in contact with the catalyst) is a microporous layer made of carbon powder and a hydrophobic agent (generally PTFE). The latter serves to minimize the water flooding. The second layer is a macroporous conductive carbon substrate consisting of the carbon paper or carbon cloth. Therefore, an ideal GDL should have the following characteristics: appropriate hydrophobicity, surface that enhances good electronic contact, high electronic conductivity, and effective mass-transport properties for the reactant gases [12]. Regarding the C support for catalysts based on Pt nanoparticles, first, it must also provide a good electronic conductivity. Second, it must be an effective support for the finely dispersed Pt particles. To do this, it should have a sufficiently high surface area to ensure a high enough inter-distance between the Pt particles, and avoid coalescence during long time operation [24]. However, a too high surface area of the carbon support may result in Pt particles being located in very narrow pores, not being in contact with the electrolyte and therefore not participating in the reaction. In particular, for Pt catalysts supported on different carbons having surface areas in the range of 20 to 1500 m<sup>2</sup>g<sup>-1</sup>, it was found that the best performances were obtained with supports having a surface area in the range of 250-300 m<sup>2</sup>g<sup>-1</sup> [25]. Actually, Vulcan XC-72 (254 m<sup>2</sup>g<sup>-1</sup> surface area) is currently one of the most widely used carbon support materials for low-temperature fuel cell applications.

**Membrane:** the main polymer electrolyte membrane function is to separate the anode and cathode, avoiding the direct mixing of fuel and oxidant, functioning as an electronic current insulator to avoid short-circuit between the electrodes, while providing at the same time high ionic current conductivity. The required properties for the polymer are high ionic conductivity (for H<sup>+</sup> in the case of PEM, for OH<sup>-</sup> in the case of AEM), good mechanical strength, good chemical stability under the fuel cell operation conditions, low permeability to reactants, and low cost. Polymer electrolyte membranes appear macroscopically like a single phase. However, microscopically there are two phases chemically bonded to each other, each containing either hydrophilic or hydrophobic moieties, that when hydrated, result in phase separation, with the hydrophilic moieties forming continuous interconnected water containing channels [12].

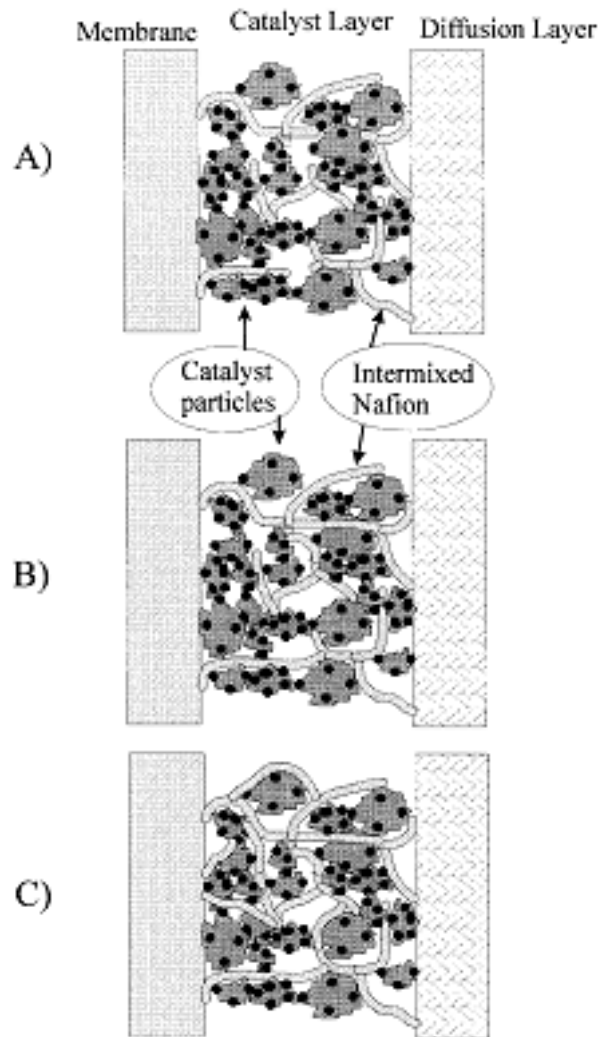
The most commonly used polymer with a relatively low cost, low water drag, low gas permeability, good mechanical properties (flexibility, strength), good chemical and thermal stability, and high protonic conductivity is DuPont's Nafion®. Its structure is similar to that of Teflon (see Figure 9A). The hydrophilic moieties that facilitate proton transport are sulfonic acid groups. The  $-\text{SO}_3^-$  groups are fixed to the polymer chain, while  $\text{H}^+$  can move throughout the membrane jumping from group to group [26].

Regarding the anion exchange membrane the research is less advanced. Therefore, many different chemical structures could be potential candidates for application in AEMFCs, providing better results in terms of chemical and thermal stability will be achieved in the next future [27]. Some of the main chemical species that could be used as alkaline solid polymer electrolyte are shown in Figure 9B.



**Figure 9.** Unit molecular structure of Nafion® proton exchange membrane electrolyte (A) and some examples of chemical structure of anion exchange groups capable to transport  $\text{OH}^-$  ions [26,27].

**Quantity of ionomer in the catalyst layer:** before being deposited on the GDL, the catalyst is dispersed by an appropriate solvent (or mixture of different solvents) to form an ink [23]. In order to ensure all of the catalyst's active sites are in contact with the polymer electrolyte membrane (see Figure 10), a certain amount of ionomer is added to the ink. For the preparation of the electrode ink, the ionomer needs to be dissolved in a solvent. The relative amount of solid phase (catalyst + C-support) and ionomer in the electrode catalytic layer has an important effect on the final fuel cell performance, as evidenced by many studies [20,28,29]. In PEMFCs, the percentage of Nafion relative to the total weight of the electrode has been recognized as a key parameter to obtain higher power densities. In particular, the results obtained by various authors could be compared despite the varying loadings, resulting that the optimal content of Nafion lay in the range of 30–40 wt. %.



**Figure 10.** Schematic planar representation of the catalytic layer. (A) Too low Nafion content: not all the catalyst particles are connected to the membrane by a Nafion bridge. (B) Optimal Nafion content: good connections for ionic and electronic conduction for all the catalyst particles (C) Too high Nafion content: not all the catalyst particles are electronically connected to the diffusion layer [28].

### 1.3. The Pt problem: strategies and research approaches to reduce the dependence on Pt.

The use of Pt as the preferred catalyst for both the anode and the cathode of PEMFCs and DMFCs, has been until now one of the main impediments to the widespread commercialization of these devices. In fact, platinum is a noble metal and as such, its use suffers of obvious problems of high cost (being Pt price at November 2015 around 1000 US \$ per troy ounce) and price volatility on the stock exchange market (see Figure 11). Moreover, the majority of platinum estimated reserves worldwide and mining production are concentrated in South Africa, as shown in Figure 12.

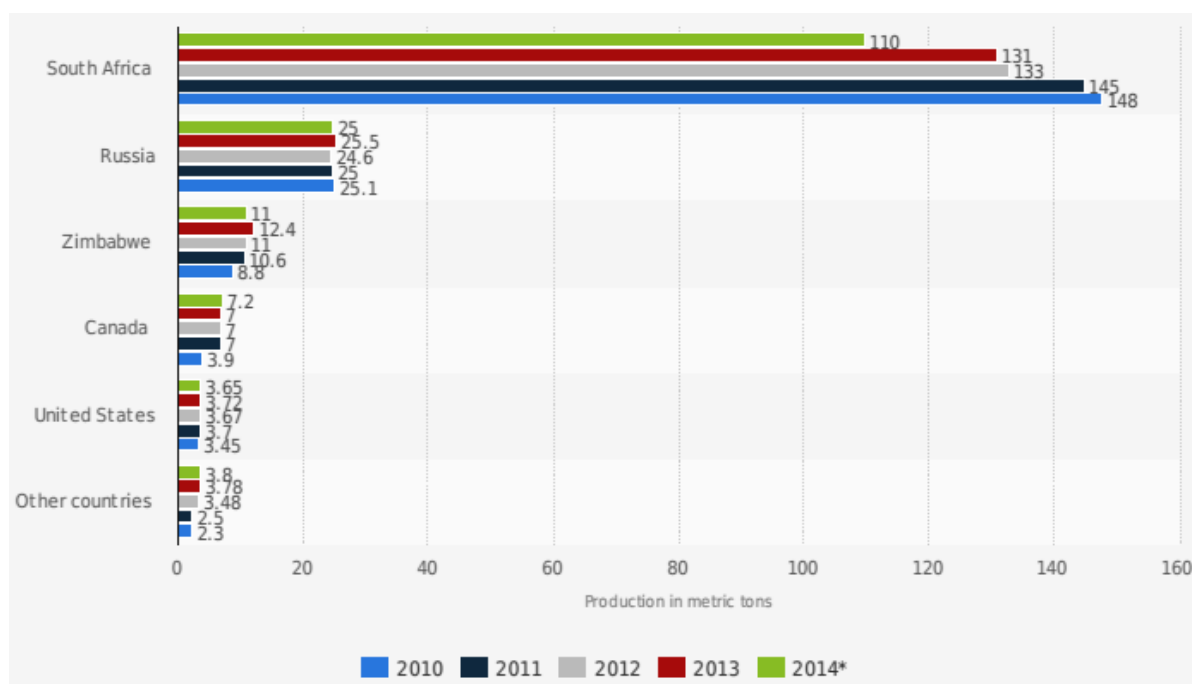
In recent years, significant improvements have been obtained in decreasing of the amount of platinum used in FC stacks (purpose of the United States Department of Energy for PEMFC systems for transportation application: total content of noble metals for both electrodes  $\leq 0.125 \text{ mg cm}^{-2}$  by 2017 [30]). Nevertheless, assuming a complete replacement of the fleet of internal combustion engine vehicles currently produced each year with fuel cell vehicles, and considering the world's estimated platinum reserves, the price of platinum would rise to unsustainable levels, and the reserves would be destined to run out quickly. In addition, in this scenario, it is likely that Pt cost will increase with the increasing demand of Pt, as the FC vehicles widespread commercialization will start.

For example, considering each car provided with a minimum 50 kW stack, this would require a steady Pt demand of 1000 tons a year. In recent years, the global Pt production has only been ca. 200 tons a year. An eventual global fleet of 1 billion PEMFC cars would commit 10,000 tons of Pt. The total world Pt reserves, proven and inferred, are estimated at 40,000 tons, if mining down to 2 km is assumed. Based on these numbers, it is clear that the Pt recycling rate must be very high for such a fleet to be sustainable. Under such market pressure, the Pt cost would likely rise significantly. Therefore, replacing platinum-based catalysts with a more abundant material would greatly improve the outlook for the widespread development of automotive fuel cells [31].



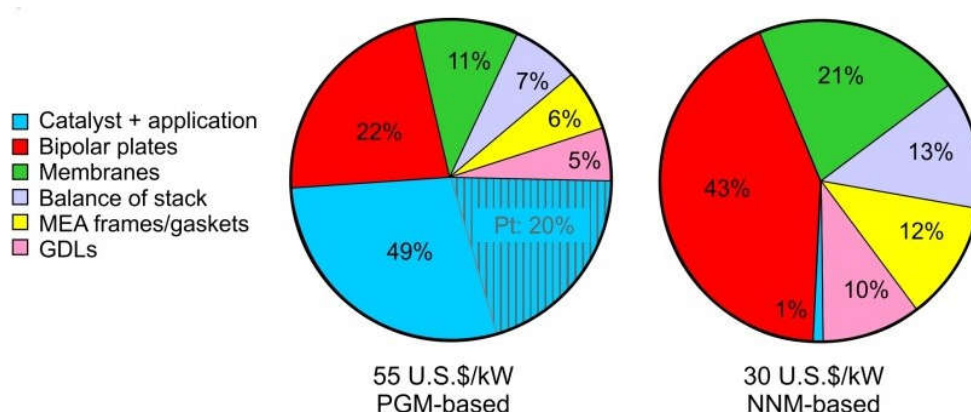
**Figure 11.** Oscillations of the Pt commodity price from January 2000 to October 2015 [32].





**Figure 12.** Major countries in global mine production of platinum from 2010 to 2014 [33].

Currently, Pt-based catalysts contribute to a large portion of cost of a state-of-the-art PEMFC stack [34–36]. A recent technical report from the United States Department of Energy [33] forecasted a cost of 55 U.S.\$/kW for a 80 kW stack containing Pt-based catalyst, produced as 500,000 units per year (see Figure 13). In the cost breakdown of the stack, with Pt price accounted as 1,500 U.S.\$ per troy ounce [37], the cost of the catalyst plus its application accounts for 49% (20% only for purchasing Pt) of the total price of the stack itself (Figure 13).



**Figure 13.** Cost breakdown of a 80 kW Platinum group metal (PGM)-based stack (assumptions done on 2013: Pt loading  $0.153 \text{ mg}_{\text{Pt}} \text{ cm}^{-2}$ ; power density  $692 \text{ mW cm}^{-2}$ ; Pt price assumed as 1,500 U.S.\$ per troy ounce; 500,000 units per year production [37]) and of a 80 kW non-noble metal (NNM)-based stack (assumptions done on 2015). NNM loading  $4 \text{ mg}_{\text{cat}} \text{ cm}^{-2}$ ; power density  $370 \text{ mW cm}^{-2}$ ; catalyst cost 0.35 U.S. \$/kW; 500,000 units per year production [38].

Durability is an additional key factor affecting the PEMFC performance. In fact, platinum dissolution/coalescence phenomena and carbon support corrosion are mainly responsible for PEMFC degradation. Therefore, a breakthrough in the development of cost effective, highly performing and durable catalysts has been identified as the determining factor for success toward PEMFC commercialization [39–41], and the development of alternative cheaper catalysts is of primary importance.

In order to overcome these problems, the USA Department of Energy has identified and carry out two different research directions, as shown in Figure 14.

The first strategy is focused on low Pt loading electrocatalyst development. The second strategy is focused on non-noble metal (NNM) cathodic electrocatalyst. In facts, Pt loadings are usually higher on cathode than on anode of a PEMFC. In the acid environment of PEMFC (around pH 1), the hydrogen oxidation reaction (HOR) on Pt is a faster electrochemical reaction than the oxygen reduction reaction (ORR) on Pt. The latter reaction is notoriously slow. Consequently, about 5–10 times more Pt is needed at the cathode of PEM fuel cells than at the anode [39]. Therefore, a much greater cost reduction can be achieved by replacing Pt with a lower cost non noble metal-based catalyst at the cathode of PEM fuel cells [42].

However, for a long-term strategy toward commercialization, only NNM catalysts would be the definitive solution to the problem of dependence on Pt [41]. A preliminary new cost breakdown analyses estimate the cost of a NNM-based 80 kW PEMFC stack as 30 U.S.\$/kW, with a cost of 0.35 U.S.\$/kW for the NNM catalyst (see Figure 13) [38]. Considering the current average state-of-the-art level of specific power density ranging from 300 to 400 mW cm<sup>-2</sup> reached for NNM-catalysts [38], the improvement of this parameter to levels close to the specific power density of Pt-based catalysts (more than 700 mW cm<sup>-2</sup> [37]) is crucial on the point of view of the stack size and dimensioning.

| Characteristic  | Units   | 2011 Status   | Targets |       |
|---|---|---|---------|-------|
|   |   |   | 2017    | 2020  |
| Platinum group metal total content (both electrodes) <sup>a</sup>         | g / kW (rated)                                  | 0.19 <sup>b</sup>   | 0.125   | 0.125 |
| Platinum group metal (pgm) total loading <sup>a</sup>                     | mg PGM / cm <sup>2</sup> electrode area         | 0.15 <sup>b</sup>   | 0.125   | 0.125 |
| Loss in initial catalytic activity <sup>c</sup>                           | % mass activity loss                            | 48 <sup>b</sup>   | <40     | <40   |
| Electro catalyst support stability <sup>d</sup>                           | % mass activity loss                            | <10 <sup>b</sup>  | <10     | <10   |
| Mass activity <sup>e</sup>  | A / mg Pt @ 900 mV <sub>IR-free</sub>           | 0.24 <sup>b</sup>   | 0.44    | 0.44  |
| Non-Pt catalyst activity per volume of supported catalyst <sup>e, f</sup> | A / cm <sup>3</sup> @ 800 mV <sub>IR-free</sub> | 60 (measured at 0.8 V) <sup>g</sup><br>165 (extrapolated from >0.85 V) <sup>g</sup> | 300     | 300   |

<sup>a</sup> PGM content and loading targets may have to be lower to achieve system cost targets.

<sup>b</sup> M. Debe, U.S. Department of Energy Hydrogen and Fuel Cells Program 2011 Annual Merit Review Proceedings, May, 2011, ([http://www.hydrogen.energy.gov/pdfs/review11/fc001\\_debe\\_2011\\_o.pdf](http://www.hydrogen.energy.gov/pdfs/review11/fc001_debe_2011_o.pdf))

<sup>c</sup> Durability measured in a 25-50 cm<sup>2</sup> MEA during triangle sweep cycles at 50 mV/s between 0.6 V and 1.0 V at 80°C, atmospheric pressure, 100% relative humidity, H<sub>2</sub> at 200 sccm and N<sub>2</sub> at 75 sccm for a 50 cm<sup>2</sup> cell. Based on U.S. DRIVE Fuel Cell Tech Team Cell Component Accelerated Stress Test and Polarization Curve Protocols ([http://www.uscar.org/commands/files\\_download.php?files\\_id=267](http://www.uscar.org/commands/files_download.php?files_id=267)), Electrocatalyst Cycle and Metrics (Table 1). Activity loss is based on loss of mass activity, using initial catalyst mass, at end of test.

<sup>d</sup> Durability measured in a 25-50 cm<sup>2</sup> MEA during a hold at 1.2 V in H<sub>2</sub>/N<sub>2</sub> at 80°C, 150 kPa absolute, 100% relative humidity. Based on U.S. DRIVE Fuel Cell Tech Team Cell Component Accelerated Stress Test and Polarization Curve Protocols ([http://www.uscar.org/commands/files\\_download.php?files\\_id=267](http://www.uscar.org/commands/files_download.php?files_id=267)), Catalyst Support Cycle and Metrics (Table 2). Activity loss is based on loss of mass activity, using initial catalyst mass, at end of test.

<sup>e</sup> Test at 80°C H<sub>2</sub>/O<sub>2</sub> in MEA; fully humidified with total outlet pressure of 150 KPa; anode stoichiometry 2; cathode stoichiometry 9.5 (as per Gasteiger et al. Applied Catalysis B: Environmental, 56 (2005) 9-35).

<sup>f</sup> Volume = active area \* catalyst layer thickness.

<sup>g</sup> P. Zelenay, H. Chung, C. Johnston, N. Mack, M. Nelson, P. Turner, G. Wu, FY 2011 Progress Report for the DOE Hydrogen Program, p. 816, U.S. Department of Energy, Feb. 2011, DOE/GO-102011-3178.

**Figure 14.** United States Department of Energy 2012 Technical Plans Targets for Fuel Cells: Electrocatalysts for Transportation Applications [30].

## 1.4. Electrocatalysis of ORR.

### 1.4.1. Theoretical aspects: Butler-Volmer equation and Tafel approximation.

The oxygen reduction reaction (ORR) is one of the most important reaction in life processes such as biological respiration, and in energy converting systems such as fuel cells and metal-air batteries.

ORR in aqueous solutions occurs mainly by two pathways: the direct 4-electron reduction pathway from  $O_2$  to  $H_2O$ , and the 2-electron reduction pathway from  $O_2$  to hydrogen peroxide ( $H_2O_2$ ).

In polymer electrolyte membrane (PEM) fuel cells, including direct methanol fuel cells (DMFCs), ORR is the reaction occurring at the cathode. Normally, the ORR kinetics is very slow. In order to speed up the ORR kinetics to reach a practical usable level in a fuel cell, a cathode ORR catalyst is needed [43].

In order to minimize the losses due to cathodic activation overpotential, it is desirable that the ORR occurs at potentials as close as possible to the reversible electrode potential (thermodynamic electrode potential) with a satisfactory reaction rate.

We can represent the elementary reaction in a simple model:  $O + n_\alpha e^- \rightleftharpoons R$

where O and R represent the oxidant and reductant, and  $n_\alpha$  is the number of electrons transferred in a simple elementary reaction, which is different from the overall electron-transfer number (n) in a complex reaction such as ORR is. In fact, for a complex electrochemical reaction, the reaction mechanism consists of several elementary reactions, among which there should be one such elementary reaction as the reaction rate-determining step. The value of  $n_\alpha$  is normally 1. If we define E as the electrode potential and  $E_{eq}$  as the equilibrium potential for the electrochemical reaction (for ORR  $E_{eq} = 1.23$  V vs SHE), the overpotential ( $\eta$ ) is given by:

$$\eta = E - E_{eq}$$

Considering an elementary reaction, the relation between the current density and the overpotential is given by the Butler-Volmer equation [15,44,45]:

$$i = i_0 \left[ \exp\left(\frac{\alpha_a n_\alpha F \eta}{RT}\right) - \exp\left(-\frac{\alpha_c n_\alpha F \eta}{RT}\right) \right] \quad (5)$$

Where:

i is the current density;

$i_0$  is the exchange current density;

$n_\alpha$  is the number of electrons transferred in the rate determining step;

$\alpha_a$  and  $\alpha_c$  are the anodic and cathodic transfer coefficients respectively ( $\alpha_a + \alpha_c = 1$ );

$\eta$  is the overpotential;

F is the Faraday constant;

R is the gas constant;

T is the absolute temperature.

The exchange current density ( $i_0$ ) represents either the forward or backward current density when the forward and the backward reaction rates become equal, in other words, when the reaction is at the equilibrium state, and the net current in the system is zero.

As evident from the Butler-Volmer equation, overpotential is the driving force of the electrode reaction: the larger the overpotential, the faster the electrode reaction rate would be. It is also evident that if the overpotential is high enough (i.e.  $< -60$  mV), the first term in equation (5) becomes much smaller than the first one, and can be neglected. Therefore, the equation (5) can be rewritten as follows:

$$i = -i_0 \exp\left(-\frac{\alpha_c n_\alpha F \eta}{RT}\right) \quad (6) \quad (6)$$

That is, in linearized form:

$$E = E_{eq} - \frac{RT}{\alpha_c n_\alpha F} \ln(i_0) + \frac{RT}{\alpha_c n_\alpha F} \ln(i) \quad (7)$$

This is called Tafel equation, which gives a linear relationship between the potential and the logarithm of the current density. From the intercept and the slope of the straight line, both the exchange current density and the transfer coefficient can be calculated. The slope is called the “Tafel slope”. The higher the Tafel slope, the faster the overpotential increases with the current density. Thus, for an electrochemical reaction to obtain a high current at low overpotential, the reaction should exhibit a low Tafel slope [43].

#### 1.4.2. Electrochemical experimental techniques for ORR activity measurements.

##### Three-electrode electrochemical cell.

The three-electrode cell setup is the most common electrochemical cell configuration used to measure the ORR activity data. As shown in Figure XX, it counts of three electrodes, a reference electrode (RE), a working electrode (WE) and a counter electrode (CE) [46].

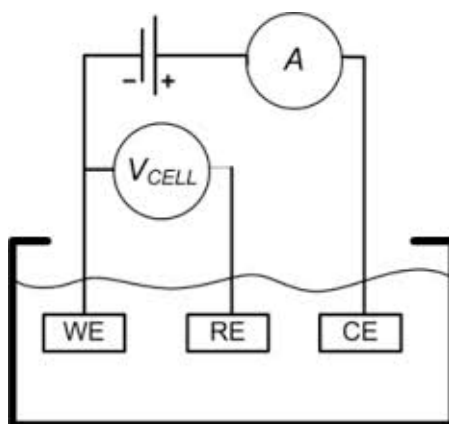
The RE is an electrode with a stable and well-known electrode potential and it is used as a point of reference in the electrochemical cell for the potential control and measurement. The high stability of the reference electrode potential is usually reached by employing a redox system with constant concentrations of each specie in the redox reaction. The current flow through the reference electrode is kept close to zero.

The WE is the electrode on which the reaction of interest is occurring. Working electrodes must be made of an inert material for the reaction of interest, and for the reaction environment. In particular, for experiments involving catalysts for ORR, the catalyst under examination is usually deposited on a WE made of glassy carbon (GC).

The CE is used to close the current circuit in the electrochemical cell. It is usually made of an inert material (e.g. Pt, Au, graphite, glassy carbon) and it does not participate in the electrochemical reaction. Because the current is flowing between the WE and the CE, the total surface area of the CE

(source / sink of electrons) must be higher than the area of the WE so that it will not be a limiting factor in the kinetics of the electrochemical process under investigation.

As shown in Figure 15, the current flows between the CE and the WE. The potential difference is controlled between the WE and the CE and measured between the RE (kept at close proximity of the WE) and the WE. The potential difference between RE and WE is controlled by controlling the polarization of the CE. The potential between the WE and CE usually is not measured. It is adjusted so that the potential difference between the WE and RE will be equal to the potential difference specified by the user. This configuration allows the potential across the electrochemical interface at the WE to be controlled with respect to the RE.

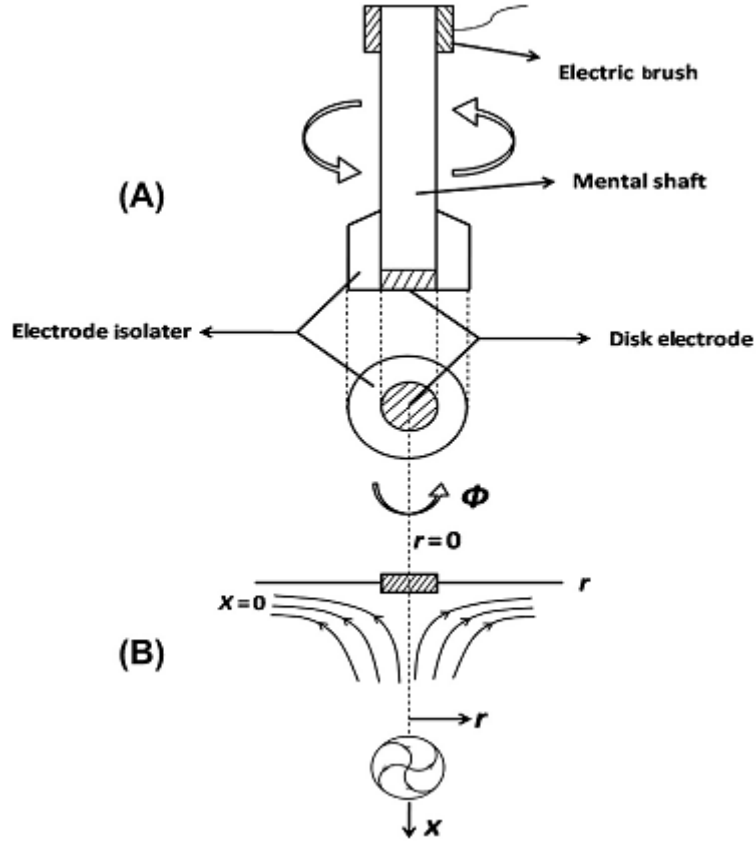


**Figure 15.** 3-electrodes electrochemical cell configuration [47].

### Rotating Disk Electrode (RDE)

The Rotating Disk Electrode apparatus is a special type of 3-electrodes electrochemical cell, where the WE can be put in rotation precisely controlling the rotating rate. In this way, a quantitative control of diffusion layer thickness is realized, resulting in feasible quantitative analysis of the electrode reaction kinetics. Due to the solution convection, the reactant (oxygen) dissolved in the solution will move together with the convection at the same transport rate [48,49].

Figure 16-A shows a schematic structure of the RDE. The disk electrode's surface is plane and it is in contact with the electrolyte solution. An electric insulator (e.g. Teflon) covers the remaining part of the electrode. An electrical brush is used to make the electrical connection between the electrode shaft and the electric cable. When the electrode is rotating, the solution runs from the bulk to the surface, and then it is flushed out along the direction parallel to the disk surface, as shown in Figure 16-B [48].



**Figure 16.** Scheme of the rotating disk electrode (A). Solution flow pattern near the disk electrode surface (B):  $x$  is the coordinate direction perpendicular to the disk electrode surface,  $r$  is the coordinate direction parallel to the disk surface, and  $\Phi$  is the coordinate direction of the electrode rotation, respectively [48].

The main equation governing the RDE operation is the Koutecky-Levich equation:

$$\frac{1}{I} = \frac{1}{I_K} + \frac{1}{I_L} \quad (8)$$

where  $I$  is the current measured at the disk electrode.

$I_K$  is the kinetic current density, that is, the current that would flow under the kinetic limitation if the mass transfer were efficient enough to keep the concentration at the electrode surface equal to the bulk value, regardless of the electrode reaction [15]:

$$I_K = nFAK_{O_2}C_{O_2}\Gamma_{cat} \quad (9)$$

Where:  $n$  is the overall electron transfer number,  $F$  is the Faraday's constant,  $A$  is the electrode area,  $K_{O_2}$  is the kinetic constant of ORR,  $C_{O_2}$  is the concentration of dissolved  $O_2$ , and  $\Gamma_{cat}$  is the catalyst loading on the electrode.

$I_L$  is the limiting current (or Levich current), which represents the height of the sigmoidal wave observed in rotating disk voltammetry. In fact, for high overpotential values, there is no more kinetic limitation for the electrochemical reaction, and the concentration of the electroactive species at the

electrode surface becomes is zero. Therefore, the current at the disk depends only from the diffusional processes, that is, from the electrode's rotation speed.

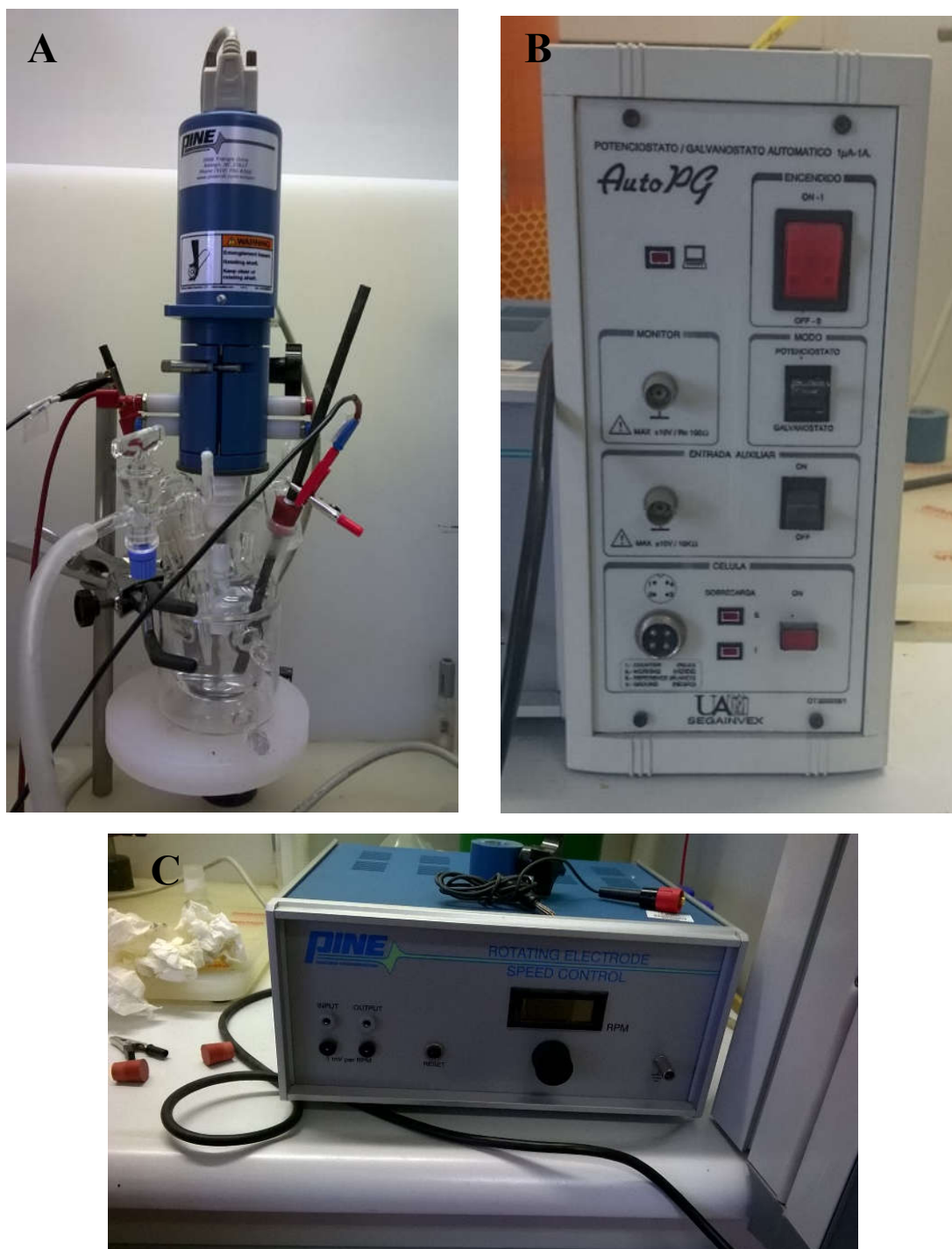
$$I_L = 0.62nFAC_{O_2}D_{O_2}^{2/3}\nu^{-1/6}\omega^{1/2} \quad (10)$$

Where:  $n$  is the overall electron transfer number,  $A$  is the electrode area,  $F$  is the Faraday's constant,  $C_{O_2}$  is the concentration of dissolved  $O_2$ ,  $D_{O_2}$  is the diffusion coefficient of  $O_2$  in the electrolyte solution,  $\nu$  is the kinematic viscosity of the electrolyte solution, and  $\omega$  is the electrode rotation speed [48]. In particular, recording the electrode polarization curve at different  $\omega$ , (being all the other parameters known), it is possible to calculate the overall electron transfer number ( $n$ ) from the slope of the plot of  $I_L^{-1}$  vs  $\omega^{-1/2}$ .



**Figure 17.** (A) RDE experimental setup for ORR tests in Politecnico di Torino – Green<sup>2</sup> Group Laboratory: RDE apparatus (Mod. ALS RRDE-3A) + Potentiostat (Mod. Bio-Logic SP-150). (B) Detail of the RDE 3-electrode electrochemical cell. (C) RDE apparatus coupled with thermostatic bath vessel used for measurement at different temperatures.





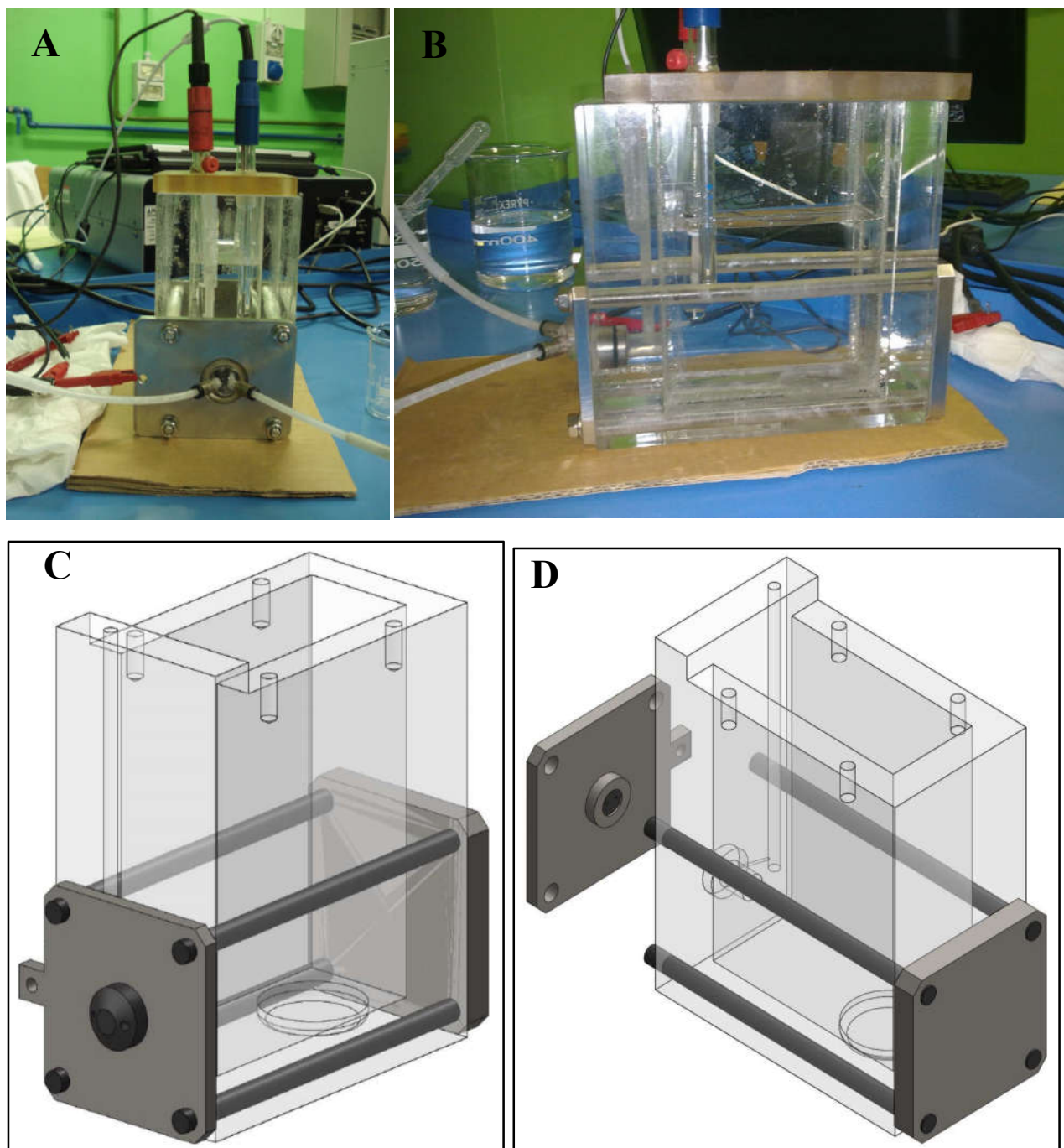
**Figure 18.** RDE experimental setup for ORR test in Universidad Autónoma de Madrid (UAM): RDE (Mod. PINE) + 3-electrode electrochemical cell (A), potentiostat-galvanostat (MOD. Auto-PG EG&G273A) (B), RDE rotation speed controller (Mod. PINE) (C).

### Gas Diffusion Electrode (GDE)

In a 3-electrodes cell configuration equipped with a gas diffusion electrode, the working electrode is substantially a half-MEA. That is, a piece of gas diffusion layer (GDL) is mounted into a holder

provided with a current collector. The GDL side covered with a catalyst layer is put in contact with the electrolyte solution and the back side is in contact with a chamber with a gaseous oxygen flow [50,51]. Optionally, a piece of membrane can be put on the catalyst layer, being in this way the system even more similar to a MEA [52,53].

As an example, in Figures 19 it is shown the GDE cell device that we used for our tests. In Figure 20 it is shown the preparation of the electrode.



**Figure 19.** Pictures (A-B) and scheme (C-D) of the GDE cell in Politecnico di Torino – Green<sup>2</sup> Group Laboratory.



**Figure 20.** Pictures of the Gas Diffusion Electrode preparation: catalyst ink deposition on the GDL (A), GDL disk cutting (B) and positioning in the holder of the plexiglass cell (C).

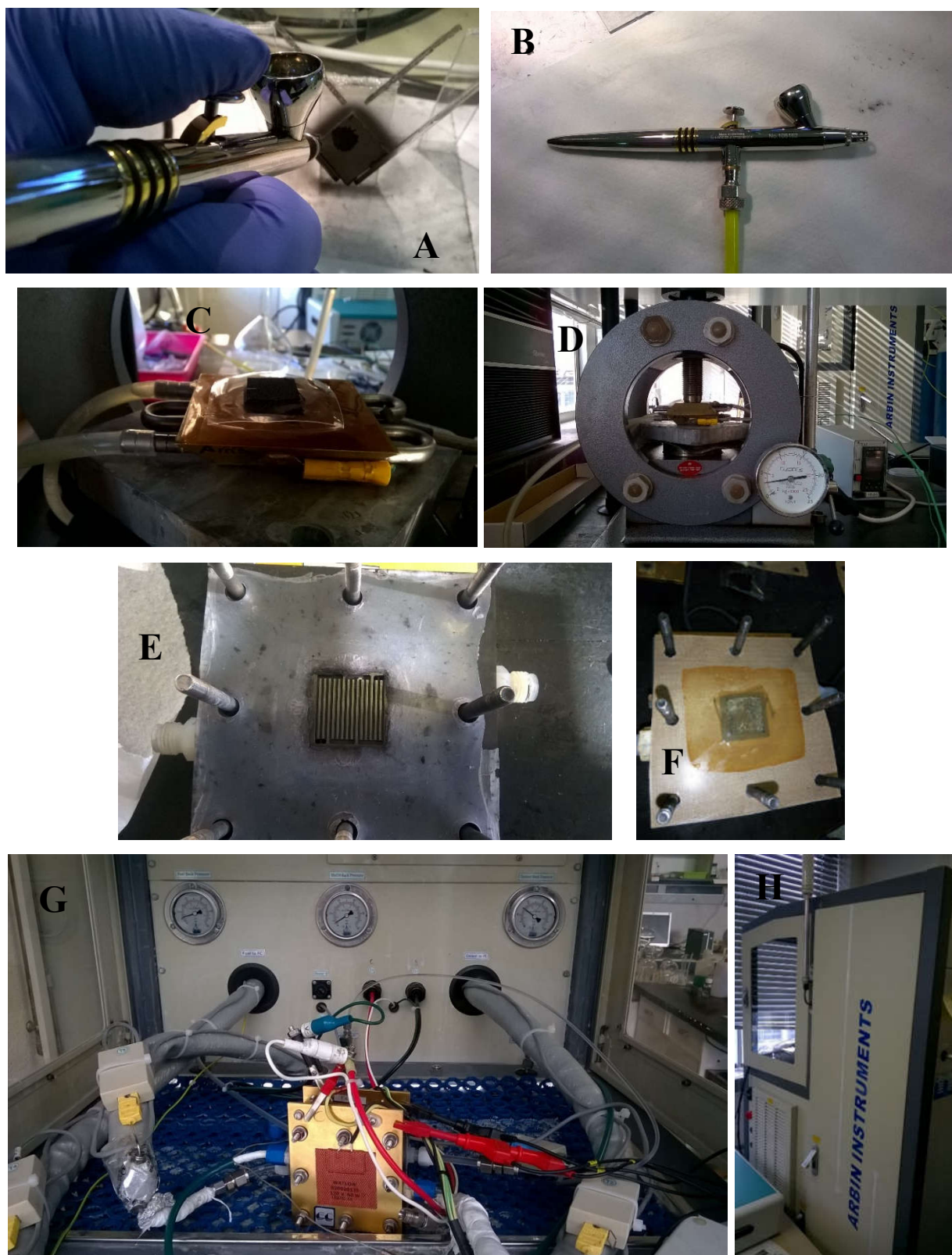
### Single Fuel Cell testing.

Testing a catalyst in a complete fuel cell device is the final step for the validation of its performances. This test is more complicated, costly and time consuming than the test in the 3-electrodes cell configuration, and it is usually performed after screening the ORR activity of a catalyst in RDE or GDE cell. However, the real performance of the catalyst in a fuel cell can be assessed. In this way, in addition to the ORR catalytic activity of the material, also other aspects like reactant and products mass transport problems (i.e.  $O_2$  gas diffusion,  $H^+$  transport through the membrane and the ionomer in the catalyst layer, water flooding) can be evaluated. Concerning the catalyst durability problem, the performance of the catalyst in a real fuel cell operating environment (e.g. temperature, pressure, pH, fuel crossover) can be assessed.

Many different operative variables must be considered in performing the test. In testing cathodic catalysts for ORR, a standard commercial Pt or Pt-Ru based catalyst (for  $H_2$  and methanol fueled fuel cells, respectively) is usually used at the anode. Cell temperature, electrolyte membrane type and thickness, reactants pressure and flow rate are other variables to be chosen. In case of liquid fuel (i.e. direct alcohol fuel cells), its concentration must also be chosen. For gaseous reactants, the possibility of humidification of the gas stream should also be considered. All these operating conditions have an influence on the performance of the fuel cell.

In the pictures of Figure 21, the different steps of the preparation of a MEA for the test in the single fuel cell station are shown.





**Figure 21.** The different steps for the single fuel cell test. (A) Brushing the catalysts ink on the GDL. (B) View of the air-brush used for the deposition of the catalysts on GDL. (C) Preparation of the MEA by hot pressing anode and cathode on the membrane. (D) View of the hot-press apparatus. (E) View of the channels of the bipolar plate. (F) Positioning the MEA between the graphite bipolar plates in the single fuel cell case. (G) Single fuel cell connected to the fuel and oxygen inlet and outlet in the test station. (H) View of the fuel cell test station (MITS Pro-FCTS, Arbin Instruments) in the UAM laboratory.

### **1.5. Non Precious Metal Catalysts (NPMC) for ORR.**

In 2005, a detailed review by Gasteiger et al. [39] highlighted the fact that even a Pt-free catalyst having a volumetric activity ( $A \text{ cm}^{-3}$  of catalytic layer) less than 1/10 of a Pt/C catalysts could never be used for automotive applications due to the very tight volumetric constraints when designing an automobile. Fortunately, several breakthroughs since 2005 have led to significant advances in the activity of NPMC. Therefore, in addition to strictly focusing only on ORR activity improvements, the optimization of the catalyst layer has become a crucial area of work for NPMC researchers. In fact, the much lower ORR activity of NPMCs versus Pt/C has necessitated much thicker cathode catalyst layers ( $\sim 100 \mu\text{m}$  for NPMC versus  $\sim 12 \mu\text{m}$  for Pt/C [54]) and it has become widely known that thick catalyst layers result in mass transport limitations [55].

The targeted Pt loading for automotive application is  $0.1 \text{ mg cm}^{-2}$  per electrode in 2015. While a negligible performance decay occurs when the anode Pt loading is reduced from 0.4 to  $0.1 \text{ mg cm}^{-2}$ , an equal reduction at the cathode without adverse effects on the performance requires that the mass activity of Pt catalysts be increased by 4-fold [56]. This explains the major focusing on the research about alternative catalysts to replace Pt at the cathode side of the fuel cell than to the anode side.

Despite the great advances in activity, the NPMC have shown remarkably poor stability and durability. Stability refers to the ability to maintain performance at constant current conditions while durability refers to the ability to maintain performance following a voltage cycling accelerated stress test. In the literature, three main mechanisms of instability for NPMCs are generally proposed [55]:

- 1) dissolution/leaching of the active metal site;
- 2) oxidative attack by  $\text{H}_2\text{O}_2$  or the resulting free radicals;
- 3) protonation of the active site or protonation of a N species neighbouring the active site followed by anion adsorption.

Regardless of the mechanism, state-of-the-art NPMCs have still demonstrated poor stability when tested in a membrane electrode assembly (MEA).

#### **1.5.1. Different types of NPMC.**

##### **M-N-C catalysts.**

The most promising NPMC for ORR in low-temperature fuel cell application are carbon-supported transition metal/nitrogen (M-N<sub>x</sub>/C) materials (M = Co, Fe, Ni, Mn, etc., and normally  $x = 2$  or 4). They have gained increasing attention due to their promising catalytic activity towards ORR, along with the utilization of abundant and inexpensive precursor materials. It was demonstrated since from 1964 that transition metal macrocyclic molecules like porphyrins and phthalocyanines could act as ORR electrocatalysts. However, they showed stability issues, as the catalyst structure decomposition in acidic media, resulting in a loss of catalytic activity. A significant breakthrough was achieved when

high temperature heat treatment (400 – 1000 °C) were introduced to the catalyst synthesis process. This approach modify the structure of M–Nx/C materials, increasing the concentration of available ORR active sites while at the same time improving the catalyst stability [57].

Therefore, due to the structure modification after the high temperature heat treatment, it was proposed that the particular use of transition metal macrocycle compounds was not strictly required, and that catalytically active sites could be formed with a variety of different metal, nitrogen and carbon precursor materials. The only requirement for the production of ORR active sites is that elemental metal ions (Fe, Co, etc.) a source of carbon (carbon support, molecule, polymer), and a source of nitrogen (macrocycle, N-bearing molecule or polymer, N-containing gas) are simultaneously present during the heat-treatment [31].

### **Conductive polymers**

Conductive polymers such as polypyrrole, polyaniline, polythiophene, poly-3-methyl-thiophen, poly-3,4-ethylenedioxythiophene, characteristically display mixed metal and polymer like properties and are considered ideal for many applications due to their low cost, high electronic conductivity and redox properties [57]. Conductive polymers have been investigated as non-precious ORR electrocatalysts in three different ways:

- utilizing conductive polymers as ORR electrocatalysts on their own [58,59];
- incorporating non-precious metal complexes into the conductive polymer matrix [58–61];
- employing conductive polymers as a nitrogen/carbon precursor material for preparing M–Nx/C catalysts via a high-temperature heat treatment, as described before [62,63].

### **Non-precious transition metal chalcogenides.**

Many different types of non-precious transition metal chalcogenides have been demonstrated to have a potential application as ORR electrocatalysts. These materials can be indicated as  $M_zN_{3-z}X_4$ , where  $M = \text{Mn, Fe, Co, Ni, Cu or Zn}$ ,  $N = \text{Ti, V, Cr, Fe, Co or Ni}$  and  $X = \text{S, Se or Te}$ . However, their ORR activity and stability are still significantly lower than those of commercially available Pt/C catalyst, and furthermore, lower than those of precious metal chalcogenide compounds like for example Mo–Ru–Se. The research is focusing in developing novel non-precious chalcogenides (including new binary and ternary combinations) along with the optimization of bulk and surface properties. The use of a carbon support could also improve the dispersion and consequently the reactive surface area of transition metal chalcogenide particles [57].

### **Non-precious transition metal oxides.**

Non-precious transition metal oxides like zirconia, tungsten oxide and cobalt oxides possess reasonable ORR activity and stability in alkaline media. However, despite suitable stability in acidic and oxidizing conditions, their limited ORR activity still remains a challenge [64,65]. The low ORR

activity is attributed to the low conductivity and poor adsorption of oxygen on the surface suggesting they may not be suitable as cathode catalysts for acidic fuel cells. Regardless, numerous studies have been reported in recent years investigating the potential application of metal oxide composites as ORR electrocatalysts. However, their performance is still not sufficient enough for practical usage as acidic fuel cell cathode catalysts. For developing more active and stable ORR catalysts, more research is necessary in order to provide facile  $O_2$  adsorption and enhanced electronic conductivity, coupled with improved stability in acidic media [57].

#### **Non-precious transition metal nitrides.**

Transition metal nitrides have shown relatively good stability in acidic conditions and under high electrochemical potentials. Therefore they could be considered as potential ORR electrocatalysts. For example, carbon supported tungsten nitride ( $W_2N/C$ ) was investigated using a single PEM fuel cell setup, where significant stability after 100 hours of operation was observed [66]. Although the ORR activity of this material was relatively low (ORR onset potential of 0.6 V vs. RHE), its high stability renders it as a promising non-precious electrocatalyst. Molybdenum nitride materials were also investigated as ORR electrocatalysts [67]. When supported on carbon black, these  $Mo_2N/C$  catalyst materials were found to display an open circuit potential of over 0.7 V in a single fuel cell setup.

#### **Non-precious transition metal oxynitrides.**

Metal oxynitrides are another kind of materials which show some ORR activity. These materials are commonly obtained by substitutionally doping nitrogen into metal oxides. This doping could effectively reduce the high inherent band gap of metal oxides, leading to enhanced electron conducting properties important to electrocatalysis [68]. Ta oxy-nitrides were investigated as ORR electrocatalysts and found to have a promising onset potential of 0.8V vs RHE.216 In addition, the incorporation of carbon into this kind of material could also further enhance their ORR activity [69]. Another example is carbon supported zirconium oxynitride ( $ZrO_xN_y/C$ ) catalysts formed by pyrolyzing  $ZrO_2/C$  at a high temperature in the presence of ammonia. This catalyst material gave an ORR onset potential of 0.7 V vs. RHE [70].

#### **Enzymatic compounds**

The extremely high onset potential and ORR activity observed on several naturally occurring oxygen reducing oxidase enzymes has stimulated in recent years the exploration of enzyme modified electrodes as alternative non-precious fuel cell cathode materials [57]. However, these systems have many issues, like the strict ORR activity dependency on temperature and pH [71]. Enzyme based catalysts in fact, could only give optimal activity at mildly acidic conditions [72]. Moreover, considering their issues with stability, utilizing these types of materials as PEM fuel cell cathode catalysts may not be realistic [57].

### 1.5.2. The best “state-of-the-art” NPMC.

Until now the maximum FC performance using NPMC catalysts available in the literature are listed in Table 1. They all belong to the M-N-C pyrolyzed (heat treated at high temperature) catalysts.

**Table 1.** Performance of NNM catalysts available in the literature measured in single cell PEMFC at 80 °C, fully humidified H<sub>2</sub> and O<sub>2</sub>.

| Research group                | Starting precursors of Fe-N <sub>x</sub> -C catalysts developed, and pyrolyzation conditions   | Max power density<br>mW cm <sup>-2</sup> | Specific power density<br>mW mg <sub>cat</sub> <sup>-1</sup> | PEMFC conditions used  |
|-------------------------------|--|--|--|--|
| Lefèvre <i>et al.</i> [73]    | Black Pearls 2000 mixed with iron acetate, ball milling. Pyrolyzation @ 1050 °C in NH <sub>3</sub>   | 280                                      | 280  | 5 cm <sup>2</sup> MEA Nafion 117, cathode: 5 mg <sub>NNM</sub> cm <sup>-2</sup> ; anode: 0.5 mg <sub>Pt</sub> cm <sup>-2</sup> (Pt/C 20 wt.%), 1 bar gauge, 0.5 bar attributed to water vapour     |
| Wu <i>et al.</i> [62]         | Ketjenblack EC 300J mixed with aniline, ammonium peroxydisulfate, iron chloride, and cobalt nitrate. Two pyrolyzations in N <sub>2</sub> from 400 to 1000 °C with intermediate acid leaching | 550                                      | 138  | 5 cm <sup>2</sup> , MEA Nafion 1135, cathode: 4 mg <sub>NNM</sub> cm <sup>-2</sup> ; anode: 0.25 mg <sub>Pt</sub> cm <sup>-2</sup> , 2.8 bar gauge   |
| Cheon <i>et al.</i> [74]      | FeTMPPCl, CoTMPP and SBA15. Pyrolyzation @ 800 °C in N <sub>2</sub>  | 700                                      | 460  | 25 cm <sup>2</sup> MEA Nafion 212, cathode: 1.52 mg <sub>NNM</sub> cm <sup>-2</sup> ; anode: 0.425 mg <sub>Pt</sub> cm <sup>-2</sup> (Pt/C 60 wt.%), 2 bar, gauge, 0.47 attributed to water vapour |
| Zitolo <i>et al.</i> [75]     | ZIF-8, 1,10-phenanthroline and iron acetate. Pyrolyzation @ 1050 °C in Ar and 5 min @ 950 °C in NH <sub>3</sub>  | 528                                      | 132  | 5 cm <sup>2</sup> MEA Nafion 211, cathode: 4 mg <sub>NNM</sub> cm <sup>-2</sup> ; anode: 0.5 mg <sub>Pt</sub> cm <sup>-2</sup> , 1 bar gauge   |
| Strickland <i>et al.</i> [76] | 2-methylimidazole, zinc nitrate, 1,10 phenanthroline, iron acetate. Pyrolyzation @ 1050 °C in Ar and 18 min @ 1050 °C in NH <sub>3</sub>   | 380                                      | 127  | 5 cm <sup>2</sup> MEA Nafion 211, cathode: 3 mg <sub>NNM</sub> cm <sup>-2</sup> ; anode: 0.25 mg <sub>Pt</sub> cm <sup>-2</sup> (Pt/C 20 wt.%), 1.5 bar gauge                                      |
| Zhao <i>et al.</i> [77]       | Imidazole, ZnO, f tris-1,10-phenanthroline, iron(II) perchlorate (TPI). Pyrolyzation @ 1050 °C in Ar, acid leaching, pyrolyzation 15 min @ 950 °C in NH <sub>3</sub>                         | 620                                      | 282  | 5 cm <sup>2</sup> MEA Nafion 211, cathode: 2.2 mg <sub>NNM</sub> cm <sup>-2</sup> ; anode: 0.25 mg <sub>Pt</sub> cm <sup>-2</sup> (Pt/C 20 wt.%), 1.5 bar gauge                                    |

Different approaches have been adopted to synthesize the active NNM catalysts listed in Table 1. For the first one, ammonia was used as nitrogen source fluxing it into a hot tubular furnace containing the



mixture of carbon and transition metal [73]. For the second one, aniline was polymerized in presence of a transition metal, then two consecutive pyrolyzations were performed [62]. For the third one, a dry macrocyclic molecule was mixed with a porous silica template and then pyrolyzed in order to obtain a porous catalyst [74]. For the fourth one a commercial metal organic framework, zeolitic imidazolate framework (MOF ZIF-8), 1,10-phenanthroline and Fe(II) acetate were dry mixed together in a ball mill, then pyrolyzed first under argon for 1 h and then under ammonia at 950 °C for 5 min, no intermediate acid leaching was performed [75]. For the fifth one, 1,10 phenanthroline, Fe(II) acetate, 2-methylimidazole and Zn(II) nitrate were mixed together to obtain a complex used to impregnate an in-house synthesized MOF. Two pyrolysis steps followed, first under argon at 1050 °C for 1 h, then under ammonia for 18 min, without intermediate acid leaching [76]. For the sixth catalyst, 5% of tris-1,10-phenanthroline Fe(II) perchlorate was mixed with ZnO and imidazole, grinded and sealed in an autoclave for 18 h at 180 °C. The product was first pyrolyzed at 1050 °C for 1 h under argon followed by a second pyrolysis under ammonia for 15 min at 950 °C, with an intermediate acid leaching [77]. In these six different syntheses, high temperature and porosity of the support play an important role in the production of highly active electrocatalyst as well as the pyrolysis atmosphere and the transition metals used.

### 1.5.3. Different proposed theories for the ORR active sites in M-N-C catalysts.

Despite decades of research, the nature of the catalytic sites in M-N-C non-noble metal catalysts for ORR is still a topic of debate. The major debate is about the role of the transition metal: is it an active participant in the ORR or it is not?

Starting from a precursor where the M-N<sub>4</sub> structure of the chelate is present, what happens to this structure during the thermal treatment in inert gas (i.e. N<sub>2</sub> or Ar)? This topic was strongly debated in the past, and it is still not completely understood today. Essentially, three models of the catalytic site for ORR were presented, one each by the research groups of van Veen, Yeager, and Wiesener, respectively [42].

- van Veen theory: the thermal treatment at temperatures at which catalytic activity is maximum (500 - 600 °C) does not lead to the complete destruction of the M-N<sub>4</sub> structure, but just to a modification which keeps the M-N<sub>4</sub> moiety intact, remaining the ORR active site structure the same as for the unpyrolyzed macrocyclic molecules.
- Yeager theory: the decomposition of M-N<sub>4</sub> macrocyclic structure starts at about 400 - 500 °C and, going at higher temperatures (800 - 850 °C), most of the coordinated transition metal becomes a mixture of oxides and metal, which spontaneously oxidize when exposed to air at room temperature. Upon contact with an electrolyte solution, the oxide species undergo dissolution, and

metallic ions subsequently adsorb or coordinate to the thermally formed N-containing sites on the carbon surface. These N-containing sites are different from the macrocycle-like M-N<sub>4</sub> structures, differently from what proposed by van Veen. The resulting M-N<sub>x</sub>-C structure, is believed to be the catalytic site for ORR.

- Wiesener theory: the role of the transition metal ions initially present in the M-N<sub>4</sub> structure of the precursor is to promote the decomposition of the chelate during the heat treatment. This leading to the formation, of C-N<sub>x</sub>, a special form of N-doped carbon, that is the true catalyst. In this case, the metal would be only a “catalyst” for the formation of the active sites, but it has no role in the ORR.

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## **CHAPTER 2. The use of different types of reduced graphene oxide for the preparation of Fe-N-C electrocatalysts for the oxygen reduction reaction.**

### **1. Introduction**

Fuel cell devices produce electricity from the energy of a fuel through a highly efficient direct electrochemical conversion process, resulting in low emissions and low environmental impact [1]. Between the different types of fuel cell, the Polymer Electrolyte Membrane Fuel Cell (PEMFC) is the most attractive for the replacement of internal combustion engine for transport applications [2], and the Direct Methanol Fuel Cells (DMFC) are very promising energy sources for low power portable electronic applications [3]. In both these devices, platinum is the most widely used catalyst for the anodic hydrogen and methanol oxidation reactions, and for the cathodic oxygen reduction reaction (ORR) [4]. The high cost of Pt is the main factor that contributes to the high cost of PEMFC and DMEFC, and this has been so far one of the main bottlenecks to the widespread commercialization of fuel cell [5]. On the cathode of the fuel cell, the sluggish reaction kinetics for the ORR leads to great overpotentials and therefore to low conversion efficiency. For this reason, higher Pt loadings are needed at the cathode than at the anode of PEMFC, stimulating consequently the research toward alternative Pt-free catalysts for ORR [6].

Several types of carbon materials functionalized with nitrogen and transition metals (Me-N/C, Me = transition metal) have been investigated as non-precious metal catalysts (NPMC) for ORR [7]. The exact structure of the ORR active site in these materials has not been clearly identified so far [8]. However, the active site is believed to be formed during a heat-treatment at 500 – 1000 °C with the simultaneous presence of transition metal ions (Fe, Co, etc.), a source of carbon (carbon support, polymer) and a source of nitrogen (N-containing molecule, polymer or gas). According to this fact, many synthesis strategies can be adopted for the preparation of NPMC supported on carbon-based materials [9]. For example, a carbon support with a high specific surface area can be impregnated with a complex formed in solution between a N-containing ligand molecule (e.g. TPTZ, 1,10-Phenanthroline) and a transition metal ion (i.e. Fe, Co) [10–13].

In particular, these NPMC have been found to be much more active towards ORR in alkaline than in acid conditions [14,15]. This has stimulated research in the development of alkaline ionomers (conducting OH<sup>-</sup> ions) [16].

To improve the activity and the stability of Me-N/C catalysts, many approaches have been explored. These include the development of new synthesis procedures, the optimization of heat-treatment



strategies, the exploration of different carbon supports, and the use of different transition metal and nitrogen containing precursor molecules [17].

Within many different carbon support materials, graphene has attracted great interest in recent years, due to its unique properties, like high theoretical surface area, high electrical conductivity and good chemical stability within a broad potential window [18].

Graphene with a relatively perfect structure and excellent properties can be produced by micro-mechanical exfoliation of highly ordered pyrolytic graphite and chemical vapor deposition (CVD) [19]. Chemically modified graphene can be obtained from graphite oxide through a cost-effective and high-yield chemical method, which is theoretically implementable for large scale production [18,20]. This material, named reduced graphene oxide (rGO), has a great amount of residual functional groups and defects that dramatically alter the structure of the carbon plane [21,22].

rGO is produced from graphite oxide (GO). GO has a similar layered structure to graphite, but the plane of carbon atoms in GO is rich in oxygen-containing groups, which expand the interlayer distance and make the atomic-thick layers hydrophilic. As a result, these oxidized layers can be exfoliated in water under moderate ultrasonication [22,23]. If the exfoliated sheets contain only one or few layers of carbon atoms like graphene, these sheets are named graphene oxide (GO). The most attractive property of GO is that it can be partly reduced to graphene-like sheets by removing the oxygen-containing groups with the recovery of a conjugated structure. The rGO sheets can be considered as one kind of chemically derived graphene [22].

In the literature, different reduction / exfoliation methods are reported: thermal annealing, microwave irradiation, chemical reduction with strong reducing agents (i.e. hydrazine or  $\text{NaBH}_4$ ), photocatalyst reduction, electrochemical reduction, solvothermal reduction and multistep reduction using combinations of different methods [21–25]. In the thermal annealing process, the exfoliation of the GO flakes is caused by the huge pressure increase generated by the sudden expansion of gases (mainly CO and  $\text{CO}_2$ ) evolved into the spaces between the graphene sheets during the heating [26]. The heating temperature significantly affects the GO reduction. If the temperature is less than 500 °C, the C/O ratio increase only up to no more than 7, while if the temperature reached 750 °C, the C/O ratio could be higher than 13. So, high temperature is needed to achieve the good reduction and electrical conductivity [22,27].

In this paper, three different types of rGO are obtained from the same GO with three different reduction-exfoliation methods. They are therefore used as carbon support materials for the synthesis of Fe-N/rGO catalysts. Fe and N were incorporated onto the rGO supports surface by a wet impregnation with the complex between Fe(II) ions and the N-rich ligand molecule TPTZ (six nitrogen atoms per molecule), followed by a heat treatment in inert atmosphere at 800°C for 3 hours.

Morphology, chemical composition, physical properties and crystalline structure of all the catalysts and their respective supports were also investigated using several instrumental methods. The activity toward ORR of the as-synthesized catalysts has been tested using RDE technique in alkaline medium. Electrochemical kinetic parameters like Tafel slope, cathodic transfer coefficient and exchange current density have also been calculated.

## 2. Experimental

### 2.1. Chemicals

Synthetic graphite flakes TIMCAL C-ENERGY SFG 6 L was purchased from IMERYS and used as received. Concentrated sulfuric acid (98 % wt.) and ethanol (>99.8% purity) were purchased from Fluka. Sodium nitrate ( $\text{NaNO}_3$ , >99.0% purity), potassium permanganate ( $\text{KMnO}_4$ , >99.0% purity), hydrogen peroxide ( $\text{H}_2\text{O}_2$ , 30% wt.), 2,4,6-tris(2-pyridyl)-1,3,5-triazine (TPTZ,  $\geq 98\%$  purity), iron(II) acetate ( $\text{Fe}(\text{CH}_3\text{COO})_2$ , >99.99% purity), Nafion (5% wt hydroalcoholic solution), concentrated hydrochloric acid (37% wt.) and potassium hydroxide (KOH, 99.0% purity) were purchased from Sigma Aldrich. Nitrogen, hydrogen and oxygen gases were purchased in cylinders by SIAD with purity  $\geq 99.999\%$ . All aqueous solutions were prepared using deionized water obtained from a Millipore Milli-Q system with resistivity  $>18 \text{ M}\Omega \text{ cm}^{-1}$ .

### 2.2. rGO supports preparation

Graphite oxide was prepared using the modified Hummers method [28,29]. In detail, 115 mL of concentrated  $\text{H}_2\text{SO}_4$  (98%) was added to a mixture of graphite flakes (5 g) and sodium nitrate (2.5 g) under stirring until complete homogeneous dispersion. The mixture was kept into an ice bath to avoid the temperature to raise over 20 °C. Then, 15 g of  $\text{KMnO}_4$  was slowly added to the mixture in small portions. After reacting for 24 hours, water (700 mL) was added to the slurry producing a large amount of heat. Then, 30%  $\text{H}_2\text{O}_2$  (5 mL) was dropped to complete the oxidation. The slurry was cooled at room temperature into a water bath and left decanting without stirring for 24 hours to obtain a brown precipitate. The supernatant was removed and the precipitate was filtered and washed repeatedly with 1 M HCl solution and deionized water until pH was about 7. Finally GO was dried at 60° in oven.

The exfoliation/reduction of GO was carried out in 3 different ways. For the first method, GO was put into a quartz boat and placed in a tubular quartz furnace under  $\text{N}_2$  atmosphere ( $\text{N}_2$  gas flow was set at  $150 \text{ N mL min}^{-1}$  with a mass flow controller from Bronkhorst, ELFLOW series). The temperature was increased until 700°C with a heating rate of  $5^\circ\text{C min}^{-1}$  and kept constant for 1 hour.

Then the furnace was switched off leaving the apparatus cooling down naturally to room temperature. The second method was similar to the previous, but the gas atmosphere was a 1:1 vol. mixture of  $H_2$  and  $N_2$  and the heating temperature was 500°C. Finally, the third method consisted in dispersing the GO in acid solution (1:1 vol. solution of 1 M HCl and ethanol) and keeping this dispersion under sonication (130 W, Soltec 2200 M 3S sonicator) for 3 hours. The three rGO obtained with these three different exfoliation/reduction methods were named rGON700, rGOHN500 and rGOsonic, respectively.

### ***2.3. Fe-N/rGO electrocatalysts preparation***

The three rGO were used as carbon support material to prepare three Fe-N/rGO catalysts. The synthesis method consists in a wet impregnation of a complex between a N-containing ligand molecule and Fe(II) ion, followed by a heat treatment at 800°C under inert atmosphere. For each rGO type, a typical amount of 100 mg was dispersed in 100 mL of a 1:1 vol. deionized water and ethanol solution under ultrasonic bath for 30 minutes (130 W, Soltec 2200 M 3S sonicator), and left stirring for 1 hour. At the same time, 176 mg of TPTZ ligand molecule, used as a nitrogen source, was dissolved in about 100 mL of deionized water, and the pH was adjusted to 1 by addition of 1 M HCl solution under stirring. This helps the dissolution of the TPTZ in the solvent. Then, 16.4 mg of  $Fe(CH_3COO)_2$  was added to the solution, with the immediate formation of a blue-colored complex. The Fe:TPTZ molar ratio in this complex was of 1:6. This excess of TPTZ ligand should favor the chemical equilibrium of the  $Fe^{2+}$  ion complexation. Moreover, this provides a greater amount of N atoms, in order to favor a higher doping level of the rGO surface with N atoms, favoring thus the formation of active sites [30]. The solution was left stirring at room temperature for 6 hours, added to the rGO dispersion and stirred overnight. The solvent was evaporated by heating, and the recovered powder was ground in a mortar. The Fe:rGO mass ratio in this powder was expected to be 0.05. All the three powders were then heat treated in a tubular quartz furnace at 800 °C for 3 hours under  $N_2$  flow (heating rate of 5°C min<sup>-1</sup>). The catalysts derived from the three different rGO supports were named Fe-N/rGON700, Fe-N/rGOHN500 and Fe-N/rGOsonic, respectively.

### ***2.4. Physico-chemical characterization***

Nitrogen adsorption isotherms of rGO supports and their respective catalysts were recorded by an ASAP 2020 Instrument (Micromeritics) at -196 °C. Before the analysis, all of the samples were placed into the cell and degassed under vacuum for 3 hours at 150 °C. The specific surface area of the samples was calculated using the Brunauer–Emmett–Teller (BET) method within the relative

pressure range of 0–1. The pore size distribution was obtained with the Barrett–Joyner–Halenda (BJH) method.

Scanning electron microscopy coupled with energy-dispersive X-ray spectroscopy (SEM-EDX FEI-Quanta™ Inspect 200 with EDAX PV 9900 instrument working at 15 kV) were performed to analyze the morphology and evaluate the average bulk chemical composition of rGO supports and Fe-N/rGO catalysts.

The crystallographic structures of the samples were analyzed using X-ray powder diffraction (XRD) with X'Pert PRO diffractometer (PANalytical) using a Cu K $\alpha$  radiation ( $\lambda = 0.15406$  nm). The X'Pert HighScore software (PANalytical) was used to determine the crystallographic phases associated with the peaks that appear in the XRD patterns.

X-ray photoelectron spectroscopy (XPS) was performed to determine the elemental surface composition of the catalysts samples. The analysis was carried out using a Physical Electronics PHI 5000 Versa Probe electron spectrometer system with monochromated Al K $\alpha$  X-ray source (1486.60 eV) run at 15 kV and 1 mA anode current. Survey scans as well as narrow scans (high resolution spectra) were recorded with a spot of 100 nm size. The survey spectra were collected from 0 to 1200 eV. The narrow N 1s spectra were collected from 396 to 405 eV and the narrow C 1s spectra from 280 to 293 eV. All of the spectra related to the three samples were obtained under identical conditions, with the samples placed in an ultrahigh vacuum chamber at  $2 \cdot 10^{-10}$  mmHg, and calibrated against a value of the C 1s binding energy of 284.5 eV. CasaXPS software was used for obtaining semi-quantitative atomic percentage compositions, using Gauss-Lorentz equations with Shirley background.

## ***2.5. Electrochemical characterization***

The electrochemical measurements for rGO supports and their respective Fe-N catalysts were performed in a conventional three-electrodes electrochemical cell configuration. The cell was equipped with a glassy carbon disk working electrode (0.0707 cm<sup>2</sup> geometric area), a Pt helical wire counter electrode, and a saturated calomel (SCE) reference electrode. Cyclic voltammetries (CV) and linear sweep voltammetries (LSV) were performed using a rotating disk electrode (RDE) equipment (RRDE-3A ALS) and a multi-potentiostat (Bio-Logic SP-150).

All of the inks were prepared in the same way. A typical ink preparation consists in mixing 10 mg of sample powder with 43  $\mu$ L of Nafion® 5% wt. solution and 400  $\mu$ L of ethanol. The ink was kept under sonication for 1 hour to achieve a good dispersion. Afterwards, 1  $\mu$ L of ink was taken with a micro-pipette and deposited on the working electrode, resulting in a catalyst loading of 0.0225 mg, which corresponds to 0.318 mg cm<sup>-2</sup> referred to the geometrical area of the disk working electrode.

All of the current densities were thus normalized per geometric area of the electrode. The electrode potentials were corrected and referred to the reversible hydrogen electrode (RHE). The electrolyte was 0.1 M KOH aqueous solution, saturated with either N<sub>2</sub> or O<sub>2</sub> by direct gas bubbling into the electrolyte solution.

Prior to start tests, 80 CV cycles were performed from 0.0 to 1.2 V vs RHE in N<sub>2</sub> saturated electrolyte at 100 mV s<sup>-1</sup> scan rate, in order to electrochemically clean and stabilize the working electrode surface. For each rGO support and catalyst, cyclic voltammograms were recorded between 0.0 and 1.2 V vs RHE in N<sub>2</sub>-saturated electrolyte at 10 mV s<sup>-1</sup> scan rate. For the ORR measurements, the solution was saturated with O<sub>2</sub>. LSV were recorded at 5 mV s<sup>-1</sup> scan rate. This scan rate value should be sufficiently low to consider the background capacitive current contribution negligible [31], and sufficiently high to allow to neglect the possible effect of impurities in the cell [31 – 33]. An electrochemical impedance spectroscopy measurement was done at OCV, with a wave amplitude of 10 mV and frequencies in the range of 10 kHz – 100 mHz, for the evaluation of the high frequency resistance value. This value was used to subtract the ohmic drop contribution from the linear sweep voltammetry curves [33].

### 3. Results and discussion

#### 3.1. Physico-chemical characterization of rGO supports and Fe–N/rGO catalysts

##### 3.1.1. BET and pore size analysis

The surface area values of the three rGO samples (Table 1) are very different depending on the reduction - exfoliation method. rGON700 has the highest BET surface area (104.7 m<sup>2</sup> g<sup>-1</sup>) suggesting that the thermal annealing exfoliation in N<sub>2</sub> atmosphere at 700°C is the best method to obtain an highly exfoliated rGO. rGOHN500 surface area is almost one half of the previous sample (51.8 m<sup>2</sup> g<sup>-1</sup>), suggesting that for this thermal annealing exfoliation method the temperature effect seems to be more important than the presence of a reducing agent (H<sub>2</sub> in this case). The sonication process leads to obtain a lower surface area (11.5 m<sup>2</sup> g<sup>-1</sup>).

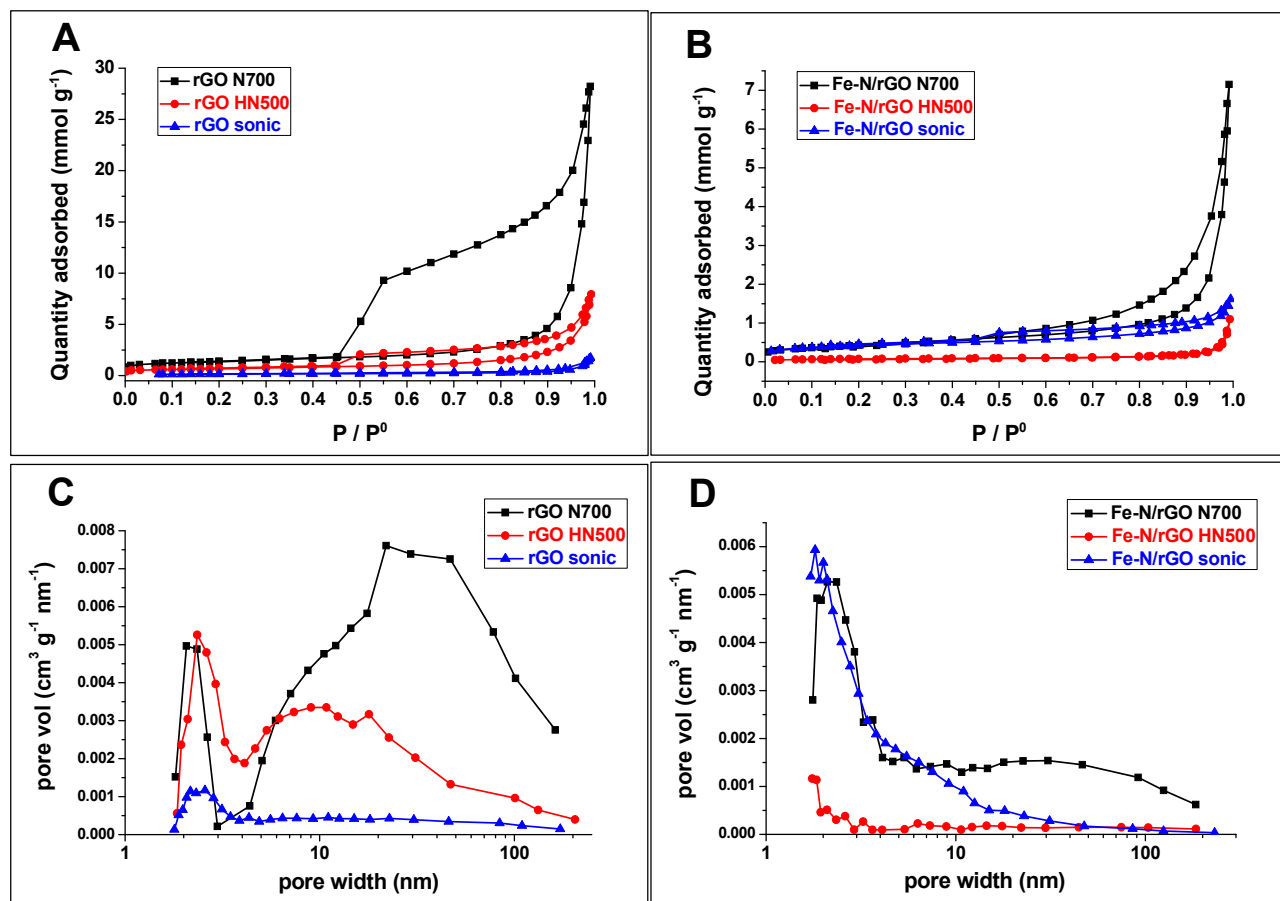
**Table 1.** Properties calculated from the nitrogen physisorption analysis for the three different rGO and their respective catalysts.

| Sample        | BET specific surface area [m <sup>2</sup> g <sup>-1</sup> ] | Adsorption pore volume [cm <sup>3</sup> g <sup>-1</sup> ] | Micropore area [m <sup>2</sup> g <sup>-1</sup> ] | Adsorption average pore size [nm] | Desorption average pore size [nm] |
|---------------|---|---|--|-----------------------------------|-----------------------------------|
| rGON700       | 104.7   | 0.954   | 40.19  | 41.2                              | 6.9                               |
| rGOHN500      | 51.8  | 0.269   | 17.19  | 23.9                              | 9.9                               |
| rGOsonic      | 11.5  | 0.059   | 4.13   | 27.6                              | 19.9                              |
| Fe-N/rGON700  | 34.1  | 0.247   | 0.27   | 27.3                              | 19.9                              |
| Fe-N/rGOHN500 | 5.8   | 0.037   | 0.68   | 37.7                              | 28.9                              |
| Fe-N/rGOsonic | 32.1  | 0.052   | 8.75   | 9.0                               | 7.1                               |

The rGO supports N<sub>2</sub> adsorption-desorption isotherms (Fig. 1A) exhibit a type II isotherm with a type H3-H4 hysteresis loop according to the International Union of Pure and Applied Chemistry (IUPAC) classification [34]. The type II shape is normally associated with a non-porous or macroporous materials, while the hysteresis appearing in the multilayer range of physisorption isotherms is usually associated with capillary condensation in mesopore structures. This is confirmed by pore size distribution analysis (Fig. 1B) which shows that these materials are mainly meso- and macroporous. During the catalysts synthesis process, the rGO supports exfoliated by thermal annealing (rGON700 and rGOHN500) undergo a significant surface area decrease (see Table 1). This could be due to the incorporation of new carbon coming from the TPTZ molecule, which graphitized during the pyrolysis treatment [11]. A further reason could be the agglomeration of the graphene nanosheets, adhering to each other during the thermal treatment at 800°C, causing a surface area decrease. In fact, as reported in the literature, during the thermal treatment the rGO sheets could adhere to each other causing a reduction of the sample's specific surface area [35–37]. On the contrary, the catalyst supported on rGOsonic undergoes a surface area increase in comparison to its respective rGO support. This behavior could be ascribed to a further exfoliation-reduction of the rGO support during the pyrolysis at 800°C. The rGOsonic, in facts, did not undergo a previous thermal annealing exfoliation, and its initial surface area was significantly lower in comparison with rGON700 and rGOHN500, probably due to the lower reduction and the consequent lower level of exfoliation.

Regarding the Fe-N/rGO catalysts, their N<sub>2</sub> adsorption-desorption isotherms (Fig. 1C) exhibit a type II shape [34]. The hysteresis loop shape is of type III for Fe-N/rGON700 and Fe-N/rGOHN500. This is usually observed with aggregates of plate-like particles giving rise to slit-shaped pores. The Fe-N/rGOHN500 loop is almost imperceptible, indicating lower amount of mesopores, as also evidenced

in Fig. 1D. The hysteresis loop shape for Fe-N/rGOsonic is more similar to type IV, suggesting the presence of narrow slit-like pores, but associated with a higher microporosity content, as also evidenced in Table 1. The surface area values are comparable to values found in the literature for rGO [11,36,37].

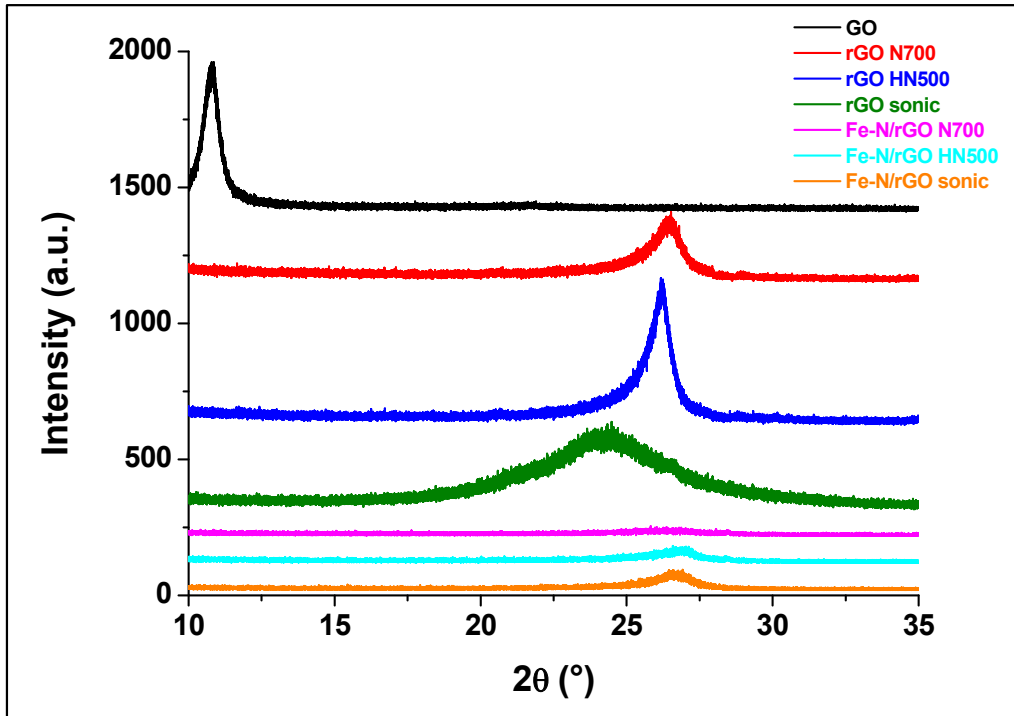


**Fig. 1** Nitrogen adsorption – desorption isotherms of the rGO (A) and the Fe-N/rGO catalysts (B). Pore size distribution of the rGO (C) and the Fe-N/rGO catalysts (D).

### 3.1.2. XRD analysis

The XRD spectra of GO, rGO supports and their respective Fe-N/rGO catalysts were recorded in order to evidence the structural changes occurring during the conversion of graphite first to GO, then to rGO through the different reduction-exfoliation methods, and finally to Fe-N/rGO catalysts. They are shown in Fig. 2.

For all of the samples, the spectra were recorded in the  $2\theta$  range 10 – 100 °. However, for all of the samples, only one peak attributable to the (002) plane of the graphitic structure was detected. Therefore, in Fig. 2, the  $2\theta$  range was restricted in the  $2\theta$  range from 10 – 35°.



**Fig. 2** XRD spectra of graphite oxide (GO), reduced graphene oxides (rGO), and Fe–N/rGO catalysts.

From the literature it is known that graphite has an intense sharp peak at  $2\theta = 26.5^\circ$  corresponding to the (002) reflection plane (JCPDS 01-0640) [30,38]. After having been oxidized to GO, the peak appears to be considerably shifted to a lower  $2\theta$  angle of  $10.8^\circ$  (see Fig. 2). Similar values are reported in the literature for GO prepared with Hummers method [11,26,36,38,39]. This shift is caused by the intercalation of oxygen containing groups which form during the strong oxidation with  $\text{KMnO}_4$ . A peak shift to lower  $2\theta$  values means an increase in the interlayer spacing  $d$ , which is proportional to  $1/\sin(\theta)$ , according to the Bragg's law. After the reduction-exfoliation processes the sharp peak at  $2\theta = 10.8^\circ$  disappears, and a broader peak appears at higher  $2\theta$  values. For rGON700, rGOHN500 and rGOsonic the peak maximum is at  $2\theta = 26.35^\circ$ ,  $26.17^\circ$ , and  $24.3^\circ$ , respectively. These shifts are due to the removal of the oxygen-containing groups occurred during the reduction-exfoliation processes. The different peak maximum position, broadening and intensity indicate that the three different processes lead to obtain reduced graphene oxides with substantially different characteristics. In particular, the lower the peak shift to  $2\theta$  angles lower than  $26.5^\circ$ , the lower is the amount of residual oxygenated groups between layers. This suggests that the exfoliation-reduction under  $\text{N}_2$  atmosphere at  $700^\circ\text{C}$  is the most efficient process for oxygen removal (see also SEM-EDX analysis). The peak broadening, that can be measured as the Full-Width at Half-Maximum (FWHM), is an indication of lower graphitic domains size, with loss of the long-range order in graphene sheets [26,40]. The intensity of the peak is related to the volume fraction of crystalline phase in the material, meaning in this case a higher content of well-stacked graphene layers [40]. From Fig. 2 it can be deduced that



rGOsonic is the rGO with the higher amount of oxygen still present (higher shift to lower  $2\theta$  angles), but it is also the more homogeneously exfoliated one (higher peak broadening). rGON700 and rGOHN500 exhibit almost the same peak broadening, with the latter peak being more intense than the former one, suggesting a lower effectiveness of the thermal annealing under  $H_2-N_2$  atmosphere at  $500^\circ C$ . A similar result was also found by Kaniyoor et al. [26]. This difference between the two annealing processes should thus be due to the temperature effect. Increasing the temperature at  $700^\circ C$  seems to be favorable for the evolution of a higher amount of oxygen-containing gases between the layers with consequent better exfoliation.

Concerning the three Fe-N/rGO catalysts, it is evident how the intensity of the (002) graphite peak at  $2\theta = 25^\circ - 26^\circ$  is considerably decreased. This suggests the formation of a more disordered structure during the catalyst synthesis process. This phenomenon can be due to both the incorporation of C and N coming from TPTZ molecule, and to further de-stacking of graphene ordered layers occurring during the pyrolysis treatment at  $800^\circ C$ . However, there are some differences between the three samples. In particular the peak almost disappeared for Fe-N/rGON700. For Fe-N/rGOHN500 a small peak is still present, but less shifted away from  $26.5^\circ$  than for the respective rGO support, suggesting a further decrease in O content (as confirmed by EDX and XPS analyses). The same considerations can be made for Fe-N/rGOsonic.

More intense peaks are observed for samples having higher N and Fe content [39,41] (see XPS analysis, Table 3), sign that Fe most likely favors the nitrogen fixation [11,39].

Peaks related with Fe containing crystallites, as metallic Fe or Fe oxides, carbides and nitrides were not detected, suggesting that these compounds have been effectively removed by the acid washing treatment with 1 M HCl, or that their presence is below the detection range of the X-ray diffractometer.

### 3.1.3. EDX analysis

EDX analysis of GO and rGO confirms that the three different exfoliation-reduction methods lead to obtain rGO with different characteristics, as discussed before. The results are summarized in Table 2.

**Table 2.** Elemental composition by EDX for GO and the rGO obtained with the three different methods.

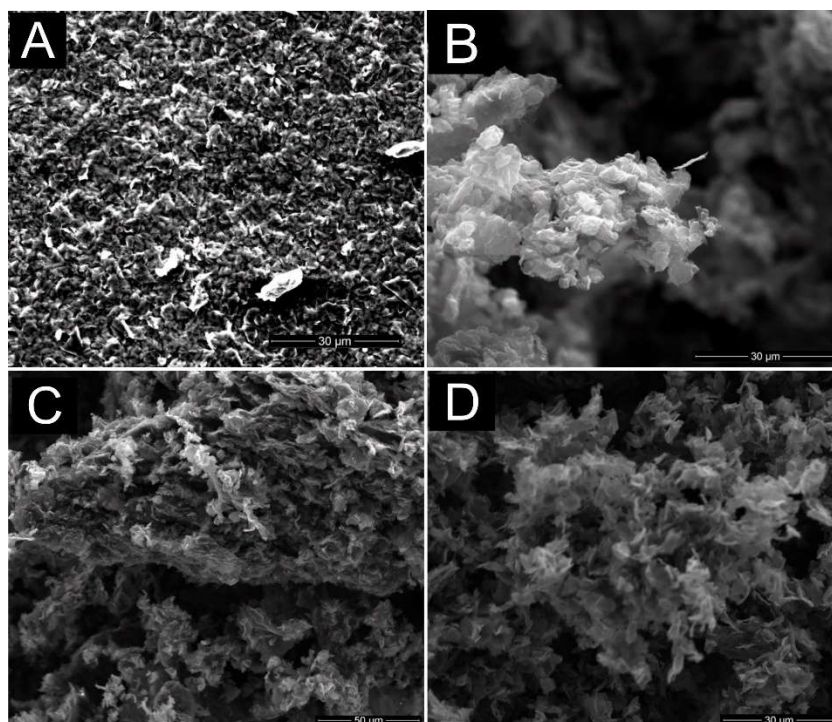
| Sample   | Total C<br>[atomic %] | Total O<br>[atomic %] | C/O atomic ratio |
|----------|-----------------------|-----------------------|------------------|
| GO       | 60.7                  | 39.3                  | 1.54             |
| rGON700  | 94.4                  | 5.6                   | 16.86            |
| rGOHN500 | 92.6                  | 7.4                   | 12.51            |
| rGOsonic | 89.6                  | 10.4                  | 8.62             |

The C/O atomic ratio for GO is 1.54, confirming the high effectiveness in graphite oxidation of the Hummers method. Similar values can be found in the literature [26,42,43]. The oxygen content increase in the order rGON700 < rGOHN500 < rGOsonic, confirming the results of XRD and BET-porosimetry analyses about the oxygenated functional groups content, and the exfoliation degree. Therefore, the best method in order to obtain a well-exfoliated and low oxygen-containing rGO is the thermal annealing at 700°C under N<sub>2</sub>.

EDX analysis was also performed on the Fe–N/rGO catalysts after the acid washing. The measured C, O and Fe atomic percentages are shown in Table 3. Fe contents vary between 0.7 and 1.0 atomic %, which correspond to wt. % between 3.1 and 4.4. This well matches with the Fe content designed during the synthesis process (5 wt. %).

#### 3.1.4. SEM pictures

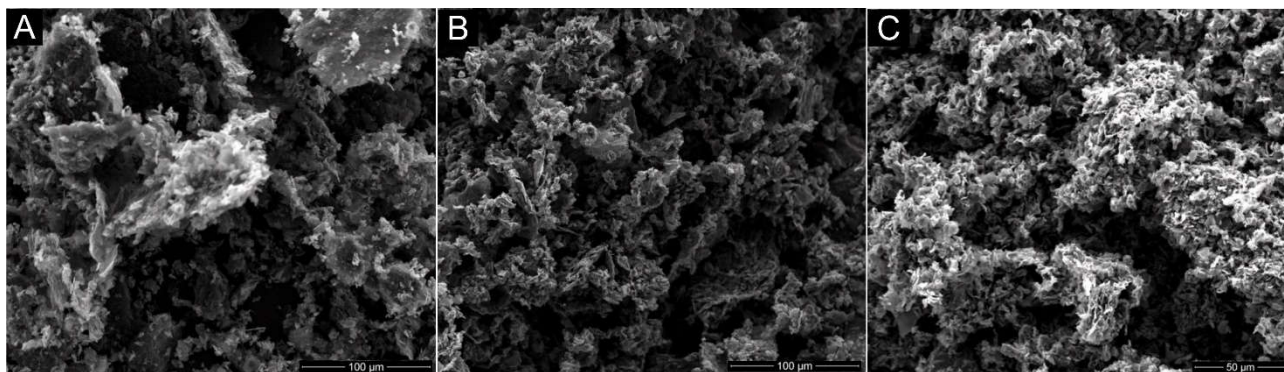
The morphology of GO, rGO supports and Fe–N/rGO catalysts was investigated by SEM. Fig. 3A shows the surface of a GO platelet. Corrugations could indicate that oxygen insertion occurred between the layers, which still appear well stacked, since exfoliation has not occurred yet. Fig. 3B, 3C and 3D show rGON700, rGOHN500 and rGOsonic, respectively. The morphology of the three different samples appears to be considerably different, confirming what found by N<sub>2</sub> adsorption and XRD analyses. In all the three samples planar structures attributable to graphene sheets are visible [11,26,44].



**Fig. 3** SEM pictures of GO (A), rGON700 (B), rGOHN500 (C) and rGOsonic (D)

In particular, in rGON700 the sheets appear to be smoother and less stacked, suggesting a better exfoliation. This could be related to the lower oxidation degree and the higher surface area of this sample. On the contrary, for rGOHN500, the sheets have a more wrinkled aspect (suggesting higher oxidation) and their exfoliation seems to be worse, being more sheets still almost stacked (confirmed by XRD). In fact, the unfolding process of rGO sheets with increasing temperature may be attributed to breaking the conjunction of interlayer and bonds between functional groups and the basal plane due to the removal of oxygen functional groups [45]. For rGOsonic the sheets are even more wrinkled, but with a lower presence of agglomerates, confirming the lower size of the stacked layers domains as evidenced by XRD analysis.

The morphology of Fe-N/rGON700, Fe-N/rGOHN500 and Fe-N/rGOsonic is shown in Fig. 4A, 4B and 4C, respectively. The graphene layers structure is partially still visible [37,44]. However, it can be noticed that the original morphology of the rGO supports appears to be modified due to the catalyst synthesis process, where the incorporation of N, Fe and further C takes place. In particular, for Fe-N/rGON700 and Fe-N/rGOHN500, the graphene layers seem to have suffered some re-stacking in comparison with their respective rGO supports. This further confirms the results of XRD and N<sub>2</sub> adsorption tests.



**Fig. 4** SEM pictures of Fe-N/rGON700 (A), Fe-N/rGOHN500 (B), Fe-N/rGOsonic (C).

### 3.1.5. XPS analysis

XPS analysis was performed for the three catalysts after the acid washing treatment to determine the surface chemical composition, and to detect the presence of N. The survey XPS scan spectra (Fig. 5A, 5B and 5C) reveal the presence of C, O, N and Fe on the catalysts' surface. More in detail, the intense C 1s peak is centered at 284.5 eV. The peak at 532 eV is attributed to oxygen (O 1s) and the peak at 400 eV is the nitrogen peak (N 1s). The peak at 712 eV can be assigned to Fe 2p. However, for all the three catalysts, the signal of the Fe 2p peaks are too weak to allow the determination of the Fe valence state via deconvolution of the high-resolution peak analysis. The catalysts total surface elemental compositions resulting from XPS analysis are summarized in Table 3. The three different catalysts have different surface N, O and Fe contents, in spite of having been undergone to the same synthesis process, suggesting that the rGO support characteristics play an important role in N and Fe fixation. In addition, in Table 3, the Fe-N/rGO catalysts elemental composition resulting from EDX analysis is shown. A comparison can be made, taking into account the differences between these two instrumental methods. XPS is a surface sensitive technique (the depth of the analysis being about 5–6 nm) [46], while EDX has a higher probe depth ( $\geq 1$  mm), which makes possible to consider the results of this analysis as bulk composition [47]. Thus, the comparison between the Fe content obtained from XPS and from EDX analysis suggests that for Fe-N/rGON700 and Fe-N/rGOsonic only a small part (0.1 and 0.2 atomic %, respectively) of the total Fe (0.7 atomic % for both catalysts) is predominantly situated on the surface, being the rest situated deeper in the porous structure of the catalyst. On the contrary, for Fe-N/rGOHN500, the Fe amount detected by the two different techniques is the same. This result could be explained with the considerably lower surface area of this sample in comparison with the previous (see Table 1), resulting in more Fe quantity situated on the catalyst surface.

**Table 3.** Elemental composition by EDX (bulk composition) and XPS (surface composition) for the Fe-N/rGO catalysts.

| Sample         |     | Total C<br>[at%] | Total O<br>[at%] | Total Fe<br>[at%] | Total N<br>[at%] |
|----------------|-----|------------------|------------------|-------------------|------------------|
| Fe-N/rGON700   | EDX | 94.8             | 4.5              | 0.7               | -                |
|                | XPS | 94.6             | 3.0              | 0.1               | 2.3              |
| Fe-N/rGOHN500  | EDX | 95.1             | 3.9              | 1.0               | -                |
|                | XPS | 87.4             | 5.4              | 1.0               | 5.9              |
| Fe-N/ rGOsonic | EDX | 96.1             | 3.2              | 0.7               | -                |
|                | XPS | 89.4             | 6.3              | 0.2               | 4.1              |

The high-resolution C1s spectra are shown for the three catalysts in Fig. 5D-E-F. All of the deconvolutions show three components. The relative percent quantities of each component are summarized in Table 4. The sharp peak at 284.5 eV corresponds to graphitic-like carbon (sp<sup>2</sup> ibridization). The peak at 285.0 – 285.5 eV could be assigned to a combination of signals due to carbon with sp<sup>3</sup> ibridization and C=N bond (N-C sp<sup>2</sup> type) [25,48–50]. The broad peak at higher binding energy values can be attributed to C-N bound (N-C sp<sup>3</sup> type) and to different C-O bonds (C-O-C; O-C=O and HO-C=O) [25,48–52].

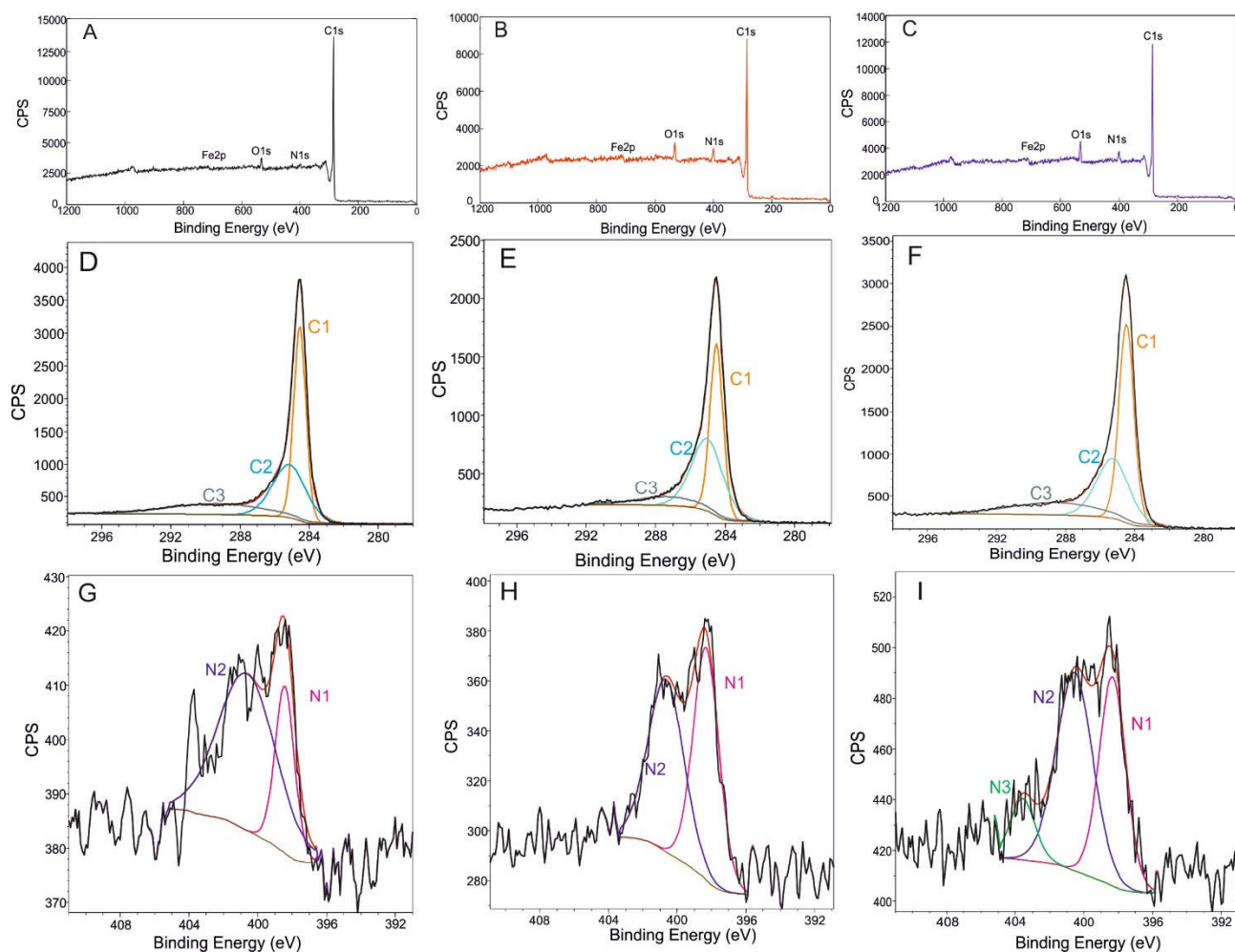
The high-resolution N 1s spectra of Fe-N/rGO catalysts are fitted in three different components (see Fig. 5G-H-I) and their relative amounts are shown in Table 4. The first component, with peak maximum at 398.4 eV is attributed to pyridinic-type N and/or to N coordinated with a metal atom (Fe-N<sub>x</sub> moieties). The second peak, with maximum at 400.6 eV is assigned to graphitic-type N and/or pyrrolic type N. The third component, which exhibits a maximum at 403.6 eV and is detected only for Fe-N/rGO sonic, can be related to the presence of N oxidized functional groups [11,53–57]. Fe-N/rGON700 is the sample that has the lower relative content of pyridinic-N and Fe-coordinated N. Moreover it is also the sample with the lower total N and Fe content (see Table 3). As can be found in the literature, pyridinic-N is usually situated in micropores [9,58,59], which are less abundant in Fe-N/rGON700 (see Table 1). These facts could explain the lower pyridinic-N and Fe-N<sub>x</sub> content for this catalyst. Fe-N/rGOHN500 and Fe-N/rGOsonic have almost identical graphitic-pyrrolic N content (around 50%). Fe-N/rGOsonic has also a certain quantity of oxidized-N. On the contrary, the other two catalysts do not exhibit oxidized-N bonds in appreciable quantity. This could be related to the higher surface O content of Fe-N/rGOsonic catalyst.

**Table 4.** Nitrogen and carbon contents with relative intensities and binding energies of N 1s (N1: pyridinic N and/or Fe-N<sub>x</sub>; N2: pyrrolic and/or graphitic N; N3: oxidized N) and C 1s (C1: graphitic C; C2: C-C sp<sup>3</sup> and/or C=N sp<sup>2</sup>; C3: C-N sp<sup>3</sup> and/or oxidized C) peaks from XPS analysis of the Fe-N/rGO catalysts.

| Sample        | N 1s                     |                          |                          | C 1s                     |                          |                          |
|---------------|--------------------------|--------------------------|--------------------------|--------------------------|--------------------------|--------------------------|
|               | N1 [at. %]<br>(B.E [eV]) | N2 [at. %]<br>(B.E [eV]) | N3 [at. %]<br>(B.E [eV]) | C1 [at. %]<br>(B.E [eV]) | C2 [at. %]<br>(B.E [eV]) | C3 [at. %]<br>(B.E [eV]) |
| Fe-N/rGON700  | 26.2<br>(398.4)          | 73.8<br>(400.6)          | n.d.<br>-                | 45.7<br>(284.5)          | 34.5<br>(285.1)          | 19.8<br>(289.3)          |
| Fe-N/rGOHN500 | 49.4<br>(398.3)          | 50.6<br>(400.6)          | n.d.<br>-                | 43.9<br>(284.5)          | 44.9<br>(285.0)          | 11.2<br>(287.2)          |
| Fe-N/rGOsonic | 38.9<br>(398.3)          | 50.5<br>(400.5)          | 10.6<br>(403.6)          | 49.0<br>(284.5)          | 32.5<br>(285.3)          | 18.5<br>(288.5)          |

Therefore, the amount of nitrogen incorporated, as well as the abundance of the different nitrogen species created during the catalysts synthesis process, is significantly influenced by the nature of the starting rGO support. Regarding the relative content of the different N bound types, the amounts found in our samples are comparable to the values found in the literature for similar rGO-supported catalysts doped with N and Fe [11,56]. Nitrogen doping occurring during a heat treatment at T between 700 and 1000 °C in presence of a transition metal ion, is essential to significantly increase the catalytic activity of carbon-based materials [9]. However, neither the exact structure of the active sites, nor the role of the transition metal in them have been clearly identified yet [8].

In fact, no direct relation was found between total N and Fe content and catalyst electroactivity towards ORR. The same conclusion can be done restricting the analysis to the different nitrogen types. This means that even if nitrogen atoms are known to be part of active sites, their amount is not the limiting factor for the ORR electroactivity [55].



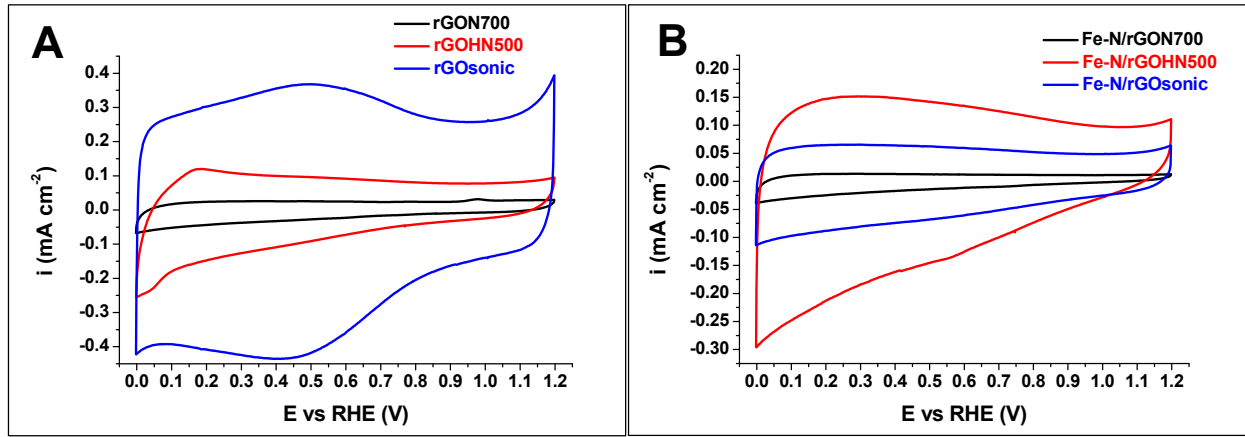
**Fig. 5** XPS survey spectra of Fe-N/rGON700 (A), Fe-N/rGOHN500 (B), and Fe-N/rGOsonic (C). Deconvolution of the high resolution XPS spectra of C 1s for Fe-N/rGON700 (D), Fe-N/rGOHN500 (E), and Fe-N/rGOsonic (F). Deconvolution of the high resolution XPS spectra of N 1s for Fe-N/rGON700 (G), Fe-N/rGOHN500 (H), and Fe-N/rGOsonic (I). The different C 1s and N 1s peaks are defined in Table 4.

### 3.2. Electrochemical characterization

#### 3.2.1. Cyclic voltammetries in $N_2$ -saturated electrolyte.

Cyclic voltammetries were recorded in 0.1 M KOH solution saturated with inert gas ( $N_2$ ) for the rGO supports (Fig. 6A) and their respective Fe-N/rGO catalysts (Fig. 6B).





**Fig. 6** CV recorded at 10 mV s<sup>-1</sup> scan rate in N<sub>2</sub>-saturated 0.1 M KOH for rGO supports (A) and Fe-N/rGO catalysts (B).

Then, starting from these capacitive current densities values, the average specific capacitance per mass of catalyst ( $C_m$ ) was calculated by using the following equation [55]:

$$C_m = \frac{\int_{E_2}^{E_1} i_{cap} dE}{2v(E_2 - E_1)m_c} \quad (1)$$

where  $i_{cap}$  is the capacitive current density,  $E$  is the potential,  $v$  is scan rate,  $E_1$  and  $E_2$  are the extremes of the scanned potential range and  $m_c$  is the catalyst loading. For rGO supports the as calculated capacitance values are summarized in Table 5. It can be noticed that the specific capacitance is greater for the samples which exhibit a lower C/O ratio. This means that capacitance is strictly related with surface oxidation and more generally, with surface functionalization, as reported in several works [60–63]. In the case of rGO supports, since no other elements than C and O are detected by the EDX, the surface functionalization could be totally ascribed to oxygen-containing functional groups still present due to the only partial progress of the reduction-exfoliation processes, as also confirmed by XRD analysis.

Generally, the enhancement of specific capacitance for carbon materials can be realized by special oxidation of carbon for increasing the surface functionality (e.g. through chemical treatment or electro-chemical polarization) [63]. The capacitive current phenomena on this type of carbonaceous materials could be influenced by different factors: pore geometry, pore size distribution, electrical conductivity, wettability, and presence of surface electroactive species [61,63]. Pseudo-capacitance effect of surface redox-sites must also be considered. Pseudo-capacitance at the carbon surface can be due to chemisorption phenomena with partial charge transfer, or to redox processes (e.g. involving quinone-hydroquinone functional groups). These pseudo-capacitance effects related with faradic



reactions of surface groups enhance the value of the capacitance [63]. Therefore, the importance of these pseudo-capacitance phenomena seem to be significantly higher than the electrostatic double layer capacitance, which is related to the surface area [11,64]. Theoretically, the higher the specific surface area, the higher the specific capacitance should be. Practically, the situation is more complicated, and carbons with smaller surface area give a larger specific capacitance than those with a larger surface area [63]. However, this could be limited by the surface wettability and accessibility. An important factor, in fact, is the accessibility of micropores to aqueous solution [65].

The specific capacitance values for the Fe-N/rGO catalysts are also shown in Table 5. The samples with more surface modification (higher N, O and Fe content) also exhibit higher capacitance. For Fe-N/rGON700 there is a decrease of the capacitance value with respect to rGON700 support of about one half. This could be partly due to the considerable surface area decrease (see Table 1). Concerning Fe-N/rGO, its capacitance slightly increases in comparison with its respective support (rGOHN500). This could be ascribed to the increase of the surface functionalization (Table 2 and 3) calculated as C to other atoms ratio. Fe-N/rGOsonic specific capacitance is considerably lower than for rGOsonic support, and this could probably be caused by further reduction of C-oxidized surface groups (that are still present in great quantity on rGOsonic) during the pyrolysis at 800° C in the catalyst synthesis process.

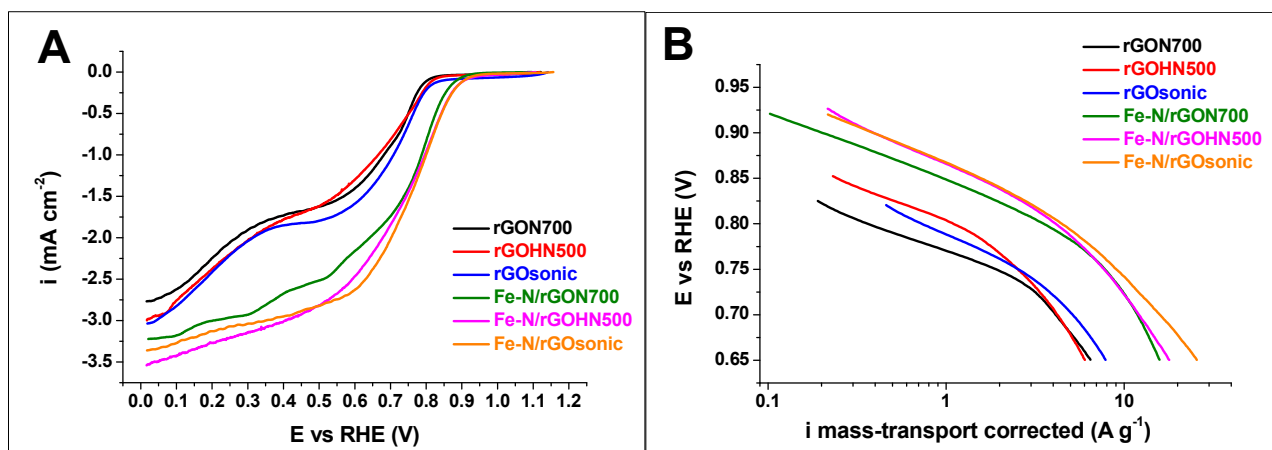
### 3.2.2. ORR electroactivity.

The oxygen reduction activity in alkaline medium was assessed by the RDE technique for the three different types of rGO and their respective Fe-N/rGO electrocatalysts. As evidenced in Fig. 7A, the rGO have a not negligible activity towards ORR. This is due to the fact that in alkaline medium, carbon materials themselves are effective catalysts for the reduction of O<sub>2</sub> to peroxide [66]. The ORR activity of the electrocatalysts is highly enhanced in comparison with the rGO supports. Observing the LSV recorded in RDE test (Fig. 7A), it is evident how both the ORR onset potential (defined as the potential at which a current density of 0.1 mA cm<sup>-2</sup> is generated [67]) and the half-wave potential of the Fe-N/rGO catalysts are between 100 and 150 mV higher than for their respective rGO supports. This electroactivity increase is due to the incorporation of N and Fe in the rGO carbon structure during the heat treatment at high temperature. In the linear sweep voltammetries of the three rGO (see Fig. 7A) there is no any trace of well-developed diffusion limited plateau current zone, sign that the current density at high overpotential values is still in a mixed kinetic and mass- or charge-transport limited zone [68]. The values of the limiting current densities range can be assumed to be in the range between -2.76 and -3.03 mA cm<sup>-2</sup>.

Otherwise, for the Fe-N/rGO catalysts, the linear sweep voltammetry shape at high overpotentials is less inclined, even if also in this case there is no well-developed diffusion limited zone. The limiting current densities are higher than for rGO supports, and range between -3.25 and -3.55 mA cm<sup>-2</sup>. These limiting current densities values were used to calculate the mass-transport corrected ORR electro-reduction kinetic activity by equation (2):

$$i_k = -\frac{i_L \cdot i}{i_L - i} \quad (2)$$

where  $i_k$  is mass transport-corrected current density,  $i$  is the current density, and  $i_L$  is the limiting current density. A correction for the ohmic drop was also done, based on the resistance values obtained by the impedance measurements as described in the experimental section. The as-calculated  $i_k$  values can be transformed in specific mass current densities (A g<sup>-1</sup>), simply dividing by the catalyst loading on the electrode (mg cm<sup>-2</sup>). The potential vs logarithm of specific mass current density plot for the rGO and the Fe-N/rGO catalysts are shown in Fig. 7B. The ORR mass activity values (A per g of catalyst) at 0.9 and 0.8 v vs RHE for Fe-N/rGO catalysts and at 0.8 V vs RHE for rGO supports are shown in Table 5.



**Fig. 7** LSV recorded in O<sub>2</sub>-saturated 0.1 M KOH solution at a rotational speed of 900 rpm and potential scan rate of 5 mV s<sup>-1</sup> (A). Tafel plot after mass-transport limitation correction (B).

The portion of the curves at low overpotentials has a linear trend (Tafel behavior), and allows the calculation of two kinetic parameters: the exchange current density ( $i_0$ ) and the cathodic transfer coefficient ( $\alpha_c$ ), according to the Tafel equation [2,69–71]:

$$E = E_0 + \frac{2.303RT}{\alpha_c F} \log i_0 - \frac{2.303RT}{\alpha_c F} \log i \quad (3)$$

where  $E$  is the electrode potential,  $E_0$  is the thermodynamic electrode potential of the ORR (1.23 V vs SHE),  $R$  is the universal gas constant ( $8.314 \text{ J mol}^{-1} \text{ K}^{-1}$ ),  $T$  is the working temperature (K),  $F$  is the Faraday constant ( $96487 \text{ C mol}^{-1}$ ),  $\alpha_c$  is the cathodic transfer coefficient [69],  $i_0$  is the exchange current density, and  $i$  is the measured current density.

As can be seen from Fig. 7B, the Tafel behavior zone is in the range 0.92 – 0.84 V vs RHE for Fe-N/rGO catalysts and 0.85 – 0.75 v vs RHE for rGO supports.

According to Eq. (3), after having determined the slope ( $2.303RT / \alpha_c F$ ) and the intercept ( $E_0 + (2.303RT / \alpha_c F) \log(i_0)$ ) from the plot of  $E$  versus  $\log(i)$ , both the  $\alpha_c$  and  $i_0$  values were calculated, and their values are shown in Table 5.

**Table 5.** Some electrochemical parameters calculated from the RDE half-cell test results

| Sample         | Specific capacitance<br>[F g <sup>-1</sup> ] | activity at 0.9 V<br>[A g <sup>-1</sup> ] | activity at 0.8 V<br>[A g <sup>-1</sup> ] | Tafel slope<br>[mV dec <sup>-1</sup> ] | $\alpha_c$ | $i_0$<br>[mAcm <sup>-2</sup> ] | Onset E<br>[mV] | Half-wave E<br>[mV] |
|----------------|--|---|---|--|------------|--------------------------------|-----------------|---------------------|
| rGON700        | 7.5  | -   | 0.362                                     | 67.8                                   | 0.873      | $5.24 \cdot 10^{-8}$           | 804             | 605                 |
| rGOHN500       | 26.2   | -   | 0.969                                     | 72.2                                   | 0.820      | $4.01 \cdot 10^{-7}$           | 819             | 545                 |
| rGOsonic       | 94.3   | -   | 0.666                                     | 87.4                                   | 0.677      | $2.82 \cdot 10^{-6}$           | 848             | 619                 |
| Fe-N/rGON700   | 3.8  | 0.196                                     | 3.521                                     | 75.0                                   | 0.789      | $2.57 \cdot 10^{-6}$           | 885             | 721                 |
| Fe-N/rGOHN500  | 38.1   | 0.384                                     | 4.116                                     | 86.5                                   | 0.684      | $1.94 \cdot 10^{-5}$           | 907             | 710                 |
| Fe-N/ rGOsonic | 17.9   | 0.390                                     | 4.465                                     | 81.6                                   | 0.725      | $1.12 \cdot 10^{-5}$           | 906             | 737                 |

The higher current density values obtained for the Fe-N/rGO catalysts in comparison with their respective rGO supports are a confirmation of the increasing of the catalytic performance of these rGO-based materials due to the heat treatment in presence of Fe and N sources. The activity increase could be a combination of different factors. In particular, N content and micropore content are more important than the overall surface area. In fact, in spite of its lower overall surface area in comparison to Fe-N/rGON700, Fe-N/rGOHN500 has a higher electroactivity. This could be related to its higher microporous surface area and very much higher N content. Otherwise, in comparison with Fe-N/rGOsonic, the Fe-N/rGOHN500 activity is slightly lower. This could be a consequence of the very much higher microporous area of the former, which otherwise has a lower N content. Micropores, in fact, are found to be closely related with the electrocatalytic activity of NPMC. Jaouen et al. [55,58,59] suggest that the distance between two pore walls must have an exact value for an active site to be formed in these types of NPMC.

Concerning cathodic transfer coefficient ( $\alpha_c$ ), all of the found values are in the range 0.6 – 0.9. This is in accordance to the values found in the literature for similar C-based materials and Me-N-C catalysts in alkaline conditions [72–75].

#### 4. Conclusions

Starting from GO, by means of three different reduction/exfoliation methods we obtained rGO samples with different characteristics, as demonstrated by physicochemical and electrochemical characterizations. Annealing at 700°C in N<sub>2</sub> lead to obtain a better exfoliated rGO. This is also the more suitable method to obtain a better reduction (higher C/O ratio). The rGO themselves have a certain electroactivity towards the ORR in alkaline conditions. However, to improve this activity, Fe-N/rGO catalysts were synthesized by doping the rGO surface using a Fe-complex with the N-containing ligand molecule TPTZ, by wet impregnation and a subsequent pyrolysis at 800°C.

Different behaviors of catalysts synthesized in the same way but starting from different rGO supports were obtained, showing different electroactivities and physicochemical properties as overall and microporous surface area and nitrogen content. The electroactivity increase is a consequence of the combination of these properties, as well as the carbon support characteristics. In particular, the importance of the starting rGO support characteristics on the final properties of the Fe-N/rGO catalyst are pointed out.

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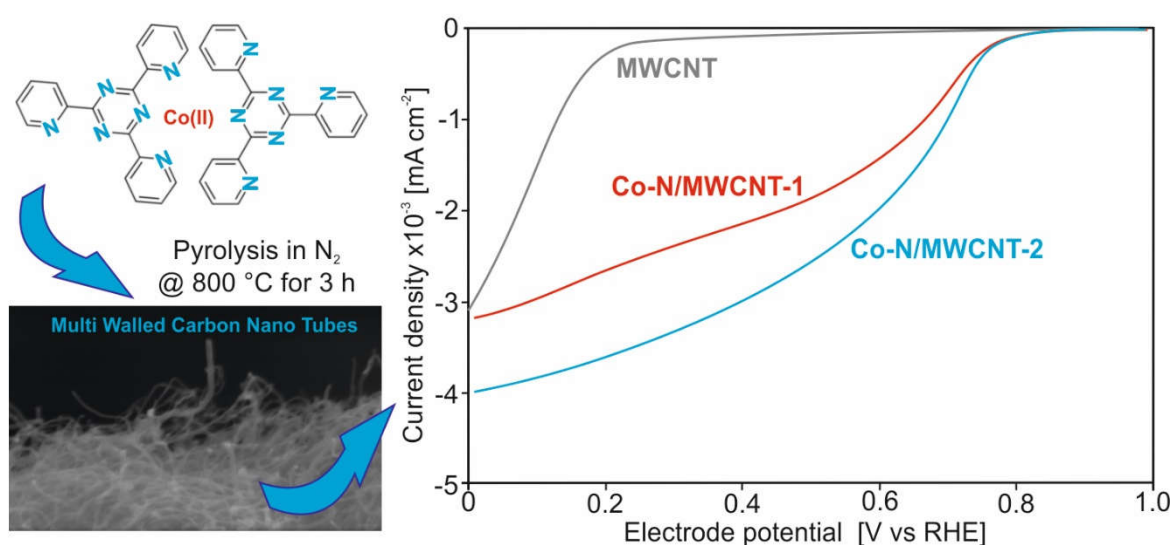
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## CHAPTER 3. Activity of Co-N multi walled carbon nanotubes electrocatalysts for oxygen reduction reaction in acid conditions.

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### 1. Introduction

The use of platinum as preferred catalyst in PEM fuel cells anode and cathode is one of the bottlenecks to the widespread commercialization of these devices, because of the high cost and scarcity of platinum [1,2]. To overcome this problem, extensive research has been carried out to reduce the Pt catalyst usage, to improve catalyst utilization, and to identify alternative non-noble metal catalysts with similar catalytic activity [3]. On the cathode of the fuel cell, the sluggish reaction kinetics for the oxygen reduction reaction (ORR) leads to great overpotentials and therefore to low conversion efficiency. This has stimulated research toward alternative non-precious metal based materials as ORR electrocatalysts [4].

Transition metal (mainly Fe and Co) macrocycles like porphyrins and phthalocyanines have been investigated as a potential ORR catalysts since the early 1960s [5,6]. More recently, several types of carbon materials functionalized with nitrogen and transition metals have also been investigated as non-precious metal catalysts (NPMC). Many synthesis strategies can be adopted for the preparation of NPMC supported on carbon-based materials [7–12]. For example, a carbon support with a high specific surface area can be impregnated with a complex formed between a N-containing ligand

molecule like TPTZ (2,4,6-tris(2-pyridyl)-1,3,5-triazine) or 1,10-phenanthroline, and a transition metal ion (i.e., Fe, Co) [12–14], as precursor molecule for the formation of the ORR active sites [4]. According to the literature, in these NPMC the active site is formed during a heat-treatment at 500–1000 °C if transition metal ions (Fe, Co, etc.), a source of carbon (carbon support, polymer) and a source of nitrogen (N-containing molecule, polymer or gas) are simultaneously present. Nitrogen, in fact, is a necessary component to form an active site for ORR in these catalysts [15–18].

Despite many years of research on non-noble metal electrocatalysts for ORR in acidic medium, the role of transition metals (Fe, Co) is still controversial, and therefore the exact ORR active site has not been exactly identified so far. Some scientists believe that the metal is an integral and electrochemically active part of the catalytic site, while others believe that it is merely a chemical catalyst for the formation of special oxygen reducing N-doped carbon structures [19]. In particular, three different types of active sites were proposed in the 1980s by van Veen, Yeager, and Wiesener respectively. On the basis of more recent studies, these different active sites could be simultaneously present in transition metal based catalysts active for ORR in acidic medium, but their activity and relative population can vary depending on the choice of the metal and nitrogen precursors, the structural properties of the carbon support, and the synthesis procedure [19].

The kinetics of these M-N/C (M = Fe, Co, etc.) electrodes is around 150–200 mV below that of Pt/C based electrocatalysts. This is partly because M-N/C electrocatalysts have a lower number of active sites per unit volume than Pt/C based electrocatalysts [20]. The activity per unit volume ( $A\text{ cm}^{-3}$ ) at a given potential of these kinds of non-noble metal electrocatalysts could be described as the product of the site density ( $\text{sites cm}^{-3}$ ) and the average turnover frequency (electrons per site per time at the given potential) and the charge of a single electron [16]. After the calculation of the non-precious metal catalysts mass activity ( $A\text{ g}^{-1}$ ), the volumetric activity ( $A\text{ cm}^{-3}$ ) can be calculated by considering the density of the catalyst in the porous cathode [21].

The best activity values of NPMC previously reported in the literature rapidly increased in recent years [16]. An overview of catalysts obtained with different synthesis procedures and their activities as mass-specific current densities ( $A\text{ g}^{-1}$ ) at 0.8 V vs RHE in RDE can be found in the works of Jaouen *et al.* [16] and Cheon *et al.* [22]. These activities range between 0.5 and 20  $A\text{ g}^{-1}$  at 0.8 V vs RHE. An exceptionally high activity of 45  $A\text{ g}^{-1}$  was obtained by Cheon *et al.* [22]. Lower specific mass activities at 0.8 V vs RHE in the range of 0.01 and 0.8  $A\text{ g}^{-1}$  are obtained by other groups [19, 23 – 26]. In some works, activities are calculated at the potential of 0.75 V vs RHE and they range between 0.1 and 2.5  $A\text{ g}^{-1}$  [27,28].

To improve both activity and stability of M-N/C catalysts, a variety of approaches have been explored. These include the optimization of synthesis conditions and procedures, the development of

heat-treatment strategies, the exploration of different carbon supports, and the use of different transition metal complexes with N-containing ligand molecules as precursors [12,23,29].

As carbon support, MWCNT have been studied by several groups [20,24,29–33]. Carbon nanotubes have high electrical conductivity [34]. This can facilitate electron delivery to the active site, making oxygen reduction fast and efficient in any possible active site. Carbon nanotubes also possess good chemical and thermal stability [35]. These properties make MWCNT good candidates to be used as carbon support for fuel cell catalysts preparation. The simultaneous doping of the carbon support with nitrogen and transition metals can be done by using a N-containing ligand molecule that can form a complex in solution with transition metals [12,23,26,29]. TPTZ ligand, which contains six nitrogen atoms per molecule, could provide a sufficient amount of nitrogen for both the N-doping of the carbon and the consequent formation of the ORR catalytic active sites.

In the literature, RDE-RRDE equipment and/or MEA configuration [36,37] are mainly used for the study of both NPMC and Pt-based catalysts ORR activity. Some attempts have been made to try to compare activity results obtained for the same catalyst in RDE and MEA, considering the differences between the two testing approaches [21,37].

In this work, two Co-N catalysts were synthesized by wet impregnation of multi-walled carbon nanotubes (MWCNT) and a complex between Co(II) ions and the N-containing TPTZ molecule, followed by one or two heat treatments. The catalysts were characterized using several instrumental methods for morphology, structure, chemical composition and thermal behavior. The activities towards ORR in acid conditions were measured in rotating disk electrode (RDE) and in a gas-diffusion electrode (GDE) cell. The stability of the as prepared Co-N/MWCNT catalysts was assessed by performing chronoamperometries in both RDE and GDE cell.

RDE tests are suitable to study the ORR in controlled fluid-dynamic conditions according to the classical approach of Levich, whereas GDE tests can be considered closer to the working operation of a fuel cell testing. In the GDE the catalyst is deposited on a gas diffusion layer (GDL) disk whose front is exposed to the electrolyte solution, where the counter and reference electrodes are also immersed. The back of the GDL, on the other hand, is exposed to a gas flow ( $O_2$ , air or  $N_2$ ) that can be adequately regulated and controlled. The GDE slot configuration also allows the insertion of an ionomer membrane layer on the catalyst [38,39].

The RDE measurements can be considered an ex-situ characterization method, which allows a fast screening for the characterization of supported catalysts with respect to their ORR activity [40,41]. If the preparation method of the glassy carbon disk results in a relatively thick and/or porous layer (1–7  $\mu m$ ) with a high ionomer content, film diffusion resistance plays an important role. Such an ionomer film diffusion resistance could strongly hamper the extraction of electrode kinetics from the measured

RDE data [36,42]. Thus, the reliability of RDE measurements could be problematic due to the absence of a real fuel cell operation correlation.

On the other hand, the GDE cell setup can be considered an in-situ characterization method with a behavior which is as close as possible to an actual fuel cell [40]. Here, the synthesized catalysts are used for fabrication of catalyst layers similar to the cathode of a membrane electrode assembly (MEA). The main advantage of the GDE cell, in fact, is the direct supply of gaseous oxygen to the cathode, avoiding losses due to oxygen diffusion through the liquid electrolyte, thus increasing the amount of accessible oxygen [43–46].

## 2. Experimental

### 2.1. Chemicals

2,4,6-tris(2-pyridyl)-1,3,5-triazine (TPTZ,  $\geq 98\%$  purity) and cobalt(II) nitrate hexahydrate ( $\text{Co}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$ ,  $\geq 98\%$  purity) were purchased from Sigma Aldrich and used as received. Concentrated hydrochloric acid (37 wt.%) and sulfuric acid (98 wt.%) were purchased from Sigma Aldrich and Fluka respectively, and used to prepare their respective aqueous solutions. Nitrogen and oxygen gases were purchased in cylinders by SIAD with purity  $\geq 99.999\%$ . Ethanol (99.5% purity) was purchased from Panreac. MWCNT (average length 5  $\mu\text{m}$ , outer diameter 6–9 nm) and Nafion® (5 wt.% hydro-alcoholic solution) were purchased from Sigma Aldrich. All aqueous solutions were prepared using deionized water obtained from a Millipore Milli-Q system with resistivity  $> 18 \text{ M}\Omega \text{ cm}^{-1}$ .

### 2.2. Catalysts synthesis

Commercial multi-walled carbon nanotubes were used as carbon support material to prepare the Co-N/MWCNT catalysts. The synthesis method consists in a wet impregnation followed by one or two subsequent heat treatments.

Typically, an amount of 300 mg of MWCNT was dispersed in 150 mL of a 1:1 vol. deionized water and ethanol solution under ultrasonic bath for 30 minutes (130 W, Soltec 2200 M 3S sonicator), and left stirring for 1 hour. At the same time, 502 mg of TPTZ ligand molecule, used as a nitrogen source, was dissolved in about 300 mL of deionized water, and the pH was adjusted to 1 by addition of 1 M HCl solution under stirring. Then, 58 mg of  $\text{Co}(\text{NO}_3)_2 \cdot 6\text{H}_2\text{O}$  was added to the TPTZ solution, with the immediate formation of a red-colored complex. The Co:TPTZ molar ratio in this complex was of 1:6. The greater quantity of TPTZ in the synthesis should assure a stoichiometric excess of ligand molecule to favor the chemical equilibrium of the Co ion complexation. Moreover, the excess of

TPTZ (and therefore of N atoms) should lead to higher doping level of the MWCNT surface with N atoms, favoring thus the formation of active sites. The solution was left stirring at room temperature for 6 hours and then it was added to the MWCNT dispersion. This mixture was stirred overnight, and therefore the solvent was evaporated by heating, and the recovered powder was grinded in a mortar. The Co:MWCNT mass ratio in this powder was expected to be 0.05.

The first catalyst, named Co-N/MWCNT-1, was heat-treated in a tubular quartz furnace under nitrogen atmosphere ( $\text{N}_2$  gas flux set at  $150 \text{ N mL min}^{-1}$  with a mass flow controller from Bronkhorst, ELFLOW series) with a heating rate of  $5 \text{ }^\circ\text{C min}^{-1}$  until  $800 \text{ }^\circ\text{C}$ , keeping this temperature constant for 3 hours, and then the furnace was switched-off leaving the apparatus cooling down naturally to room temperature.

For the second catalyst, named Co-N/MWCNT-2, this heat treatment was repeated twice in the same conditions, starting again from room temperature.

Before testing, both catalysts were acid-washed in 1 M HCl solution for 3 hours at  $60 \text{ }^\circ\text{C}$  under reflux, to remove any instable or unbounded acid-soluble cobalt, or cobalt oxide moiety [20,23,24]. Afterwards powders were filtered, washed thoroughly with deionized water until pH was 7, and dried overnight at ambient conditions.

### *2.3. Physico-chemical characterization*

Morphology of bare MWCNT and of synthesized catalyst samples were investigated using a field emission scanning electron microscope (FESEM, model JEOL JSM 6700F).

Energy dispersive X-ray spectroscopy (EDX, FEI-Quanta Inspect 200 with EDAX PV 9900 instrument working at 15 kV) was used to determine the average bulk chemical composition of the catalysts.

Nitrogen adsorption isotherms were recorded by an ASAP 2020 Instrument (Micromeritics) at  $-196 \text{ }^\circ\text{C}$ . Before the analysis, all of the samples were placed into the cell and degassed under vacuum for 3 hours at  $150 \text{ }^\circ\text{C}$ . The specific surface area of the samples was calculated using the Brunauer–Emmett–Teller (BET) method within the relative pressure range of 0–1. The pore size distribution was obtained with the Barrett–Joyner–Halenda (BJH) method.

X-ray photoelectron spectroscopy (XPS) was performed to determine the elemental surface composition of the catalysts samples. The analysis was carried out using a Physical Electronics PHI 5000 Versa Probe electron spectrometer system with monochromated Al  $\text{K}\alpha$  X-ray source ( $1486.60 \text{ eV}$ ) run at 15 kV and 1 mA anode current. Survey scans as well as narrow scans (high resolution spectra) were recorded with a spot of 100 nm size. The survey spectra were collected from 0 to 1200 eV. The narrow N1s spectra were collected from 396 to 405 eV, the narrow Co 2p spectra from 765



to 815 eV, and the narrow C1s spectra from 280 to 293 eV. All of the spectra related to the two samples were obtained under identical conditions, with the samples placed in an ultrahigh vacuum chamber at  $2 \cdot 10^{-10}$  mmHg, and calibrated against a value of the C1s binding energy of 284.5 eV. Multipak 9.0 software was used for obtaining semi-quantitative atomic percentage compositions, using Gauss-Lorentz equations with Shirley background.

To determine the crystallographic structure of the bare MWCNT and of the Co-N/MWCNT catalysts, X-ray powder diffraction (XRD) patterns were collected with a X'Pert PRO diffractometer (PANalytical) using a Bragg-Brentano geometry and a Cu K $\alpha$  radiation ( $\lambda=0,15418$  nm). The X'Pert HighScore software (PANalytical) was used to determine the crystallographic phases associated with the peaks that appear in the XRD patterns.

Thermogravimetric analysis (TGA) measurements were carried out using a NETZSCH TG 209 F1 analyzer. The measurements were performed under a continuous flow of N<sub>2</sub> (20 Ncm<sup>3</sup> min<sup>-1</sup>) with a heating rate of 5 °C min<sup>-1</sup> between 25 and 800 °C. The heating rate is the same used in the pyrolysis treatments during the catalysts synthesis.

For Fourier transform infrared spectroscopy (FTIR) measurements, powder samples were mechanically mixed with KBr and pressed, self-supporting wafers are transparent to the IR radiation. IR spectra were collected in air at 2 cm<sup>-1</sup> resolution on a Bruker Equinox 55 FT-IR spectrophotometer, equipped with a MCT (Mercury Cadmium Telluride) detector.

## *2.4. Electrochemical measurements*

### *2.4.1. RDE tests*

In RDE tests, the electrocatalytic activity towards ORR for the two Co-N/MWCNT catalysts was tested in a conventional three-electrodes electrochemical cell configuration. The cell was equipped with a glassy carbon disk working electrode (0.0707 cm<sup>2</sup> geometric area), a Pt helical wire counter electrode, and a saturated calomel (SCE) reference electrode. All of the electrode potentials were corrected and referred to the reversible hydrogen electrode (RHE).

Cyclic voltammetries (CV) and linear sweep voltammetries (LSV) were performed using a rotating disk electrode equipment (RRDE-3A ALS) and a multi-potentiostat (Bio-Logic SP-150).

The catalyst ink was prepared by mixing 15 mg of catalyst powder with 65  $\mu$ L of Nafion® 5% wt. solution and 600  $\mu$ L of ethanol under sonication for 1 hour to achieve a good dispersion. 3  $\mu$ L of ink was taken with a micro-pipette and deposited on the working electrode, resulting in a catalyst loading of 65  $\mu$ g which corresponds to 0.95 mg cm<sup>-2</sup> referred to the geometrical area of the working electrode. All of the current densities were thus normalized per geometric area of the electrode.

The electrolyte was a 0.5 M H<sub>2</sub>SO<sub>4</sub> aqueous solution saturated with either N<sub>2</sub> or O<sub>2</sub> by direct gas bubbling into the solution. The flux was carefully controlled and maintained constant through a mass flow controller (Bronkhorst, ELFLOW series) fixed at 4.5 mL min<sup>-1</sup>, considering a constant volume of 80 mL of solution.

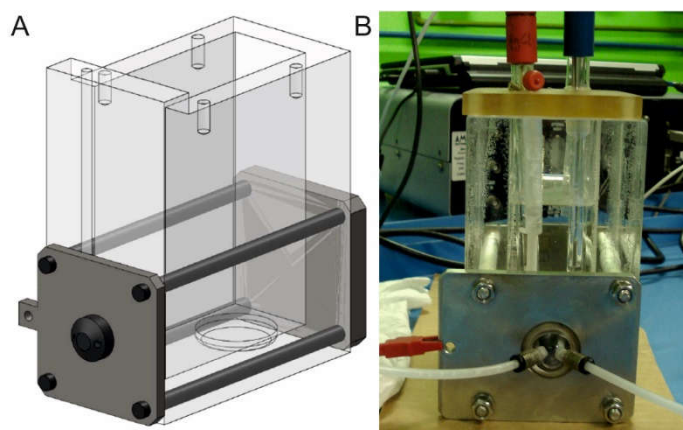
Prior to start tests, to electrochemically clean the working electrode, 80 CV cycles were performed from 0.0 to 1.2 V vs RHE in N<sub>2</sub> saturated electrolyte at 100 mV s<sup>-1</sup> scan rate.

For each catalyst, cyclic voltammograms were recorded between 0.0 and 1.2 V vs RHE in N<sub>2</sub>-saturated electrolyte at 10 mV s<sup>-1</sup> scan rate to determine the capacitive current contribution. Then, the solution was saturated with O<sub>2</sub>, the RDE rotation speed was set to 1600 rpm, and the LSV were recorded again in the same conditions (at 10 mV s<sup>-1</sup> scan rate). The faradic current densities used to calculate the ORR activity were obtained by subtracting the cathodic sweep scan capacitive currents recorded in N<sub>2</sub>-saturated electrolyte from the cathodic sweep scan currents obtained in O<sub>2</sub>-saturated electrolyte [47]. All of the measurements were performed at room temperature and ambient pressure.

#### 2.4.2. GDE cell tests

The catalysts were tested in a cell equipped with a gas-diffusion working electrode, accessible to gas reactants. The GDE cell consisted in a transparent acrylic box, provided with a cylindrical slot (11 mm diameter) where a small GDL disk can be inserted. The GDE working electrode was kept closed with a metal plate provided with a seal gasket, which was tightened to the plastic structure of the cell by means of four bolts. In the metal plate, a chamber with two small holes connected with sealed plastic tubes allows gas inlet and outlet. This chamber is in contact with the back side of the GDL. Fig. 1 shows a scheme and a picture of the GDE cell. The cell was equipped with a saturated Ag/AgCl reference electrode and a Pt plate counter electrode. The GDE working electrode geometric area was of 0.95 cm<sup>2</sup>. A 0.5 M H<sub>2</sub>SO<sub>4</sub> aqueous solution was used as electrolyte.

For the GDE preparation, 18 cm<sup>2</sup> of a carbon cloth GDL (HT-ELAT from E-TEK, USA) was coated with the catalyst ink by brush deposition to obtain a catalyst loading of 1 mg cm<sup>-2</sup>, referred to the geometrical area of the working electrode. Then a small disk of 11 mm diameter was cut and inserted in the cell. The catalyst ink was prepared by mixing 18 mg of catalyst powder with 618 µL of Nafion® 5% wt. solution, 230 µL of deionized water and 290 µL of ethanol. The ink was kept under sonication for 30 minutes and then under stirring for 1 hour.



**Fig. 1.** Scheme (A) and picture (B) of the GDE cell.

CVs and LSVs were performed using the same multi-potentiostat used for RDE tests. Gaseous  $N_2$  was first fluxed at a flow rate of  $1500 \text{ NmL min}^{-1}$  for the measurement of capacitive currents, then the gas flux was switched to pure  $O_2$  for the measurement of the ORR activity. The faradic current densities were calculated as described in section 2.4.1.

An electrochemical impedance spectroscopy measurement was taken at OCV, with a wave amplitude of 10 mV and frequencies in the range of 10 kHz – 100 mHz, for the evaluation of the high frequency resistance (R). The R value was used to subtract the ohmic drop contribution from the polarization curve [47].

#### 2.4.3. Chronoamperometry test

The stability of the two Co-N/MWCNT catalysts was investigated by means of a chronoamperometry performed both with the RDE and the GDE cell setups. In RDE the chronoamperometry was performed at a fixed potential of +0.55 V vs RHE for 17 hours in  $O_2$ -saturated 0.5 M  $H_2SO_4$ , with the working electrode rotating at 900 rpm. In GDE cell the chronoamperometry was also performed for 17 hours at the fixed potential of +0.55 V vs RHE. Gaseous oxygen was fluxed into the GDE at a constant flow rate of  $1500 \text{ NmL min}^{-1}$ . All of the current densities were normalized per geometric area of the electrode.

### 3. Results

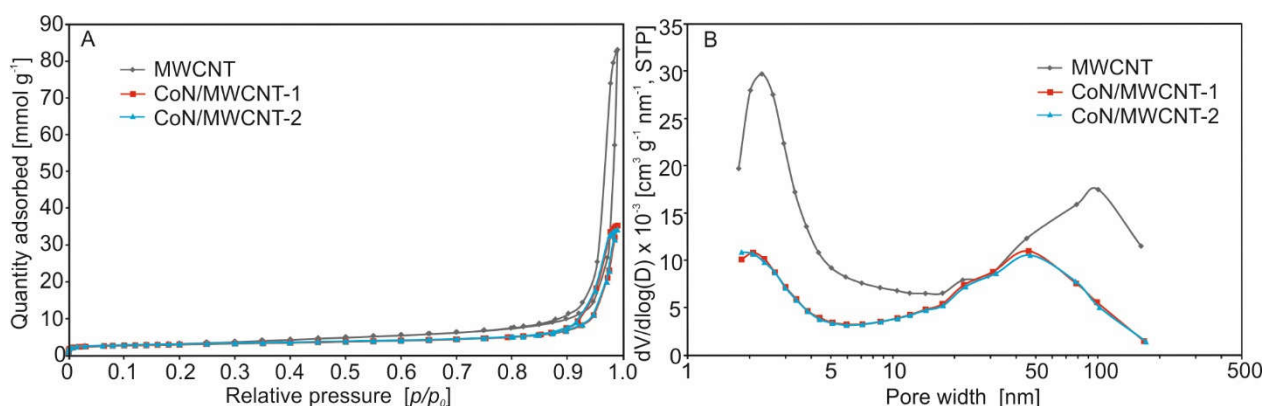
#### 3.1. Physico-chemical characterization

##### 3.1.1. BET analysis

Nitrogen adsorption/desorption analysis performed on pristine MWCNT support and on Co-N/MWCNT catalysts shows that all three samples exhibit the same isotherm shape (Fig. 2A), with the presence of a steep adsorption step in the high relative pressure range (0.9–1.0) and of an

adsorption/desorption hysteresis. This suggests that after pyrolysis treatments the original MWCNT structure does not change. Fig. 2B shows the pore size distributions of pristine MWCNT support and Co-N/MWCNT catalysts.

According to the International Union of Pure and Applied Chemistry (IUPAC) classification, the pristine MWCNT isotherm belongs to Type II, with the presence of a hysteresis loop, associated with capillary condensation taking place in mesopores [48]. As the adsorption and desorption branches are almost vertical and nearly parallel over an appreciable range of quantity of gas adsorbed, the hysteresis loop can be classified as H1-type. This is often associated with porous materials consisting of agglomerates [48], that could correspond to MWCNT aggregated felt-like morphology [49].



**Fig. 2.** Nitrogen adsorption/desorption isotherms (A) and pore size distribution (B) of pristine MWCNT and Co-N/MWCNT catalysts.

The adsorption of nitrogen on carbon nanotubes is remarkably different from the adsorption on other porous carbons in several aspects. First, due to their one-dimensional tubular structure, CNTs have a high aspect ratio and the external surface available for adsorption is considerably larger than the surface area available in the inner cavities. The adsorption on the external surface of CNTs is greater than the adsorption inside the micro/mesoporous cavities [49].

After the first heat-treatment, the BET specific surface area suffers a slight decrease in comparison to pristine MWCNT (from 259.1 to 222.8 m<sup>2</sup> g<sup>-1</sup>, Table 1), while the micropore surface area increases significantly, passing from 26.0 to 90.7 m<sup>2</sup> g<sup>-1</sup>. The same trend is observed for micropore volume. On the other hand, after the second heat-treatment, a small increase of BET specific surface area is registered, with a simultaneous increase of micropore area and volume. These results suggest that the first pyrolysis process, in which the incorporation of N and Co onto the MWCNT support structure takes place, leads to the formation of a great amount of new micropores. During the second heat treatment, further micropores are formed, probably due to the rearrangement of the MWCNT support

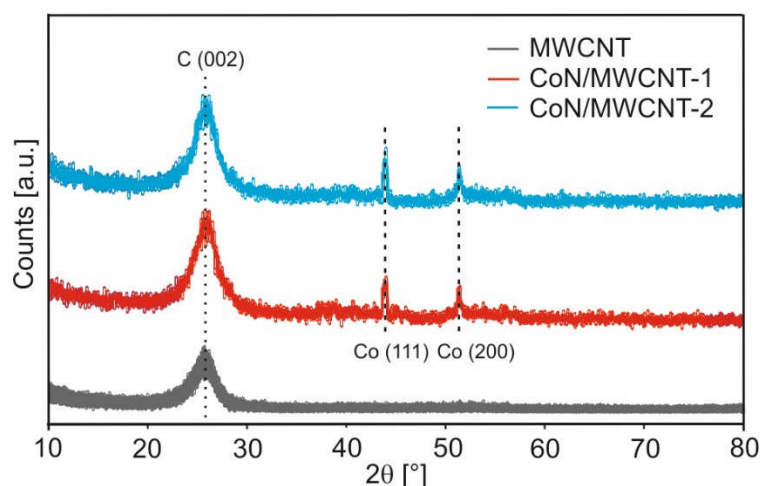
structure (as evidenced by FESEM analysis, Fig. 5C) and/or to the loss of some of the N atoms (as suggested from the lower N content measured in XPS analysis, Table 3).

**Table 1.** Surface characterization of pristine MWCNT and Co-N/MWCNT catalysts.

|              | BET surface area<br>[m <sup>2</sup> g <sup>-1</sup> ] | Micropore<br>surface area<br>[m <sup>2</sup> g <sup>-1</sup> ] | Micropore<br>volume<br>[cm <sup>3</sup> g <sup>-1</sup> ] | Adsorption average<br>pore width<br>[nm] |
|--------------|---|--|---|--|
| MWCNT        | 259.1   | 26.0   | 0.012   | 14.2                                     |
| Co-N/MWCNT-1 | 222.8   | 90.7   | 0.043   | 13.1                                     |
| Co-N/MWCNT-2 | 234.5   | 96.4   | 0.046   | 11.8                                     |

### 3.1.2. XRD analysis

XRD analysis (Fig. 3) indicates that for the Co-N/MWCNT catalysts and for the pristine MWCNT, a big broad peak is evident at  $2\theta = 25\text{--}26^\circ$  corresponding to graphite (002) reflection plane (JCPDS card nr. 00-01-0640) [50]. This suggests that the structure of the MWCNTs remains stable after the incorporation of N and Co during the pyrolysis process, as confirmed also by the nitrogen adsorption and desorption isotherms shape. In pristine MWCNT pattern there is no presence of any other peak, while in both catalysts, peaks at  $2\theta = 44^\circ$  and  $2\theta = 51^\circ$  are detected. In principle, Co oxides and other Co-containing unlinked moieties, should have been removed during the acid leaching treatment, and this is confirmed by the absence of Co oxides peaks in the XRD patterns. Therefore, the two peaks appearing in the catalysts could be attributed to metallic cobalt (JCPDS nr. 01-089-4308) that exhibits two intense diffraction peaks at  $2\theta = 44.23^\circ$  (111 reflection plane) and  $51.53^\circ$  (200 reflection plane). This was also found by *Li et al.* [26] for similar catalysts supported on carbon and prepared using Co-TPTZ complex. However, the presence of cobalt in the form of nitride Co<sub>4</sub>N (JCPDS nr 00-041-0943), which exhibits two peaks at  $2\theta = 43.72^\circ$  (111 reflection plane) and  $50.86^\circ$  (200 reflection plane), and in the form of carbide Co<sub>3</sub>C (JCPDS nr 00-043-1144), which has an intense peak at  $2\theta = 44.14^\circ$  (101 reflection plane), cannot be excluded.



**Fig. 3.** XRD patterns of pristine MWCNT and Co-N/MWCNT catalysts.

### 3.1.3. EDX analysis

EDX analysis performed on the Co-N-based catalysts before and after acid leaching is used to estimate cobalt, carbon and oxygen content. The atomic percentages measured are summarized in Table 2. The cobalt content before acid treatment for Co-N/MWCNT-1 and Co-N/MWCNT-2 is 3.67 and 3.58 wt. %, respectively (equivalent to 0.78% and 0.76% atomic). This is a good match with the value designed during the synthesis process (nominal 5.0 wt. %). Acid treatment is effective in removing not linked Co-N<sub>x</sub> moieties as well as cobalt compounds not strongly linked with the MWCNT structure. This leads to a final Co content of 0.76 and 1.09 wt. % for Co-N/MWCNT-1 and Co-N/MWCNT-2, respectively (equivalent to 0.15 and 0.23 at. %).

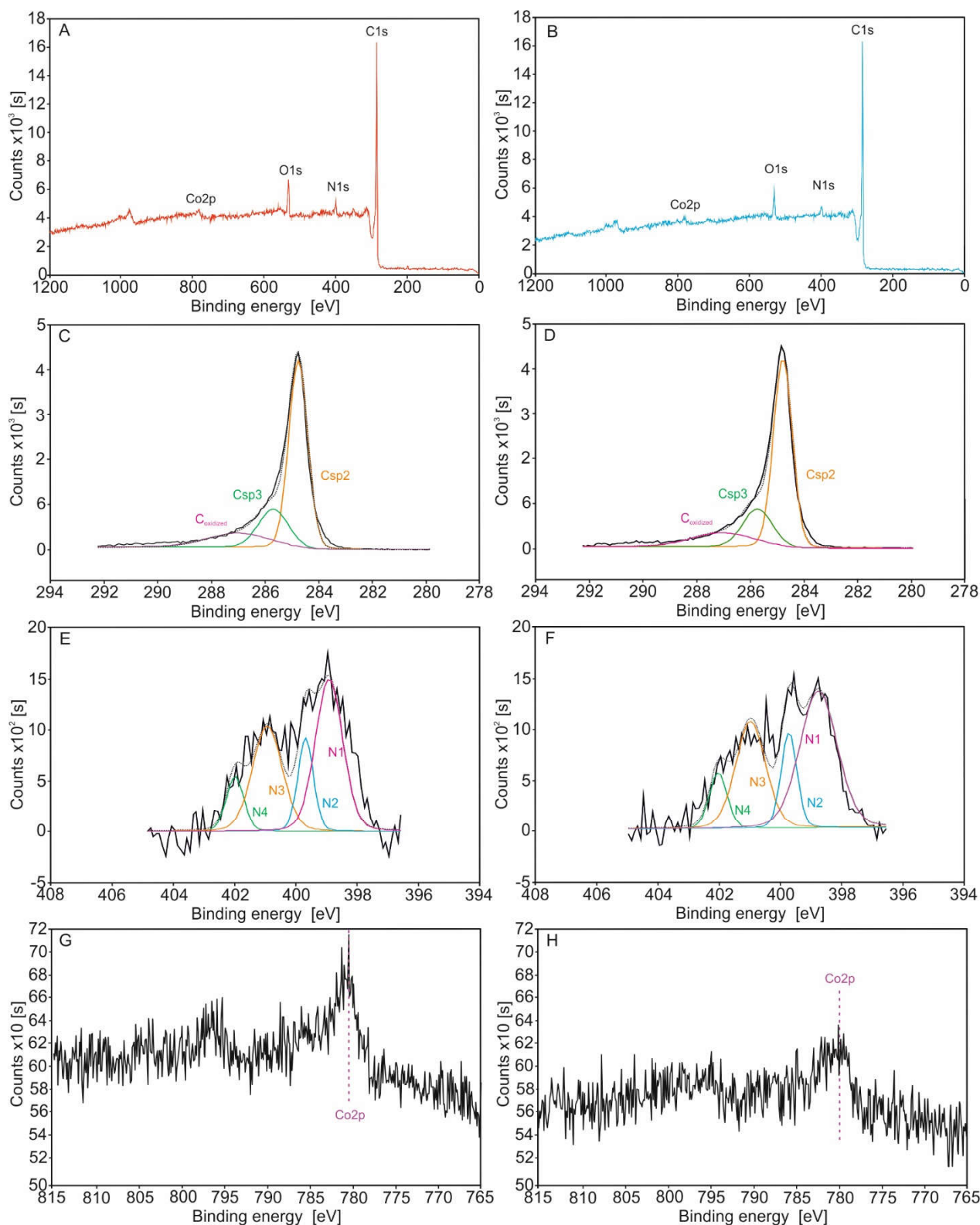
**Table 2.** Elemental compositions from EDX (atomic %) for the two Co-N/MWCNT catalysts.

|                     | Acid washing | Total C<br>[atomic %] | Total O<br>[atomic %] | Total Co<br>[atomic %] |
|---------------------|--------------|-----------------------|-----------------------|------------------------|
| <b>Co-N/MWCNT-1</b> | No           | 94.52                 | 4.70                  | 0.78                   |
| <b>Co-N/MWCNT-2</b> | No           | 95.20                 | 4.04                  | 0.76                   |
| <b>Co-N/MWCNT-1</b> | Yes          | 95.52                 | 4.32                  | 0.15                   |
| <b>Co-N/MWCNT-2</b> | Yes          | 95.98                 | 3.79                  | 0.23                   |

### 3.1.4. XPS analysis

XPS analysis was conducted on Co-N/MWCNT catalysts after acid washing treatment, to complete the elemental composition characterization. Results obtained prove further evidence of the incorporation of Co and N in the MWCNT carbon structure after the pyrolysis heat treatments and

acid leaching. Fig. 4 shows wide XPS scan spectra for Co-N/MWCNT-1 (Fig. 4A) and Co-N/MWCNT-2 (Fig. 4B). The peaks reveal the presence of C, O, N and Co in both catalysts surface. The predominant C1s peak is centered at 284.5 eV, and its asymmetric pattern can be due to the presence of C–N bonds in the carbon structure, which indicates that nitrogen atoms are successfully incorporated into the MWCNT support [27,51]. The peak at 532 eV is attributed to oxygen (O1s), and the peak at about 400 eV is the nitrogen peak (N1s). The peak at about 780 eV can be assigned to cobalt (Co2p), suggesting that also cobalt is incorporated onto MWCNT. However, the deconvolution of the high resolution of Co2p (Fig. 4G and 4H for Co-N/MWCNT-1 and Co-N/MWCNT-2, respectively) is too weak to determine Co valence state. The surface elemental composition is summarized in Table 3. The second heat-treatment on the Co-N/MWCNT-2 causes a decrease in O, N and Co contents. A significant loss of nitrogen after high-temperature pyrolysis was also found by Nallathambi *et al.* [52].



**Fig. 4.** XPS survey spectra (A and B), deconvolution of the high resolution C1s (C and D), N1s (E and F), and Co2p (G and H) XPS spectra for Co-N/MWCNT-1 (A, C, E, and G) and Co-N/MWCNT-2 (B, D, F, and H) catalysts.

The high resolution C1s spectra are shown for the two catalysts in Fig. 4C and 4D, respectively. For both catalysts, deconvolution shows two main peaks at binding energies of 284.8 and 285.7 eV, that



are respectively assigned to graphitic-like carbon (sp<sup>2</sup>) and diamond-like carbon (sp<sup>3</sup>) [53,54]. The smaller broad peak at higher binding energy values is related to chemical shifts due to C-O and/or C-N bonds [55–59]. Comparing the C1s spectra of the two samples, sp<sup>2</sup>, sp<sup>3</sup> and oxidized carbon relative contents remain almost equal.

The high resolution N1s spectra of Co-N/MWCNT catalysts are shown in Fig. 4E and 4F. These spectra are fitted into four different components: pyridinic-N (N1, with peak maximum at 398.8 eV), cyanide-N and/or M-N<sub>x</sub> bonding, with M = transition metal (N2, with peak maximum at 399.7 eV), pyrrolic-N and/or graphitic-N bonded to two C atoms and one H atom (N3, with peak maximum at 400.9 eV), and graphitic-N bonded to three C atoms (N4, with peak maximum at 402.0 eV). There are no peaks at higher binding energies (related with N oxidized groups) [21,24,27].

**Table 3.** Elemental surface compositions from XPS (atomic %) and N/C, O/C and Co/C atomic ratios for the two Co-N/MWCNT catalysts after acid washing treatment.

|                     | atomic % |     |     |     | atomic ratios |       |       |
|---------------------|----------|-----|-----|-----|---------------|-------|-------|
|                     | C        | N   | O   | Co  | N/C           | O/C   | Co/C  |
| <b>Co-N/MWCNT-1</b> | 87.3     | 6.7 | 5.2 | 0.8 | 0.077         | 0.060 | 0.009 |
| <b>Co-N/MWCNT-2</b> | 90.6     | 5.4 | 3.4 | 0.6 | 0.060         | 0.038 | 0.007 |

Table 4 shows the relative percent contents of the four different above mentioned N-types. The relative amounts are roughly similar in both catalysts, and only some marginal differences can be observed. In Co-N/MWCNT-2 the relative amount of pyridinic nitrogen (N1) is about 5% higher than in Co-N/MWCNT-1, and the amounts of the other three N-types (N2, N3, N4) are slightly lower in the former than in the latter. In particular, the lower amount of Co-N in Co-N/MWCNT-2 could be related with the slightly lower total Co surface content (Table 3). Moreover, according to the finding of Dodelet's group [16–18], the pyridinic-N (N1) is usually situated in micropores, which are more abundant in Co-N/MMWCNT-2 (Table 1). This could explain the higher pyridinic-N relative content found in this catalyst. The amount of nitrogen incorporated onto the nanotubes is influenced by the heat treatments, and it decreases after the second pyrolysis step. On the other hand, the nature of nitrogen species created onto the C-network of nanotubes is not significantly influenced by the heat treatment, and both catalysts have similar type of relative proportion of N-species. Regarding the relative abundance of pyridinic and pyrrolic-N, the amounts found in our samples are comparable to the values found by Pérez-Alonso *et al.* [20] for similar MWCNT-supported catalysts doped with N and Fe.

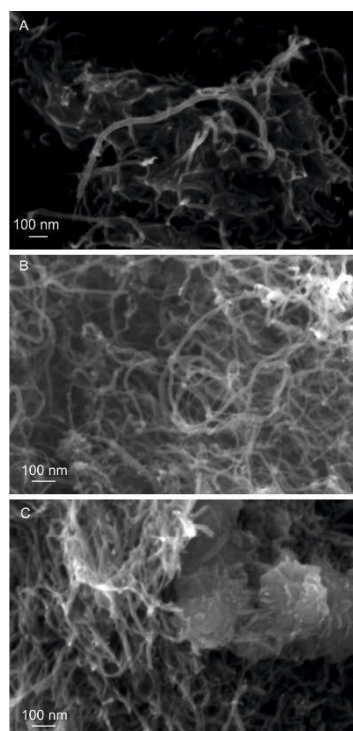
**Table 4.** Nitrogen contents with relative intensities and binding energies of N1s peaks from XPS analysis of the Co-N/MWCNT catalysts (N1: pyridinic N; N2: nitrile and/or or Co-N<sub>x</sub>; N3: pyrrolic N and/or graphitic N1 position; N4: graphitic and/or oxidized N.)

|                            | Atomic % |       |       |       |
|----------------------------|----------|-------|-------|-------|
|                            | N1       | N2    | N3    | N4    |
| <b>Binding energy [eV]</b> | 398.8    | 399.7 | 400.9 | 402.0 |
| <b>Co-N/MWCNT-1</b>        | 42.7     | 15.1  | 32.3  | 10.0  |
| <b>Co-N/MWCNT-2</b>        | 47.4     | 13.8  | 29.6  | 9.1   |

### 3.1.5. FESEM analysis

The morphological structure of the multi-walled carbon nanotubes can be clearly observed (Fig. 5A) for the MWCNT bare support. Brighter zones could correspond to MWCNT cross-linking contacts zones and to MWCNT terminations: EDX analyses in these areas revealed the presence of carbon only. The MWCNT external diameter is approximately between 20 and 10 nm.

Figure 5B show Co-N/MWCNT-1 evidences unchanged framework structure after the first pyrolysis. Co-containing crystallites are sometimes observed on the surface of nanotubes. After the second pyrolysis, on catalyst Co-N/MWCNT-2 (Fig. 5C), the MWCNT structure appears partially collapsed. Co-containing crystallites are still evident. However, they appear to be smaller and deeper conglomerated into the carbon nanotubes agglomerates, compared to Co-N/MWCNT-1. The presence of crystallites of Co-containing species is confirmed by the results of the XRD analysis (Fig. 3).

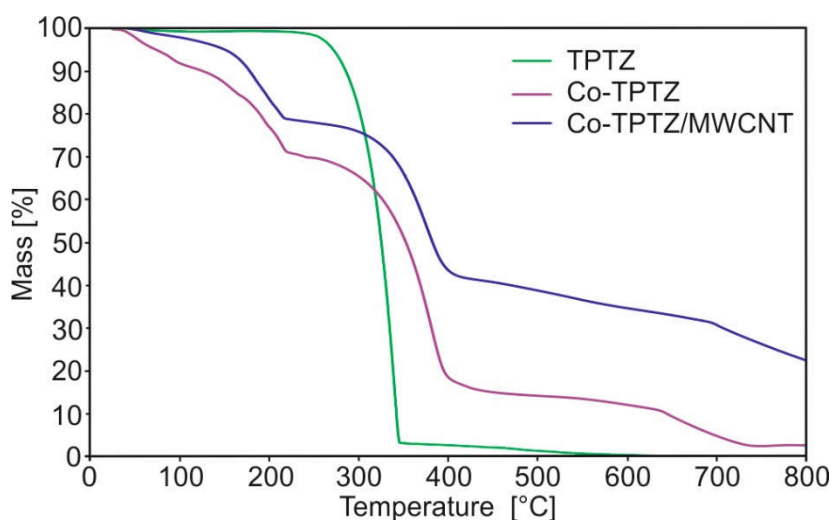


**Fig. 5.** FESEM pictures of pristine MWCNT (A), Co-N/MWCNT-1 (B) and Co-N/MWCNT-2 (C) catalysts.

### 3.1.6. TGA analysis

TGA analysis was conducted on the MWCNT impregnated with the Co-TPTZ complex, to investigate the behavior during the thermal treatment (Fig. 6). For comparison, TGA analysis was also conducted on unsupported Co-TPTZ complex and pure TPTZ.

The curve of pure TPTZ shows that this molecule rapidly decomposes in the temperature range between 250 and 345 °C. The Co-TPTZ complex has a more complicated behavior. There is a first mass decrease in the temperature range from 40 to 220 °C, that could correspond to the loss of physisorbed and coordinated water molecules [25,60]. A second steep weight loss is observed starting from 250 °C, until 400 °C. This can be related to TPTZ decomposition. Unlike the pure TPTZ, at temperatures higher than 400 °C the mass does not go to zero: an almost flat zone is observed from 400 to 650 °C, probably related to a partial graphitization of the C and N atoms of TPTZ. Similar behavior was also found by Tian *et al.* [14] for TPTZ in presence of Fe and Zn. Further mass loss is observed above 650 °C, until almost 3% at 750 °C. This quantity could correspond to the residual metallic cobalt. This residual mass, in fact, well matches with the initial Co content in the Co-TPTZ complex. The curve of the MWCNT impregnated with Co-TPTZ complex follows the same trend of the unsupported complex curve (Fig. 6). The lower mass decrease is therefore due to the presence of the MWCNT, which are more stable at high temperatures.

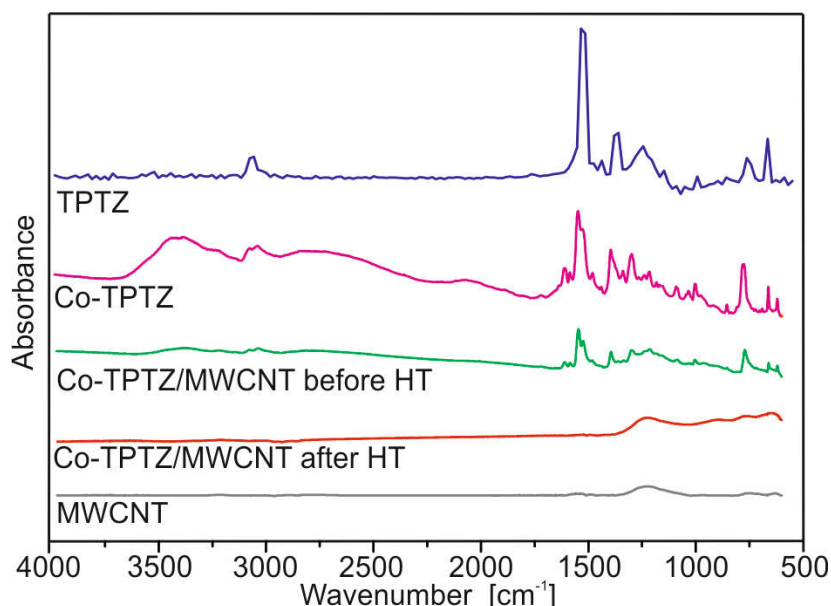


**Fig. 6.** TGA analysis under inert atmosphere of TPTZ, Co-TPTZ complex, and MWCNT impregnated with Co-TPTZ complex before the pyrolysis treatment.

### 3.1.7. FTIR analysis

FTIR spectra (Fig. 7) were recorded on the MWCNT impregnated with the Co-TPTZ complex before and after the pyrolysis heat treatment. Co-TPTZ complex, TPTZ alone, and pristine MWCNT were also analyzed for comparison.

The Co-TPTZ complex spectrum exhibits a broad absorbance peak in the range 3600-3300  $\text{cm}^{-1}$ , attributable to O-H stretching vibrations of water molecules, indicating the presence of hydrogen bonding [61]. The broad peak, smaller than the previous one, in the range 3100-3000  $\text{cm}^{-1}$  can be attributed to C-H stretching of aromatic rings [62]. Peak bands in the range 1650-1450 and 1400-1250  $\text{cm}^{-1}$  are attributed to C-C and C-N stretching vibrations of pyridine and triazine structures of the TPTZ molecule [61, 63–65]. These bands appear in heterocyclic as well as carbocyclic aromatic compounds, in both monocyclic and polycyclic structures [66]. The band between about 1200 and 1000  $\text{cm}^{-1}$  can be attributed to C-H in-plane bending of the aromatic rings [62]. The band in the range 850–620  $\text{cm}^{-1}$ , with three sharp peaks at about 775, 660 and 620  $\text{cm}^{-1}$  can be assigned to the C-H out-of-plane bending vibrations of aromatic compounds of the pyridyl rings. [61,62]. These peaks are usually strong and characteristic of the number of substituents in the ring [62]. Peaks at 1572 and 1525  $\text{cm}^{-1}$  can be attributed to TPTZ ligand coordinated with Co [61]. Peaks in the range between 935 and 913  $\text{cm}^{-1}$  can be attributed to Co-N bond in Co-containing macrocyclic compounds [64]. The peaks related to the organic groups of the Co-TPTZ complex match with the peaks of the TPTZ alone. Regarding the spectra of the MWCNT impregnated with the Co-TPTZ complex before the pyrolysis treatment, almost the same peaks and bands as the Co-TPTZ complex can be found, but with lower intensities. This is due to the presence of the MWCNT, that are almost transparent to IR radiation, as can be deduced by their FTIR spectrum, where no significant peaks appear.



**Fig. 7.** FTIR spectra of TPTZ, Co-TPTZ complex, MWCNT impregnated with Co-TPTZ complex before and after the pyrolysis heat treatment (HT), and pristine MWCNT.

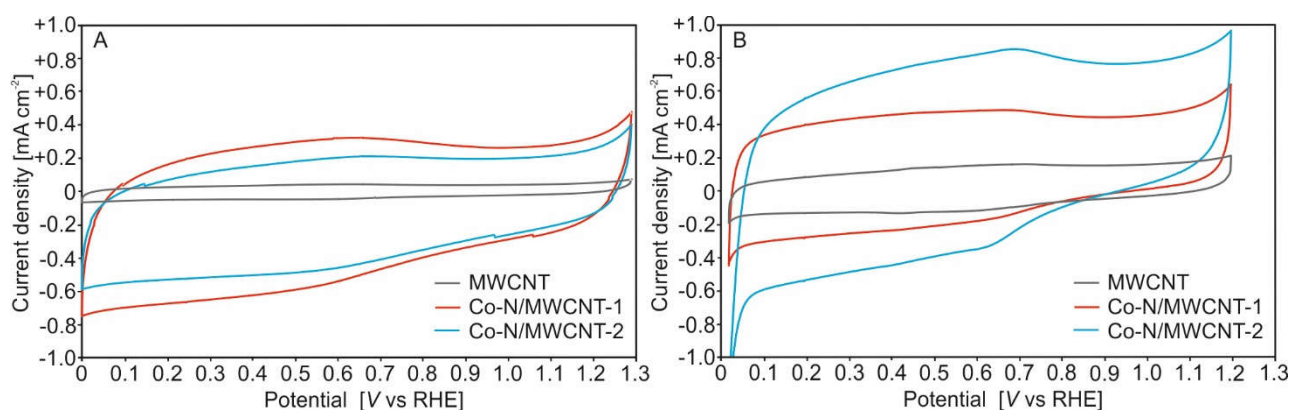
The MWCNT impregnated with the Co-TPTZ complex after pyrolysis at 800 °C (that is, the Co-N/MWCNT-1 catalyst) exhibits a FTIR spectrum very similar to the pristine MWCNT, and none of the peaks observed before the pyrolysis can be found, as also observed by Wang *et al.* [65]. Vibrations found between 500 and 1500  $\text{cm}^{-1}$  can be attributed to the KBr (not reported here). The disappearance of the characteristic peaks of the Co-TPTZ complex after the pyrolysis can be caused by two reasons. First, the complete disappearance of the original Co-TPTZ chelate structure during the pyrolysis, confirming the instability of this molecule at temperatures above 650 °C, as also evidenced by the TGA analysis results (Fig 6). Second, the relative amount of Co-N complexes after the pyrolysis is too small to be detected by the instrument, also due to the MWCNT high relative abundance and their transparency to infrared radiation.

### 3.2. Electrochemical characterization

#### 3.2.1. Cyclic voltammetries

The voltammograms recorded in presence of inert gas exhibit similar shapes in both RDE (Fig. 8A) and GDE cell (Fig. 8B), and the current density values are of the same order of magnitude.

The two catalysts have specific mass capacitance values between 28 and 47  $\text{F g}^{-1}$ , similarly to other non-noble metal electrocatalysts on porous carbon support [21].

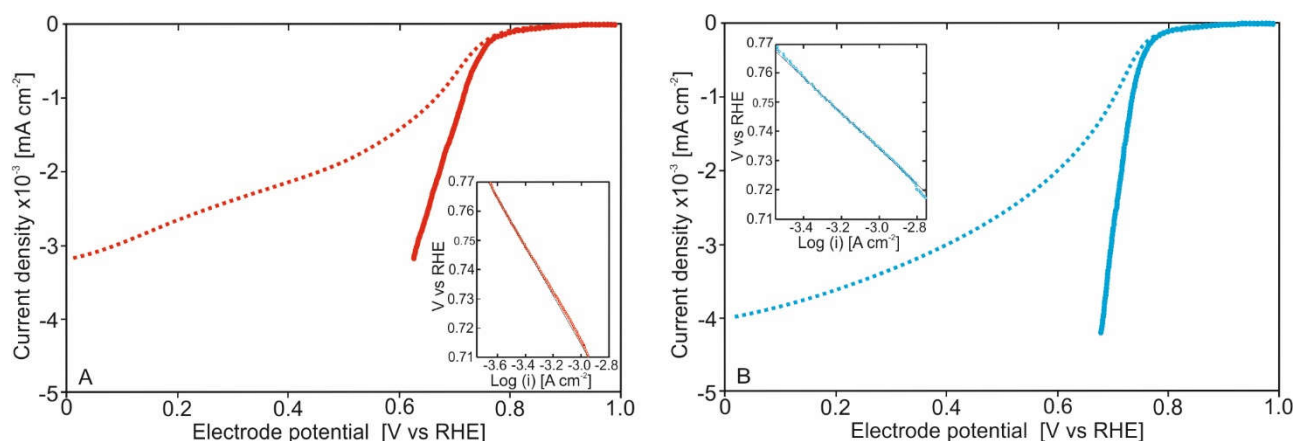


**Fig. 8.** Cyclic voltammograms of MWCNT support and Co-N/MWCNT catalysts recorded at 10  $\text{mV s}^{-1}$  scan rate in  $\text{N}_2$ -saturated 0.5 M  $\text{H}_2\text{SO}_4$  solution for RDE (A) and fluxing  $\text{N}_2$  gas in the working electrode for GDE cell (B).

The higher capacitive current exhibited by the catalysts in comparison with the pristine MWCNT, could be attributed to a series of redox processes involving the functional groups created during the incorporation of N and Co-N<sub>x</sub> groups, or even to the presence of C-oxidized functional groups on the MWCNT structure [67]. Oxygen presence, in fact, is revealed by XPS and EDX analyses (see Tables 2 and 3).

### 3.2.2. ORR activities

The ORR activity of the electrocatalysts is highly enhanced in comparison with the pristine MWCNT support, which shows practically no activity towards ORR in acidic conditions (not reported here). Co-N/MWCNT-2 catalyst is more active than Co-N/MWCNT-1. Apparently, the second heat treatment on Co-N/MWCNT-2 catalyst seems to be useful to increase the catalytic ORR activity. Observing the curves recorded in RDE test (Fig. 9), no well-developed diffusion limited plateau current zone is present for both catalysts, sign that the current density at high overpotential values could be still in a mixed kinetic and mass- or charge-transport limited zone [36,68]. The value of the limiting current densities, for Co-N/MWCNT-1 and Co-N/MWCNT-2, can be taken as 3.3 and 4.0  $\text{mA cm}^{-2}$ , respectively. Moreover, Co-N/MWCNT-2 exhibits a steeper current increase in the intermediate overpotential region (0.5–0.7 V vs RHE).

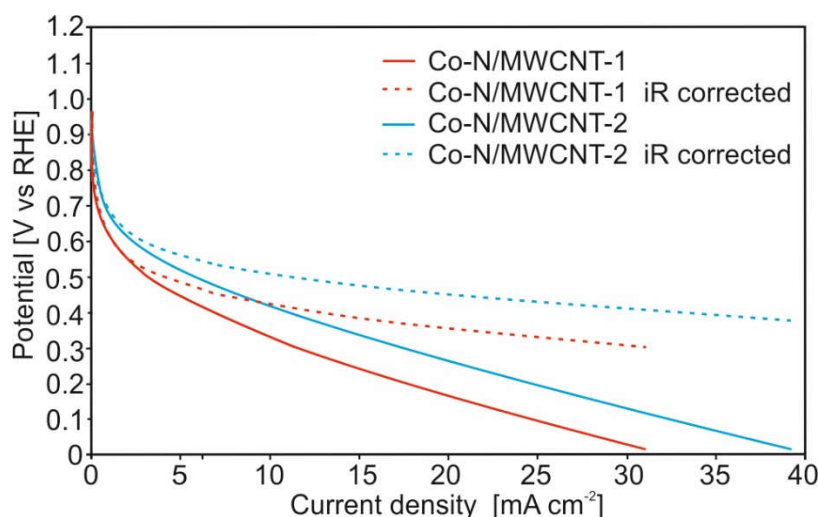


**Fig. 9.** ORR activity expressed as current density vs electrode potential (RHE) measured with RDE in  $\text{O}_2$ -saturated 0.5 M  $\text{H}_2\text{SO}_4$  solution at a rotational speed of 1600 rpm for Co-N/MWCNT-1 (A) and Co-N/MWCNT-2 (B): experimental curve (dashed lines), mass-transfer and iR corrected kinetic current density (continuous lines). The inset shows the Tafel behavior of the corrected kinetic current density. The Tafel slope of the linear portion of this graph allows the determination of the charge transfer coefficient  $\alpha$  for the ORR. Potential scan rate:  $10 \text{ mV s}^{-1}$ .

The ORR electro-reduction kinetic activity was calculated from mass-transport-corrected kinetic current density:  $i_k = i_L \cdot i / (i_L - i)$ , where  $i$  is the faradaic current density and  $i_L$  is the limiting diffusion current-density of the catalyst. A semi-empirical model similar to the model developed by Spinelli *et al.* [69] for PEM fuel cells, is used to evaluate the catalytic activity. The value of the electrical resistance is considered to account for ohmic drop in the electronic conductors, and for phenomena which require a more sophisticated treatment, such as non-ohmic effects due to the porous 3D nature of the electrodes, as the diffusion of the reactant through the porous layer and the solubility of the reactant in the porous layer, taking into account surface segregation, as reported by Chlistunoff [70]. A correction for the ohmic drop was applied to determine the ORR kinetic activity, shown in Fig. 9.

Such a correction was based on the resistance values obtained by the impedance measurements as indicated in the experimental section, taking into account the trend of the computed kinetic current curve.

The electrocatalytic activity of the Co-N/MWCNT catalysts was also tested in GDE cell. The current trend at high overpotentials (0.0 – 0.4 V vs RHE, Fig. 10) obtained in the GDE cell seems to linearly increase, suggesting the presence of an important ohmic drop limitation. For this reason, corrected values for the ohmic drop contribution are also reported. This kind of  $iR$ -limitation behavior was also observed for similar GDE cell setups by other groups [38,39]. Like previously observed in RDE tests, also in GDE cell tests the Co-N/MWCNT-2 catalyst exhibits higher electroactivity in comparison with Co-N/MWCNT-1.



**Fig. 10.** ORR activity (original and  $iR$ -corrected) measured in GDE cell in 0.5 M  $H_2SO_4$  solution fluxing gaseous oxygen in the working electrode for Co-N/MWCNT catalysts. Potential scan rate:  $10 \text{ mV s}^{-1}$ .

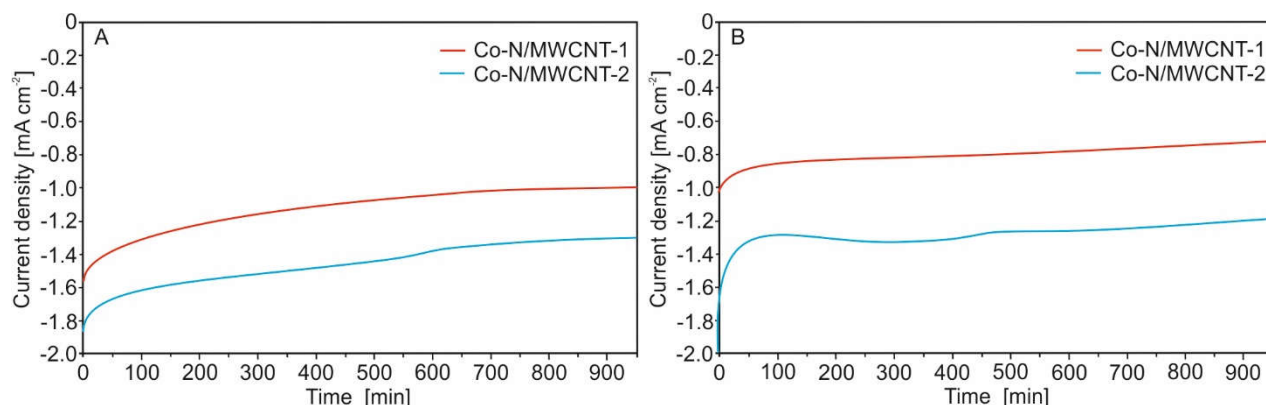
### 3.2.3. Chronoamperometry tests

Chronoamperometries in both RDE and GDE cell were also performed for the two Co-N/MWCNT catalysts, to investigate their behavior in time during operation at a fixed potential, and to assess electroactivity decay.

Fig. 11 show the chronoamperometric curves of the two catalysts recorded at +0.55 V vs RHE potential in RDE and in GDE cell, respectively. In RDE, the sample pyrolyzed twice exhibits a lower percent current density loss (about 21% after 950 minutes test) in comparison to the catalyst pyrolyzed only once (which exhibits about 34% loss after 950 minutes). A similar ORR current decay behavior was also observed in chronoamperometry test in acid conditions for similar types of catalysts by other groups [23,24,27].



In GDE cell, a similar current decay is observed. In this case, the difference between the losses of the two catalysts is lower, being of about 26% for Co-N/MWCNT-1 and 23% for Co-N/MWCNT-2 after 950 minutes.



**Fig. 11.** Chronoamperometric curves of Co-N/MWCNT catalysts for ORR activity at a potential of +0.55 V vs. RHE in O<sub>2</sub>-saturated 0.5 M H<sub>2</sub>SO<sub>4</sub> solution in RDE at a rotational speed of 900 rpm (A), and fluxing O<sub>2</sub> gas in the working electrode in GDE cell (B). Potential scan rate: 10 mV s<sup>-1</sup>.

## 4. Discussion

### 4.1. Physico-chemical characterization

XPS is a surface sensitive technique (the depth of the analysis being about 5–6 nm) [20], while the probe depth for EDX ( $\geq 1 \mu\text{m}$ ) makes possible to consider the results of this analysis as bulk composition [71]. Thus, the comparison between the Co content obtained from XPS analysis (surface composition, Table 3) and the results obtained from EDX analysis (bulk composition, Table 2), suggests that Co is predominantly situated on the MWCNT support surface. This is as expected from the wet impregnation with the Co(II)-TPTZ complex.

The overall N/C atomic ratios calculated on the basis of the results of XPS analysis, and summarized in Table 3, are similar to the values found by Geng *et al.* [72] for nitrogen-doped carbon nanotubes containing the same overall N amount. The N/C values found by Byon *et al.* [24] and Domínguez *et al.* [25] for Fe-N/MWCNT were also similar. However, N/C and transition metal/C atomic ratios of our catalysts are higher than in similar Me-N/MWCNT catalysts found by other research groups [13,20,24,25,35].

Nitrogen doping has repeatedly been reported to increase the catalytic activity of graphitic carbon. However, the role of the real “electrocatalytically active sites” is still not clear. Regarding the different types of N bonding, in some studies, the electrocatalytic activity is attributed to pyridinic-N



and/or pyrrolic-N [36,57]. On the contrary, other studies suggest that graphitic-N is more important for the electrocatalytic activity of nitrogen-doped carbon [58,59]. Nitrogen-doping in a basal plane of carbon may be more favorable than in edge sites because the number of available doping sites is greater in the basal plane than in the edge [73].

Concerning the overall surface nitrogen content, Jaouen *et al.* [21] have observed its influence for nine different NPMC, and no relation was found between N content and catalyst electroactivity towards ORR. The same conclusion was drawn restricting the analysis to pyridinic or pyrrolic-N types. This could mean that, even if nitrogen atoms are known to be part of active sites, their amount is not the limiting factor for activity, compared to other factors. Regarding the relationship between the transition metal content and the catalytic activity, Jaouen *et al.* [74] observed that the activity increases only up to a Co (or Fe) content of about 1 wt. %. Then, for higher metal contents the activity starts to decrease, due to the concomitant decrease of the microporous area of the catalysts caused by the excessive metal coverage.

Even though the exact structure of the active site cannot clearly be identified by means of the performed physicochemical analysis techniques, it is evident that some of the nitrogen and cobalt atoms from the Co-TPTZ complex are incorporated onto the MWCNT surface during the pyrolysis. Therefore, during the catalysts synthesis, the surface of MWCNT has been modified, as confirmed by the XPS analysis (N and Co are effectively detected on the catalysts surface). Furthermore, the electrochemical analyses evidenced a great enhancement of electroactivity towards ORR.

#### 4.2. Electrochemical characterization

Different factors could influence the capacitance of carbon materials: pore geometry, pore size distribution, electrical conductivity, wettability, and presence of surface electroactive species [67,75,76]. Additionally, pseudo-capacitance effect of surface redox-sites must be considered. At the carbon surface, in fact, apart from the electrostatic double layer capacitance, a significant pseudo-capacitance is often present. This can be due to chemisorption phenomena with partial charge transfer, or to redox processes (e.g. involving quinone-hydroquinone functional groups). These pseudo-capacitance effects related with the faradaic reactions of surface groups enhance the value of the capacitance [67]. Therefore, the increase of the capacitance of the Co-N/MWCNT catalysts in comparison with the pristine MWCNT could be related to the described phenomena.

Rigorous and correct analysis of the data from RDE experiments can be complicated in presence of a porous, not very thin catalyst film. In fact, with porous electrodes, the depth of oxygen penetration inside the electrode structure changes with the electrode potential. If the electrocatalyst is Pt, oxygen reduction is fast enough that at high overpotential, the reaction is limited only on the outer part of the

porous electrode, and a flat limiting plateau is observed. For other electrocatalysts poorer than Pt, some of the electrocatalytic particles inside the electrode might be in contact with oxygen even at high overpotential, causing a not proper flat limiting plateau [77]. Moreover, the distribution of electrocatalytic sites on the electrode surface could be responsible for such behavior: when active sites are not abundant and reaction is slower, the plateau results slightly inclined [78–80], as in the case of Fig. 9.

In spite of the difficulty of analyzing the kinetic current for ORR, a Tafel behavior was observed in a rather limited potential range as indicated in the insets of Fig. 9A and 9B, for the two Co-N/MWCNT catalysts, respectively. In particular, catalyst Co-N/MWCNT-1 has a Tafel slope of  $-80.9 \text{ mV dec}^{-1}$ , with a charge transfer coefficient  $\alpha$  equal to 0.73 (inset of Fig. 9A), whereas catalyst Co-N/MWCNT-2 shows a Tafel slope of  $-60.8 \text{ mV dec}^{-1}$ , with  $\alpha$  equal to 0.97 (inset of Fig. 9B), very close to the theoretical behavior of Pt/C based catalysts ( $-58 \text{ mV dec}^{-1}$ , with  $\alpha$  equal to 1, ascribed to the transfer of the first electron as the rate-determining step and Temkin conditions of intermediate adsorption). Higher Tafel slope values could be ascribed to a more complicated ORR mechanism, which may result from the migration of intermediates [20,81], or from the presence of surface redox couples/functional groups which act as a barrier for the oxygen reduction [82].

RDE testing, after mass transfer and ohmic drop correction, allowed an estimation of the electrocatalytic activity of the two catalysts. According to this computation, an activity value of  $0.54 \text{ mA cm}^{-2}$  was found at 0.75 V vs RHE for catalyst Co-N/MWCNT-2, while an activity of  $0.37 \text{ mA cm}^{-2}$  was obtained for catalyst Co-N/MWCNT-1 at the same potential. The potential value of 0.75 vs RHE lies within the potential range of validity of the Tafel behavior as reported in the insets of Fig. 9. For the purpose of comparison with “the state of the art” in the literature for similar catalysts (See section 1), the above values can be easily transformed in mass activities, simply dividing by the catalyst load on the electrode ( $\text{g cm}^{-2}$ ) resulting in  $0.57 \text{ A g}^{-1}$  for Co-N/MWCNT-2 and  $0.39 \text{ A g}^{-1}$  for Co-N/MWCNT-1. The activities obtained are comparable to most of the NPMC in the literature, although they are still far away from the best “state of the art” values [16,22].

From the results of the electrochemical characterization on Co-N/MWCNT catalysts in this work, performing the second pyrolysis treatment seems to be beneficial for both the electroactivity and the stability in time. The higher activity of Co-N/MWCNT-2 catalyst could be related to its higher micropore content in comparison with Co-N/MWCNT-1 (Table 1). Micropores, in fact, are found to be closely related with the electrocatalytic activity of NPMC. Jaouen *et al.* [16] suggest that the distance between two pore walls must have an exact value for an active site to be formed in these types of NPMC, suggesting that the catalytic site is a molecular assembly bridging two pore walls. For example, the microporous surface area of various NPMC was investigated by Jaouen *et al.* [21]

for nine different NPMC, showing a trend of increasing activity with increased micropore surface area.

The catalysts activity losses noticed in the chronoamperometry tests, could be due to many different reasons. The loss in the carbon conductivity plays a crucial role because of carbon corrosion due to radicals attack [83–85]. Another reason could be the unstable nitrogen fixation. In particular, pyridinic and pyrrolic nitrogen can be protonated in acidic medium, leading to loss of stability with time, whereas stability could be attributed to the presence of stable N groups, mainly graphitic-like [27,86,87]. Therefore, the activity losses of the Co-N/MWCNT catalysts could be attributed to their relatively high content of both pyridinic and pyrrolic nitrogen, and relatively low content of graphitic nitrogen (Table 4). The higher stability of Co-N/MWCNT-2 could be ascribed to a higher degree of graphitization of the carbon support [88,89].

The Co-N/MWCNT catalysts developed in this work, can also be considered as starting point for further optimization of the different synthesis parameters such as the precursors quantities, the number of heat treatments and their temperatures and duration. Moreover, impregnations with further quantity of Co and N-containing molecules, using these catalysts as C-supports can be considered, to improve the final catalyst performances [90,91].

## 5. Conclusions

Two cobalt-nitrogen catalysts were synthesized by wet impregnation of multi walled carbon nanotubes (MWCNT) with a complex formed between Co(II) ions and the nitrogen-containing molecule 2,4,6-tris(2-pyridyl)-1,3,5-triazine (TPTZ), followed by one or two identical heat treatments in N<sub>2</sub> atmosphere at 800 °C for 3 hours. The physicochemical characterization confirmed the incorporation of N and Co in the MWCNT structure. This is related with the formation of active sites for ORR, even if the nature of the active site is still unknown.

The electrocatalytic activity towards ORR of the catalysts in acid conditions was assessed by RDE apparatus and a GDE cell. In both testing approaches, the catalyst heat-treated twice (Co-N/MWCNT-2) exhibited higher electroactivity than the catalyst heat-treated once (Co-N/MWCNT-1). Chronoamperometries performed at 0.55 V vs RHE on both RDE and GDE cell showed less electroactivity decay and better current performance for the catalyst heat-treated twice, as if the second heat-treatment allowed a better stabilization of the active sites. The higher electroactivity and stability of the Co-N/MWCNT-2, heat-treated twice, could be ascribed to an increase of the microporosity. The activities obtained are comparable to most of the NPMC in the literature.

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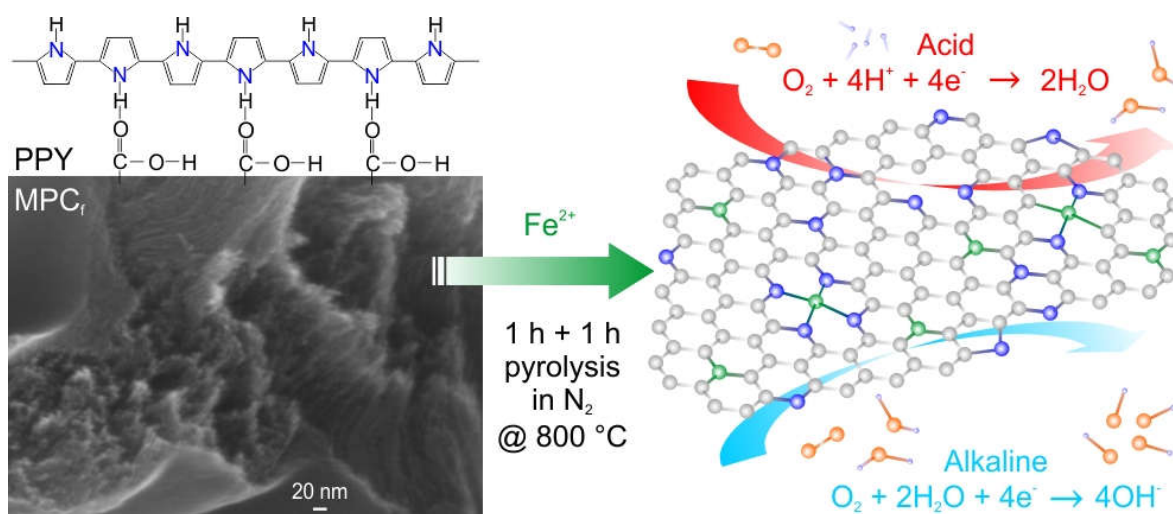




## CHAPTER 4. Optimization of a Fe-N-C electrocatalyst supported on mesoporous carbon functionalized with polypyrrole for oxygen reduction reaction under both alkaline and acidic conditions.

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### 1. Introduction

The high cost of Pt has been until now one of the main factors that have limited the widespread commercialization of the PEM fuel cell devices.<sup>1</sup> In particular, on the cathode of the PEM fuel cells, a high amount of Pt has to be used, due to the sluggish kinetics of the oxygen reduction reaction (ORR).<sup>2</sup> This leads to great overpotentials and lower energy conversion efficiency, making crucial the research toward non-precious metal based materials as ORR electrocatalysts in alternative to Pt.<sup>3</sup> Several types of carbon-based materials containing nitrogen and transition metal atoms have been found to be active towards ORR. The first studies were conducted in the 1960s on transition metals (Fe, Co) macrocyclic compounds like phthalocyanines and porphyrins.<sup>4</sup> In more recent years, many different synthesis strategies have been successfully adopted to obtain active Me-N-C (Me = Fe, Co, Cu, Mn, ecc.) ORR catalysts, using many different C supports, N-containing molecules, polymers or ammonia gas as N sources, and different transition metals ions.<sup>5</sup>

Heat treatment at temperatures between 600 and 1000 °C in inert (Ar, N<sub>2</sub>) or reactive (NH<sub>3</sub>) atmosphere has also been found to be very effective in increasing the ORR activity and stability of these materials.<sup>6</sup> Performing a second heat treatment seems also to have a positive effect.<sup>7,8</sup>

Regarding the C support characteristics, it should have good electrical conductivity properties in order to assure a fast electron delivery to the active site.<sup>9</sup> It should also have high specific surface area and good pore size distribution properties in order to provide a sufficiently high number of active sites per unit area of the electrode, and at the same time favour the reactants and products transport to and from the active sites.<sup>10</sup>

The use of N-containing polymers like polyaniline and polypyrrole, has been proved to be an effective and cheap way to functionalize the surface of a carbon support with nitrogen atoms<sup>11</sup>, or even to directly produce N-doped carbon materials without using any additional carbon support.<sup>12,13</sup> N-containing electroconductive polymers (i.e. polyaniline, polypyrrole, polythiophene) were found to be active toward ORR even without performing any heat treatment.<sup>14–16</sup> However, after having heat treated at high temperature under inert atmosphere, the ORR electroactivity improves significantly, as well as the stability.<sup>7,17–19</sup>

In this work, the synthesis of a noble metal-free Fe-N-C catalyst for ORR is optimized in order to obtain a more active catalyst. Inexpensive molecules (in comparison with Pt and more costly N-containing organic macrocyclic complexes) like sucrose and pyrrole are used as C and N sources, respectively. The first part of the optimization was the investigation of the effect of the addition of the N-containing surfactant polyvinylpyrrolidone (PVP) during the wet impregnation of the MPC-PPY support with Fe(II) ions. The use of surfactants in solution in synthesis procedures involving metal ions reduction and deposition with or without C-based supports has been found to be useful to achieve a better metal particles dispersion and distribution in different literature studies.<sup>20–22</sup> However, to the best of our knowledge, the effect of the use of PVP (as well as of other surfactants) in syntheses involving metal ions impregnation or complexation with N-containing molecules has not been investigated yet. The effect of performing a preliminary heat treatment before the wet impregnation with Fe ions was also investigated. Afterwards, in the second part, a further optimization was done, using the best catalyst obtained in the first part as support. The influence of a second pyrolysis treatment performed with or without further impregnation with different amounts of Fe was investigated. The activities towards ORR in acid and alkaline conditions were measured using a rotating disk electrode (RDE) equipment. The catalysts activity vary depending on the different synthesis parameters. An evident ORR activity increase after the second heat treatment was found, and a direct correlation between the electroactivity and the catalyst surface area and micropores content was observed.

## 2. Experimental

### 2.1. Chemicals

Tetraethyl orthosilicate (TEOS,  $\geq 98\%$  purity), Hydrochloric acid (37 wt. %), Pluronic P123® triblock copolymer, Nitric acid (70 wt. %), Sulfuric acid (98 wt. %), Sucrose ( $\geq 99.0\%$  purity), Hydrofluoric acid ( $\geq 40$  wt. %), Pyrrole ( $\geq 98\%$  purity), Ethanol ( $\geq 99.8\%$  purity), Acetone ( $\geq 99.8\%$  purity), Perchloric acid (70 wt. %), Ammonium persulfate (APS,  $\geq 99.8\%$  purity), Nafion® 5 wt. % hydroalcoholic solution, Iron(II) Acetate ( $\geq 99.99\%$  purity) and Polyvinylpyrrolidone (PVP, mw 10000) were purchased from Sigma Aldrich. Nitrogen and oxygen gases were supplied in cylinders by SIAD with 99.999% purity. All aqueous solutions were prepared using ultrapure deionized water obtained from a Millipore Milli-Q system with resistivity  $>18 \text{ M}\Omega \text{ cm}^{-1}$ .

### 2.2. Synthesis

#### 2.2.1. Synthesis of silica template

Mesoporous silica SBA-15 was prepared following the procedure reported by Zeng et al.<sup>23</sup>, using the triblock copolymer EO<sub>20</sub>PO<sub>70</sub>EO<sub>20</sub> (Pluronic P123) as surfactant and TEOS as silica source.

In detail, 8.3 g of P123 was dissolved into 312 mL of 1.6 M HCl solution under stirring at 40 °C. Then, 19 mL of TEOS was added and the solution was stirred for 20 h keeping the temperature constant at 40 °C. Then, the temperature was increased at 100°C and maintained constant for 24 h. The product was filtered, washed with deionized water, and calcined in oven at 550 °C for 10 h under air in order to completely remove the surfactant.

#### 2.2.2. Synthesis of mesoporous carbon

Mesoporous carbon (MPC) was synthesized using mesoporous silica SBA-15 via hard templating method.<sup>23</sup> Sucrose was used as the carbon source and the synthesis method consists on impregnating the SBA-15 silica with a solution containing sucrose and sulphuric acid. More in detail, a solution containing 10 mL of deionized water, 0.152 mL of H<sub>2</sub>SO<sub>4</sub> and 2.5 g of sucrose was pipetted drop by drop onto 2 g of SBA-15. Then the temperature was increased at 100°C on a hot plate, and kept constant for 6 hours. Subsequently the temperature was increased to 160 °C and kept constant for 6 h more. This two-steps heating procedure is repeated after pipetting drop by drop a solution containing 10 mL of deionized water, 0.098 mL of H<sub>2</sub>SO<sub>4</sub> and 1.6 g of sucrose. This further addition of solution was done in order to completely fill the internal pores of the SBA-15 silica with the carbon precursor. Then, the carbon-silica mixture was heat-treated in a quartz-tube reactor at 830 °C for 6 h under nitrogen flow. To completely remove the silica template, the mixture was dispersed in 110 mL

of 5 % wt. HF solution. Finally, MPC was filtered under vacuum, washed with abundant deionized water and acetone, and dried in air.

In the following step, MPC was functionalized by reaction with concentrated sulphuric and nitric acid mixture, in order to introduce oxygen-containing functional groups (e.g. carbonyls, hydroxyls and carboxylic groups) on the MPC surface. 750 mg of MPC were introduced together with 120 mL of 1:1 vol. mixture of 98% wt.  $\text{H}_2\text{SO}_4$  and 65% wt.  $\text{HNO}_3$  into a triangular flask connected to a reflux apparatus. They were kept in reflux under stirring for 2 hours. Then 400 mL of deionized water was added (this causes a fast temperature increase). The mixture was stirred and kept under reflux overnight. Then the functionalized MPC were filtered under vacuum, washed with abundant deionized water until neutral pH and dried in air. This surface functionalization should favour the pyrrole polymerization to preferentially take place on the MPC surface, due to the formation of hydrogen bonds between the oxygen-containing functional groups and the -NH groups of pyrrole.<sup>11</sup>

#### 2.2.3. Synthesis of Fe-N-C catalysts – First optimization step

In the following step of the synthesis, 350 mg of functionalized MPC were dispersed into 100 mL of 1:1 vol. solution of 1 M  $\text{HClO}_4$  and ethanol. Then 90.2  $\mu\text{L}$  of pyrrole monomer was added (pyrrole: MPC wt. ratio 1:4) and the mixture was left under stirring for 2 hours. Afterwards, 0.298 g of APS (pyrrole:APS molar ratio 1:1), used as oxidant for the polymerization of pyrrole,<sup>24,25</sup> was dissolved in 10 mL deionized water and added slowly drop by drop to the MPC-pyrrole mixture. After leaving the reaction under stirring for 12 hours, the suspension was filtered, washed with 500 mL deionized water and 50 mL acetone, and dried in air at room temperature overnight.

Afterwards, 100 mg of MPC-PPY composite was added to 100 mL of 1:1 deionized water - ethanol solution and stirred for 30 min. Then, 8.95 mL of 0.01 M Fe(II) acetate solution was added, and the dispersion was placed into an ultrasonic bath (130W, Soltec 2200M3S sonicator) for 30 min. and left under stirring overnight. Then the solvent was evaporated by heating, and the recovered powder was pounded in a mortar. This first sample was named S1.

Another sample was obtained in the same way but with the addition of 20 mg of PVP (0.1 wt. % in the solution) as surfactant (S2).

Two more samples were prepared in the same way as the previous ones, but heat-treating the MPC-PPY support at 800°C under  $\text{N}_2$  flow for 3 hours (same heat treatment procedure described below) before the impregnation with Fe(II) ions (S3 and S4).

The Fe:MPC-PPY ratio in all these samples was expected to be 5% wt. All of the samples were heat treated in a tubular quartz furnace under nitrogen atmosphere ( $\text{N}_2$  gas flux set at 80  $\text{NmL min}^{-1}$  with a mass flow controller from Bronkhorst, ELFLOW series). The heating rate was 10  $^\circ\text{C min}^{-1}$ . When the temperature reached 800°C, it was kept constant for 1 h. Then the furnace was switched-off,

leaving the apparatus cooling down naturally to room temperature. Then, to remove any unbounded Fe moiety, all of the samples were washed with 75 mL of 1 M HCl solution under stirring for 3 h, filtered and dried at room temperature overnight.

The MPC-PPY support without Fe impregnation before (S5) and after pyrolysis (S6) was also tested for comparison.

A summary of the samples synthesized in the first optimization step and subsequently analyzed is presented in Table 1.

**Table 1.** Summary of the catalysts synthesized in the first optimization step.

| Sample name | Preliminary pyrolysis | Impregnation with Fe <sup>2+</sup> ions | Use of PVP during Fe <sup>2+</sup> impregnation |
|-------------|-----------------------|---|---|
| S1          | No                    | Yes                                     | No  |
| S2          | No                    | Yes                                     | Yes   |
| S3          | Yes                   | Yes                                     | No  |
| S4          | Yes                   | Yes                                     | Yes   |
| S5          | No                    | No                                      | -   |
| S6          | Yes                   | No                                      | -   |

#### 2.2.4. Synthesis of Fe-N-C catalysts – Second optimization step

In the second optimization step, the most active catalyst obtained in the first part was used as C-N support. Four more catalysts were produced. The first one was obtained simply after a second pyrolysis in N<sub>2</sub> atmosphere at 800°C preformed exactly in the same conditions as in the first step, without impregnation with more Fe (S7). For the other three catalysts, before performing the second heat treatment, a further impregnation of the support with different Fe(II) ions amounts (5 – 15 – 30 wt. % for S8 – S9 – S10 respectively) was performed, using the same impregnation procedure that led to obtain the more active catalyst in the first optimization step (i.e. without PVP addition). Table 2 shows a summary of the samples prepared in the second optimization step.

**Table 2.** Summary of the catalysts synthesized in the second optimization step.

| Sample name | Impregnation with Fe <sup>2+</sup> ions before 2 <sup>nd</sup> pyrolysis | Fe wt. % on C support |
|-------------|--|-----------------------|
| S7          | No   | -                     |
| S8          | Yes  | 5                     |
| S9          | Yes  | 15                    |
| S10         | Yes  | 30                    |

As a purpose of clarity, the whole synthesis process is schematized in Figure S7 in the Supporting Information.

### 2.3. Physical characterization

Nitrogen adsorption and desorption isotherms of SBA-15 silica, MPC, MPC-PPY supports, and Fe-N-C catalysts were recorded using an ASAP 2020 Instrument (Micromeritics) at  $-196\text{ }^{\circ}\text{C}$ , within the relative pressure range of 0 – 1. Before the analysis, all of the samples were placed into the cell and degassed under vacuum for 3 hours at  $150\text{ }^{\circ}\text{C}$ . The specific surface area of the samples was calculated using the Brunauer–Emmett–Teller (BET) method within the relative pressure range 0.1 – 0.3. The pore size distribution for mesopores was obtained with the Barrett–Joyner–Halenda (BJH) method. The micropores area and volume were obtained by the t-plot method and by a Density Functional Theory (DFT) model.

Scanning electron microscopy coupled with energy-dispersive X-ray spectroscopy (SEM-EDX FEI-Quanta<sup>TM</sup> Inspect 200 with EDAX PV 9900 instrument working at 15 kV), was performed to analyze the chemical composition of the samples, detecting the presence of Fe in the bulk of Fe-N-C catalysts. Morphology of SBA-15 silica, MPC, MPC-PPY, and Fe-N-C catalysts (S1 and S7) were investigated using a field emission scanning electron microscope (FESEM, model JEOL JSM 6700F).

Transmission electron microscopy (TEM) was performed on the most performing Fe-N-C catalyst (S7) using a FEI Monochromated Tecnai 200STEM-FEG microscope with a point resolution of 0.2 nm, information limit of 0.1 nm, which was operated at 200 kV, coupled with a boron EDS (Energy Dispersive Spectroscopy), in which images were acquired with CCD camera (4096x4096). Samples to be examined were prepared by immersing a Quantifoil R copper microgrid in a dispersion of the catalyst in ethanol ( $5\text{ mg mL}^{-1}$ ).

X-ray photoelectron spectroscopy (XPS) was performed to determine the elemental surface composition of the catalysts samples, detecting the presence of N and Fe. The analysis was carried out using a Physical Electronics PHI 5000 Versa Probe electron spectrometer system with monochromated Al  $K_{\alpha}$  X-ray source ( $1486.60\text{ eV}$ ) run at 15 kV and 1 mA anode current. Survey scans as well as narrow scans (high resolution spectra) were recorded with a spot of 100 nm size. The survey spectra were collected from 0 to 1200 eV. The narrow N 1s spectra were collected from 390 to 412 eV, the narrow Fe 2p spectra from 700 to 740 eV, and the narrow C 1s spectra from 278 to 298 eV. Before the measurements, all of the samples were placed in an ultrahigh vacuum chamber at  $2 \cdot 10^{-10}$  mmHg, and calibrated against a value of the C 1s binding energy of 284.5 eV. CasaXPS software was used for obtaining the N 1s and C 1s peaks deconvolution and the semi-quantitative atomic percentage compositions, using Gauss – Lorentz equations with Shirley-type background. A 70% Gaussian / 30% Lorentzian line shape was used to evaluate peaks position and areas.

For Fourier transform infrared spectroscopy (FTIR) measurements, powder samples were mechanically mixed with KBr and pressed. IR spectra were collected in air at  $2\text{ cm}^{-1}$  resolution on a Bruker Equinox 55 FTIR spectrophotometer, equipped with a MCT (Mercury Cadmium Telluride) detector.

#### 2.4. Electrochemical measurements

The electrochemical tests were conducted in a conventional three-electrodes electrochemical cell configuration, using a rotating disk electrode equipment (RRDE-3A ALS) and a multi-potentiostat (Bio-Logic SP-150). The cell was equipped with a glassy carbon disk working electrode ( $0.07\text{ cm}^2$  geometric area), a Pt helical wire counter electrode, and a saturated calomel reference electrode (SCE). The electrolyte was  $0.5\text{ M H}_2\text{SO}_4$  solution for tests in acidic conditions and  $0.1\text{ M KOH}$  solution for tests in alkaline conditions. The electrolytes were saturated with  $\text{N}_2$  for cyclic voltammetries (CV) and with  $\text{O}_2$  for ORR activity linear sweep voltammetries (LSV) analyses, by direct gas bubbling into the solution.

For the catalyst deposition on the working electrode surface, a catalyst ink was prepared. A typical ink preparation consists in mixing  $10\text{ mg}$  of sample powder with  $43\text{ }\mu\text{L}$  of Nafion® 5% wt. solution and  $400\text{ }\mu\text{L}$  of ethanol. The ink was kept under sonication for 1 hour to achieve a good dispersion. Afterwards,  $1\text{ }\mu\text{L}$  of ink was taken with a micro-pipette and deposited on the working electrode, resulting in a catalyst loading of  $0.0225\text{ mg}$ , which corresponds to  $0.318\text{ mg cm}^{-2}$  referred to the geometrical area of the disk working electrode. The electrode potentials were corrected and referred to the reversible hydrogen electrode (RHE).

Prior to start tests, 50 CV cycles at  $100\text{ mV s}^{-1}$  scan rate and 20 more cycles at  $10\text{ mV s}^{-1}$  scan rate were performed from  $0.0$  to  $1.2\text{ V}$  vs RHE in  $\text{N}_2$  saturated electrolyte, in order to obtain an electrochemically clean and stable working electrode surface.<sup>26</sup>

For each sample, CV were recorded between  $0.0$  and  $1.2\text{ V}$  vs RHE in  $\text{N}_2$ -saturated electrolyte at  $10\text{ mV s}^{-1}$  scan rate.

For the ORR measurements, LSV were recorded at  $5\text{ mV s}^{-1}$  scan rate and with a RDE rotation speed of  $900\text{ rpm}$ . This scan rate value should be sufficiently low to consider the background capacitive current contribution negligible and sufficiently high to allow neglecting the possible effects of impurities in the cell.<sup>27</sup> An electrochemical impedance spectroscopy measurement was done at OCV, with a wave amplitude of  $10\text{ mV}$  and frequencies in the range of  $10\text{ kHz} - 100\text{ mHz}$ , for the evaluation of the high frequency resistance value. This value was used to subtract the ohmic drop contribution from the linear sweep voltammetry curves.<sup>28,29</sup>



### 3. Results and discussion

#### 3.1. Electrochemical characterization

##### 3.1.1. First optimization step

All of the catalysts obtained in the first synthesis optimization part (see Table 1) have been electrochemically tested. The MPC-PPY support without Fe impregnation before and after pyrolysis (S5 and S6, respectively) is also examined for comparison, in order to investigate the effect of the iron presence during the heat treatment. The CV recorded in N<sub>2</sub> saturated acidic and alkaline electrolyte are shown in Fig. 1A and 1C, respectively.

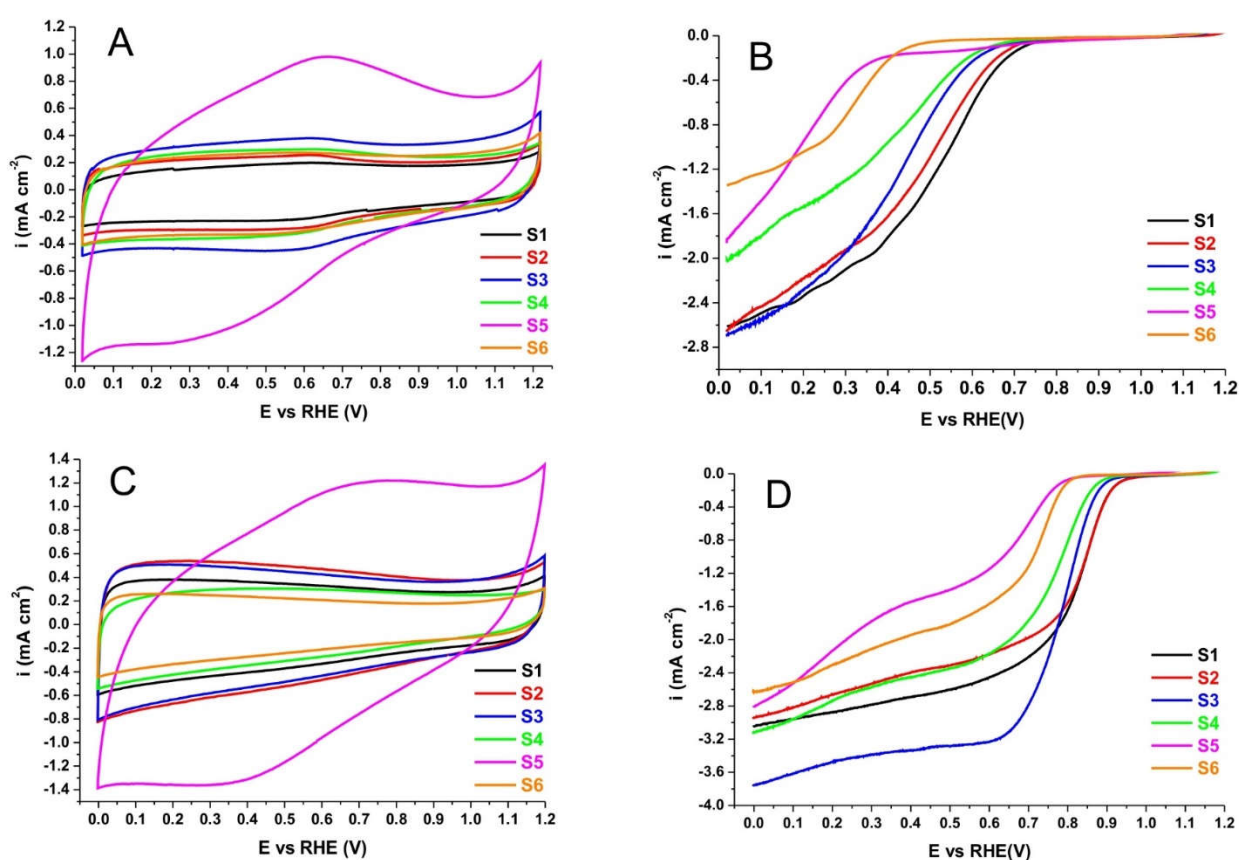
All of the samples exhibit almost the same capacitive current values and CV shape in both acidic and alkaline conditions, except for S5. This could be due to its surface functionalization with polypyrrole, which undergoes to surface oxidation-reduction processes during the potential cycling.<sup>30</sup> This is evidenced by the presence of broad oxidation-reduction peaks, especially for the CV in acid conditions. The surface functionalization, in fact, is responsible of surface pseudo-capacitive phenomena that dramatically increase the capacitive currents in etheroatom-doped carbon materials.<sup>31</sup> For the catalysts synthesized with Fe impregnation (S1-2-3-4), no evident presence of Fe reduction/oxidation peaks is detected. This could be due to the low amount of Fe on the catalysts surface, as evidenced by XPS analyses (see Section 3.2). Most of the Fe-containing moieties should have been removed during the acid leaching treatment with 1 M HCl.

The ORR activities are shown in the LSV plots in Fig. 1B (acid conditions) and Fig. 1D (alkaline conditions). First of all, it is evident that the ORR overpotential is lower in alkaline than in acid conditions, as usually observed for this type of Me-N-C catalysts.<sup>32,33</sup> The catalysts synthesized without the addition of PVP during the impregnation with Fe(II) ions (S1 and S3) are more active in both acidic and alkaline conditions than the respective ones obtained in presence of PVP (S2 and S4). Thus, the use of PVP in this type of wet impregnation synthesis is not useful. In spite of being PVP a N-containing organic molecule, its presence in the solution could cause a covering of the carbon support surface after solvent evaporation. Therefore, the incomplete PVP removal during the pyrolysis heat treatment could have hindered the formation of the active sites.<sup>34,35</sup>

The other aspect of the synthesis that was considered was the pyrolysis of the MPC-PPY support before the impregnation with Fe(II) ions. As shown in Fig. 1B and 1D, S3 and S4 are less active than S1 and S2 in terms of onset potential. This suggests that the preliminary heat treatment is not useful in order to increase the ORR activity. In this preliminary pyrolysis, only C- and N-containing material undergo to the pyrolysis, without the presence of any transition metal sources. Moreover, during this heat treatment at high temperature, all the N initially present in the form of PPY is most likely

incorporated into the MPC carbon structure and/or released as gaseous by-products. Therefore, in the subsequent impregnation and pyrolysis, the Fe(II) ions could only interact with the remaining N atoms that have already been incorporated onto the MPC support. This leads to obtain a less active catalyst. This fact is a further confirmation of the finding that in order to effectively form the ORR active sites, C, N and transition metal sources have to be simultaneously present during the high temperature (600 – 1000 °C) heat treatment.<sup>6</sup>

Thus, the most effective as well as cheaper and less time consuming synthesis method consists in performing the impregnation with Fe(II) ions without adding PVP and using the unpyrolyzed MPC-PPY support. Therefore, S1 was chosen as best catalyst synthesized in the first optimization step.



**Figure 1.** CV recorded at 10 mV s<sup>-1</sup> in N<sub>2</sub>-saturated electrolyte in acid (A) and alkaline (C) conditions for the catalysts synthesized in the first optimization step. LSV curves recorded at 5 mV s<sup>-1</sup> scan rate in O<sub>2</sub>-saturated electrolyte in acid (B) and alkaline (D) conditions for the same catalysts.

### 3.1.2. Second optimization step

The most active catalyst obtained in the first part (S1) was used as support for the syntheses carried out in the second part. Here, a second pyrolysis at 800 °C in inert atmosphere was performed after wet impregnation with different additional Fe(II) quantities (see Table 2).

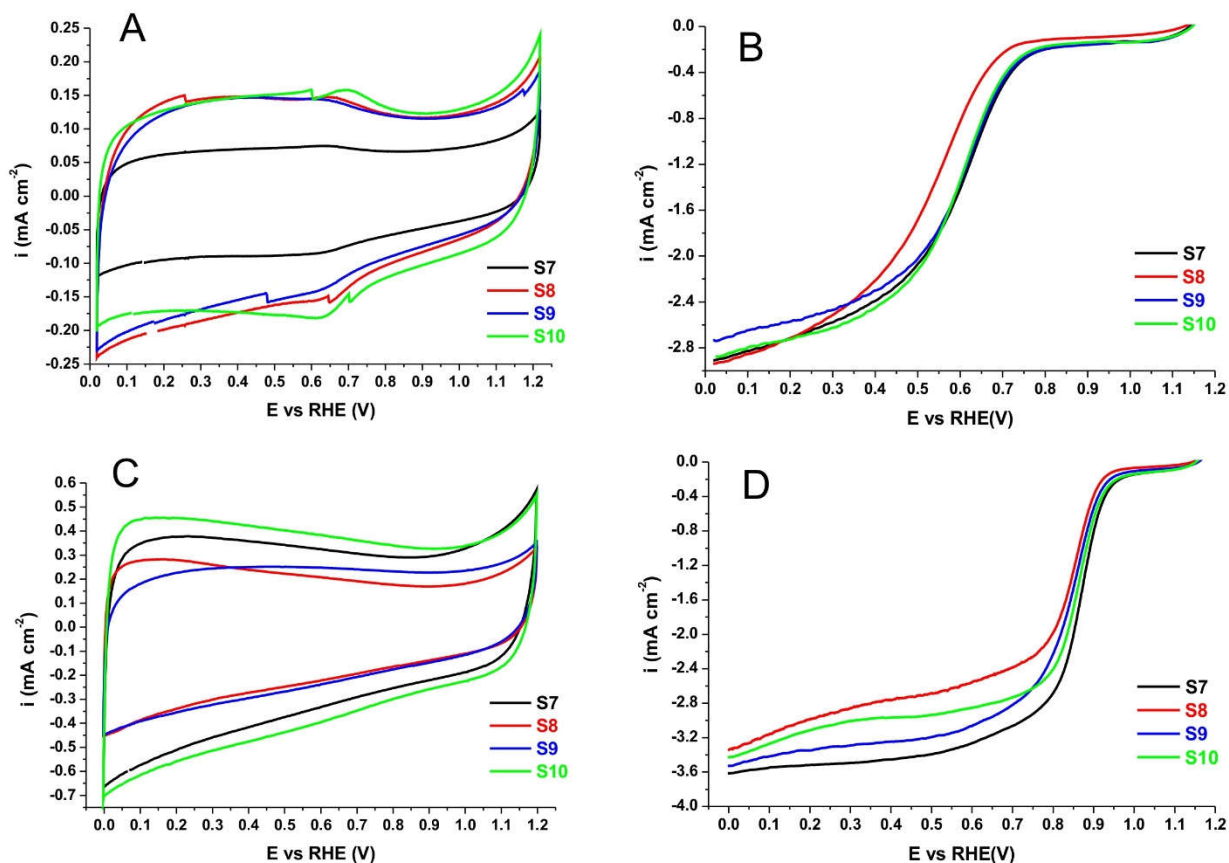
As found in the first optimization step, the CV recorded in N<sub>2</sub>-saturated electrolytes for the samples synthesized in the second step have similar shapes and capacitive current densities (see Fig. 2A and C for tests in acid and alkaline conditions, respectively).

Regarding the ORR electroactivity, as shown in Fig. 2B (acid conditions) and Fig. 2D (alkaline conditions), the most active catalyst was obtained after a second heat treatment without a further impregnation with Fe(II) ions (S7).

Comparing Fig. 1B and Fig. 2B, it is evident how the second heat treatment at 800°C under inert atmosphere is beneficial in order to get a better catalytic performance in acidic conditions, regardless of the amount of Fe deposited on the support in the second impregnation. However, the relative wt. % of Fe has an influence on the electroactivity. In particular, the best catalytic performance is obtained with a simple heat treatment of the support, without any Fe addition (S7). A further impregnation with 15 and 30 wt. % of Fe(II) ions leads to a similar activity (S9 and S10). A lower performance was found for the catalyst impregnated with only 5 wt. % Fe(II) (S8).

The ORR activity increase caused by the second heat treatment is less evident in alkaline conditions, as can be seen comparing Fig. 1D and Fig. 2D. Also under alkaline pH, the highest activity increase is observed without any further Fe addition (S7). An improvement in terms of limiting current density, also occurred for the samples impregnated with the different Fe(II) ions amounts.

In conclusion, performing a second pyrolysis is beneficial for the catalyst performance in both acidic and alkaline conditions. On the contrary, the further impregnation with Fe(II) ions before the second pyrolysis is limiting, or at least, it is not useful to get a better electrocatalytic activity.



**Figure 2.** CV recorded at  $10 \text{ mV s}^{-1}$  in  $\text{N}_2$ -saturated electrolyte in acid (A) and alkaline (C) conditions for the catalysts synthesized in the second optimization step. LSV curves recorded at  $5 \text{ mV s}^{-1}$  scan rate in  $\text{O}_2$ -saturated electrolyte in acid (B) and alkaline (D) conditions for the same catalysts.

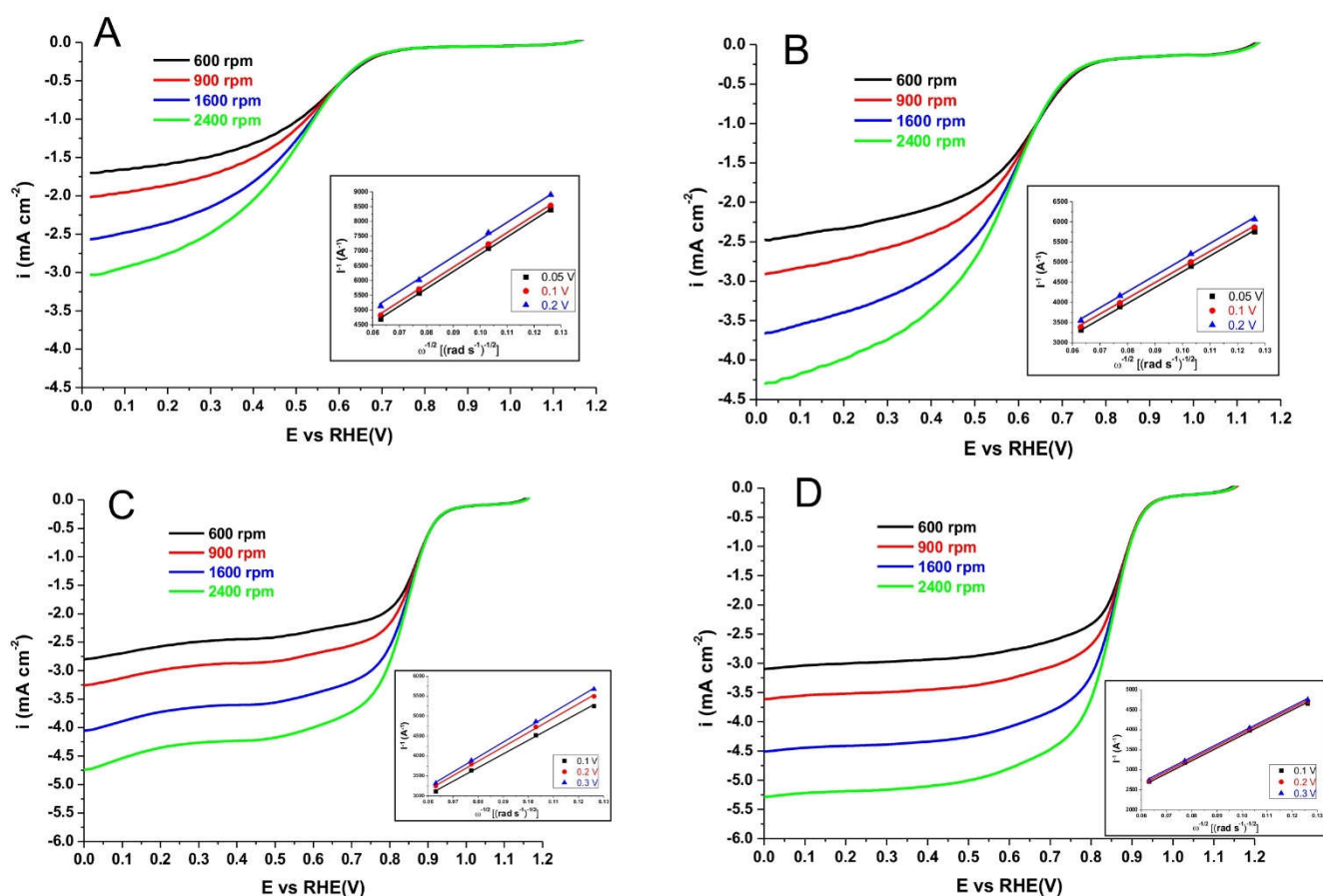
The effects of the second heat treatment in terms of ORR activity and selectivity have been investigated more in depth in both acidic and alkaline conditions. A Koutecky–Levich (K–L) analysis was performed on the most active catalyst heat treated once (S1) and on the most active catalyst heat treated twice (S7). The total number of electrons involved in the oxygen reduction was calculated using the K–L theory, where the limiting current  $I_L$  (A) is given by the following equation:

$$I_L = 0.62nFACD^{2/3}v^{-1/6}\omega^{1/2} \quad (1)$$

Where  $n$  is the number of electrons transferred in the half reaction ( $\text{mol}^{-1}$ ),  $F$  is the Faraday's constant ( $\text{C mol}^{-1}$ ),  $A$  is the electrode area ( $\text{cm}^2$ ),  $C$  is the concentration of dissolved  $\text{O}_2$  ( $\text{mol cm}^{-3}$ ),  $D$  is the diffusion coefficient of  $\text{O}_2$  ( $\text{cm}^2 \text{s}^{-1}$ ),  $v$  is the kinematic viscosity of the electrolyte solution ( $\text{cm}^2 \text{s}^{-1}$ ), and  $\omega$  is the electrode rotation rate ( $\text{rad s}^{-1}$ ).

The overall number of electrons involved in the reaction can be calculated from the slope of the plot of  $I^{-1}$  vs.  $\omega^{-1/2}$ . This calculation can be done at any potential as long as the current is a combination

between kinetic and diffusion currents, as reported in the literature.<sup>36</sup> However, the calculation is more accurate when it is done at a potential where the diffusion current is dominating.<sup>37</sup> Thus,  $n$  was calculated by analyzing the slopes of the K–L plots at different voltages: specifically at 0.05, 0.1 and 0.2 V vs RHE for the test in acidic electrolyte, and 0.1, 0.2, and 0.3 V vs RHE for the test in alkaline electrolyte. As can be seen in the insets of Fig. 3A-B-C-D, the calculated slopes are for both S1 and S7 are almost constant for all of the considered potential values. The number of electrons calculated using these slope values are shown in Table 3. This number is closer to 4 for the sample heat treated twice in both acidic and alkaline conditions. This suggests that the second heat treatment not only helps to get a higher ORR activity, but it is also useful to attain a more complete O<sub>2</sub> reduction, with lower hydrogen peroxide release.



**Figure 3.** LSV curves at different rotation speeds recorded at 5 mV s<sup>-1</sup> scan rate for S1 in acid (A) and alkaline (C) electrolyte and for S7 in acid (B) and alkaline (D) electrolyte. The insets show the corresponding Koutecky–Levich plots at different potentials.

On the sample heat treated once (S1) under acidic conditions the ORR follows almost only the partial reduction pathway, being  $n$  very close to 2 at all of the potential examined. After the second heat

treatment (S7), the number of electrons significantly increases, corresponding to a H<sub>2</sub>O<sub>2</sub> production between 42.7 % and 47.6 %.

In alkaline conditions, the catalyst S1 exhibits a number of electrons in the range between 3.27 and 3.60 at the different potentials examined. This still corresponds to a considerably high H<sub>2</sub>O<sub>2</sub> production (between 20.2 and 36.4 %). With the second heat treatment process the production of H<sub>2</sub>O<sub>2</sub> dramatically decreases to 3.01% at 0.1 V vs RHE potential and to 9.60 % at 0.3 V vs RHE. Therefore, an almost complete 4-electrons oxygen reduction reaction pathway is attained in alkaline conditions at the end of the synthesis optimization.

**Table 3.** Total number of electrons involved in the ORR and corresponding hydrogen peroxide generation (molar %) resulting from the K–L analysis for catalysts S1 and S7 in acid and alkaline conditions.

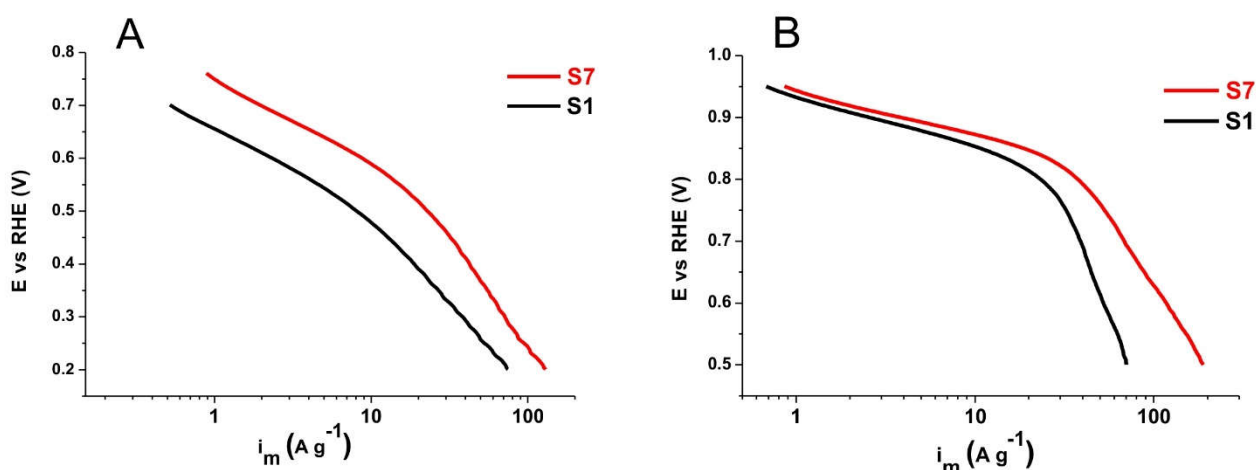
| Acidic conditions   |                 |                      |                                 |                      |                                 |                      |                                 |
|---------------------|-----------------|----------------------|---------------------------------|----------------------|---------------------------------|----------------------|---------------------------------|
| Sample              | N° of pyrolysis | 0.05 V vs RHE        |                                 | 0.1 V vs RHE         |                                 | 0.2 V vs RHE         |                                 |
|                     |                 | N° of e <sup>-</sup> | % H <sub>2</sub> O <sub>2</sub> | N° of e <sup>-</sup> | % H <sub>2</sub> O <sub>2</sub> | N° of e <sup>-</sup> | % H <sub>2</sub> O <sub>2</sub> |
| S1                  | 1               | 2.08                 | 96.14                           | 2.07                 | 94.44                           | 2.03                 | 98.43                           |
| S7                  | 2               | 3.15                 | 42.74                           | 3.11                 | 44.65                           | 3.05                 | 47.63                           |
| Alkaline conditions |                 |                      |                                 |                      |                                 |                      |                                 |
| Sample              | N° of pyrolysis | 0.1 V vs RHE         |                                 | 0.2 V vs RHE         |                                 | 0.3 V vs RHE         |                                 |
|                     |                 | N° of e <sup>-</sup> | % H <sub>2</sub> O <sub>2</sub> | N° of e <sup>-</sup> | % H <sub>2</sub> O <sub>2</sub> | N° of e <sup>-</sup> | % H <sub>2</sub> O <sub>2</sub> |
| S1                  | 1               | 3.60                 | 20.20                           | 3.41                 | 29.33                           | 3.27                 | 36.37                           |
| S7                  | 2               | 3.94                 | 3.01                            | 3.87                 | 6.30                            | 3.81                 | 9.60                            |

The ORR performances of the two best catalysts resulting from the first and the second optimization steps (S1 and S7) are shown in Fig. 4A and B for acid and alkaline conditions, respectively.

The limiting current densities values were used to calculate the mass-transport corrected ORR electro-reduction kinetic activity by the following equation:

$$i_k = -\frac{i_L \cdot i}{i_L - i} \quad (2)$$

where  $i_k$  is the mass transport-corrected current density,  $i$  is the measured current density, and  $i_L$  is the limiting current density. A correction for the ohmic drop was also done, based on the resistance values obtained by the impedance measurements as described in the experimental section. The as-calculated  $i_k$  values can be transformed into specific mass current densities (A g<sup>-1</sup>) simply dividing by the catalyst loading on the electrode (mg cm<sup>-2</sup>).



**Figure 4.** Ohmic drop and mass-transport corrected Tafel plot for catalysts S1 and S7 in acid (A) and alkaline (B) conditions.

### 3.2. Physico-chemical characterization

A complete characterization of the morphology of the materials obtained at the end of each step of the synthesis was done by FESEM. Pictures are shown in Figure S1, S2 and S3. The SBA-15 silica template exhibits the typical uniform rod-like morphology.<sup>38</sup> These short rods, with average length and thickness of about 1  $\mu\text{m}$  and 200 nm respectively, are joined together to form larger agglomerates (Fig. S1 A-B-C-D). The MPC have the same rod-like morphology as the SBA-15. Moreover, by the higher magnification picture, it is evident the presence of a uniform channel-like structure. This indicates that a complete filling of the inner space of the SBA-15 channels occurred during the negative replica synthesis method<sup>39</sup> (Fig. S2 A-B). Thus, an ordered mesoporous carbon material was successfully obtained after the removal of the SBA-15 template.

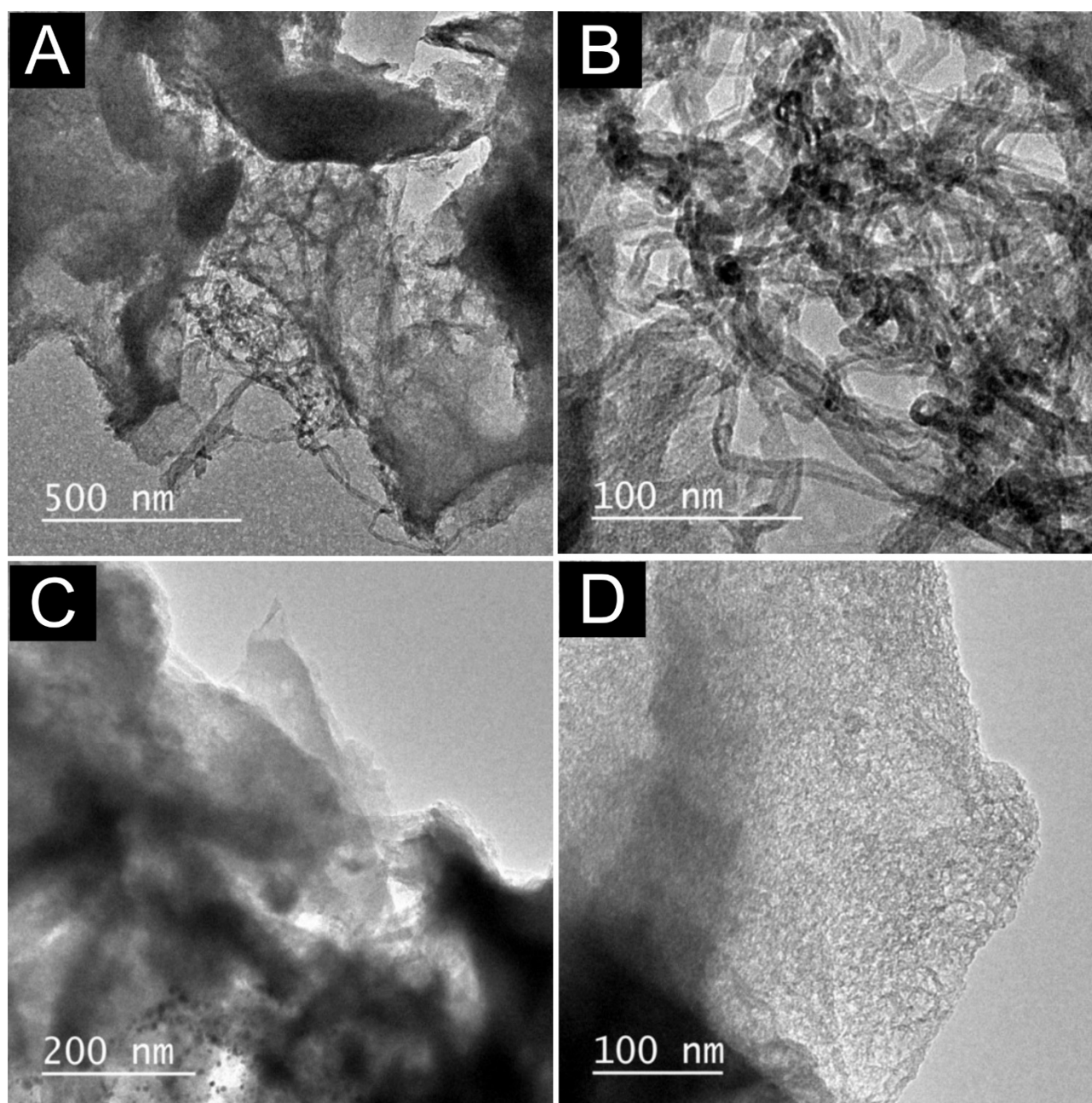
The functionalization with concentrated  $\text{HNO}_3$  and  $\text{H}_2\text{SO}_4$  induces an evident modification of the MPC surface, which becomes more irregular (Fig. S2 C-D). The following step of the synthesis consisted in the pyrrole polymerization. As it was hypothesized, and as it is suggested by Fig. S2 E-F, this polymerization took place onto the MPC support surface. In fact, there is no presence of unlinked PPY flakes and the channels and pores on the MPC structure are no more evident. They have most likely been covered by a uniform PPY layer, which forms due to the presence of hydrogen bonds between the oxygen-containing groups on the functionalized MPC surface and the N–H groups of PPY.

Fig. S3 A-B show the aspect of the best catalyst obtained after the first optimization step (S1). It is evident that a huge structure modification occurred in comparison with the MPC covered with PPY. The pyrolysis at 800°C after the impregnation with Fe(II) ions causes the PPY layer rupture and rearrangement onto the MPC surface, which appears now more irregular, with less presence of the

rod-like structures with ordered channels, although still slightly evident. A highly irregular zone, with aspect similar to a nanotubes agglomerate, is evident in the high magnification picture (Fig. S3 B). The morphology of the most performing catalyst resulting from the second optimization step (S7) is shown in Fig. S3 C-D. A further change in the catalyst aspect occurred during the second pyrolysis. Nevertheless, also in this case the channel-like structure is still partially evident at high magnification, (Fig. S3 D).

The morphology of S7 catalyst was investigated more in detail by TEM analysis (Fig. 5). From the picture taken at lower magnification (Fig. 5A), it can be noticed that the catalyst morphology seems to be like a combination of two different zones. One appears like agglomerates of filamentous particles, similar to carbon nanotubes<sup>11</sup>, while the other has the aspect 2-D flat structure, similar to graphene-like flakes.<sup>40,41</sup> The presence of carbon nanotubes structures is confirmed by the picture at higher magnification (Fig. 5B). The 2-D planar structures, attributable to graphene-like flakes, can be observed in Fig. 5C and 5D. Small dark nanoparticles, typical of metal containing compounds, are also visible in Fig. 5C. These could correspond to Fe-containing crystallites (i.e. metallic Fe, iron oxides, carbides, nitrides)<sup>40,42</sup>, confirming the Fe presence detected by EDX analysis.

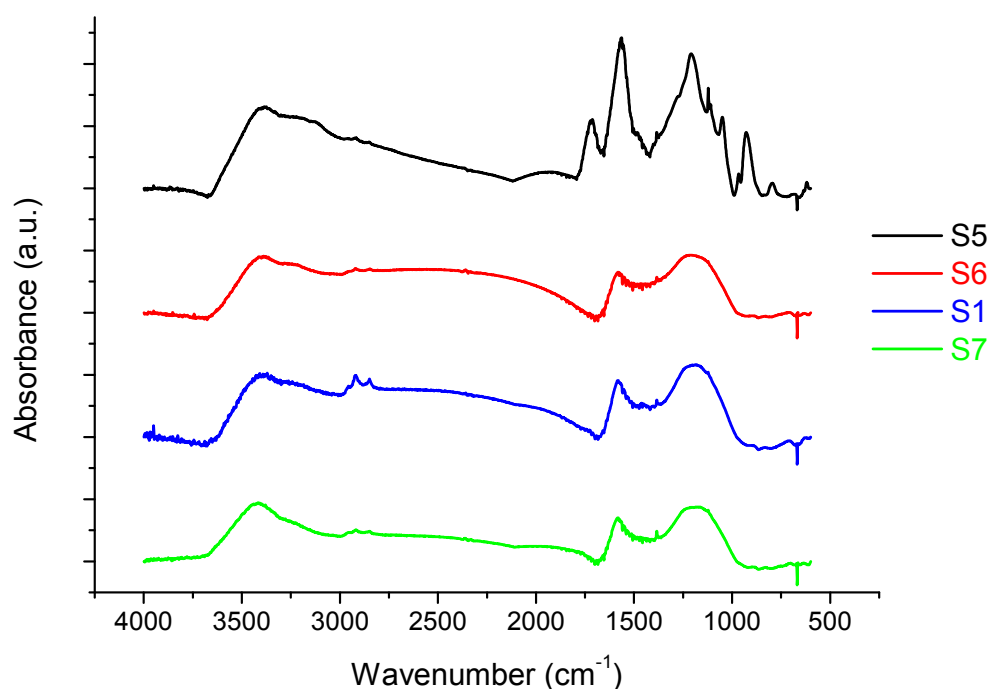




**Figure 5.** TEM images of catalyst S7 at different magnifications.

FTIR spectra (Fig. 6) were measured for the S1 and S7 catalysts. MPC coated with PPY before (S5) and after (S6) pyrolysis were also analysed for comparison. The FTIR spectrum of S5 shows absorbance peaks and bands typical of the pyrrolic structure<sup>43</sup>, as expected due to the presence of PPY. This confirms what observed in the FESEM pictures. Peaks and bands typical of oxygenated organic functional groups are also observed, due to the functionalization of the MPC surface before pyrrole polymerization. In particular, the big band in the wavenumber range  $1650\text{--}1470\text{ cm}^{-1}$  can be attributed to the C–C stretching vibrations of aromatic rings and N–H bend vibrations. The band in the range  $1350\text{--}1000\text{ cm}^{-1}$  is attributable to C–N stretching vibrations in the N-containing aromatic

rings, as well as to the C–H in-plane vibrations of the aromatic rings. The broad peak at 3200–3300  $\text{cm}^{-1}$  is characteristic of the N–H stretching vibration of the pyrrolic ring.<sup>44,45</sup> The peaks and bands characteristic of oxygenated functional groups are in the range 1760–1670  $\text{cm}^{-1}$  (C=O stretching vibration in carbonyls), 990–840  $\text{cm}^{-1}$  (O–H bending vibrations of carboxylic acid), and the two small peaks (more evident in the spectra of S1 catalyst) in the range 2950–2800  $\text{cm}^{-1}$  (O–H stretching vibrations of carboxylic acid). The small band at 820–750  $\text{cm}^{-1}$  can be assigned to the C–H bending vibrations of aromatic rings.<sup>44</sup> These results confirm the presence of PPY on the surface of MPC support, and the high degree of functionalization attained after the reaction with concentrated  $\text{HNO}_3$ – $\text{H}_2\text{SO}_4$  mixture. After pyrolysis, most of the peaks characteristics of the pyrrolic and of the oxygenated functional groups disappear. Therefore, the spectra become more similar to the spectra typical of carbonaceous materials, which are highly transparent to the IR radiation in the region between 400 and 4000  $\text{cm}^{-1}$ .<sup>12</sup> In fact, the FTIR spectra of catalysts S6, S1 and S7 exhibit only two broad absorbance peaks in the ranges 1690–1490  $\text{cm}^{-1}$  and 1350–950  $\text{cm}^{-1}$ , which are attributable to C=N bonding (i.e. pyridine-type) and N–H bonding found on N-containing carbon materials.<sup>46</sup> Similar results are reported in the literature for different types of pyrolyzed Me-N-C electrocatalysts.<sup>8,17,47</sup> This finding suggests that the original PPY structure of the precursor is totally decomposed during the pyrolysis at 800°C, with a substantial recombination of the chemical bonding.<sup>12,46</sup>



**Figure 6.** FTIR spectra of catalysts S1, S5, S6, and S7.

EDX analysis was performed in order to determine the bulk chemical composition of the catalysts, especially regarding the Fe content. The results are shown in Table 4. In both S1 and S7, the total Fe atomic content detected is close to 0.1%, which corresponds to about 0.4 wt. %. This value is much lower than the initial amount of Fe used in the synthesis impregnation process (5 wt. %). This could indicate that most of the Fe is not strongly linked to the support during the pyrolysis, having been washed away during the leaching with 1 M HCl.<sup>8,40,48</sup> However, the Fe content remains constant after the second heat treatment, suggesting that the Fe that was incorporated in the support during the first heat treatment, remains strongly fixed on it.

The MPC after functionalization (MPC<sub>f</sub>) was also analysed in order to assess the effectiveness of the treatment with concentrated HNO<sub>3</sub>–H<sub>2</sub>SO<sub>4</sub> mixture in introducing oxygenated groups onto the MPC support surface. The O content of this sample is 14.26%, confirming that a high amount of oxygen-containing functional groups has been formed. In all of the samples analysed by EDX, small S amounts are detected. This is likely due to the use of H<sub>2</sub>SO<sub>4</sub> in the functionalization process. The Cl impurity detected in S1 could be due to the acid leaching with 1 M HCl.

After the polymerization of pyrrole on the functionalized MPC surface (S5), the O and S contents decrease, while the C content increases. This is most likely due to the formation of PPY, which introduces more C and N atoms. N cannot be detected by our EDX instrument, but its presence is revealed by XPS analysis.

**Table 4.** Elemental compositions (atomic%) resulting from EDX analysis for functionalized MPC, MPC coated with PPY (S5) and the two catalysts S1 and S7 after acid washing with 1 M HCl.

| Sample           | C [at.%] | O [at.%] | S [at.%] | Cl [at.%] | Fe [at.%] | Tot [at.%] |
|------------------|----------|----------|----------|-----------|-----------|------------|
| MPC <sub>f</sub> | 85.39    | 14.26    | 0.35     | -         | -         | 100.00     |
| S5               | 87.14    | 12.67    | 0.20     | -         | -         | 100.00     |
| S1               | 96.35    | 2.63     | 0.48     | 0.45      | 0.09      | 100.00     |
| S7               | 95.14    | 4.64     | 0.13     | -         | 0.09      | 100.00     |

XPS analysis was performed after the acid washing treatment for the catalysts S1 and S7. The MPC coated with PPY before and after pyrolysis without any Fe addition (that is S5 and S6) was also analyzed for comparison, to point out the influence of the iron presence during the pyrolysis. The XPS analysis was conducted with the purpose of determine more precisely the chemical composition of the catalysts surface, detecting the presence of N. The modifications occurring along the different steps of the synthesis optimization process were also evidenced. The XPS survey spectra for all of the analyzed samples are shown in Fig. S4 of the supporting information, and the overall surface elemental compositions are summarized in Table 5.

In the pyrolyzed samples, the main component is C (96.7–93.7 at. %). O is also detected in percentages between 3.9 and 2.9 at. %. The N content is higher for S6 and it decreased for S1 and S7. For the two catalysts impregnated with Fe<sup>2+</sup> ions before the pyrolysis (S1 and S7), the Fe quantity detected was lower than 0.1 at. %. Consequently, the signal of the Fe 2p peaks are too weak to allow the determination of the Fe valence state via deconvolution of the high-resolution peak analysis (not reported here). In S5, the O and N amounts are considerably higher than in the other samples. In particular, the higher oxygen content is due to the functionalization of the MPC support, as was also found by EDX and FTIR analyses. The higher N surface content is attributable to the PPY coating, and it is a further confirmation that the polymerization of pyrrole takes preferentially place onto the surface of MPC<sub>f</sub>. Small S, Cl and F impurities are also detected in some samples. This is attributable to some of the different steps of the synthesis, i.e. the functionalization of MPC with concentrated H<sub>2</sub>SO<sub>4</sub>, the washing with 1 M HCl after the pyrolysis, and the silica template removal by reaction with HF.

**Table 5.** Elemental composition in atomic % of S5, S6, S1 and S7 from XPS analysis.

| Sample | C    | O    | N   | Fe    | S   | Cl  | F   | Tot   |
|--------|------|------|-----|-------|-----|-----|-----|-------|
| S5     | 80.7 | 13.8 | 4.5 | -     | 0.3 | -   | 0.7 | 100.0 |
| S6     | 93.7 | 3.9  | 2.4 | -     | -   | -   | -   | 100.0 |
| S1     | 95.7 | 3.4  | 0.5 | < 0.1 | 0.3 | 0.1 | -   | 100.0 |
| S7     | 96.7 | 2.9  | 0.4 | < 0.1 | -   | -   | -   | 100.0 |

The N 1s high-resolution spectra were recorded and deconvoluted into five different components (see Fig. S5 in the supporting material), corresponding to pyridinic, nitrile and/or N bonded to Fe atom, pyrrolic, graphitic and N-oxidized species, respectively. The relative amounts of each different nitrogen bond type are shown in Table 6, with their respective binding energy. As expected, the most abundant N type on S5 is pyrrolic nitrogen, due to the presence of the PPY coating on the MPC<sub>f</sub> surface. After heat treatment without presence of Fe(II) ions (S6), most of the pyrrolic-type N disappears, suggesting that the typical PPY structure is strongly modified during the pyrolysis. N is incorporated in S6 structure mainly in form of pyridinic and graphitic N. A considerably high percent of oxidized-type N is also detected on S6, probably due to the reaction with the oxidized functional groups on the MPC<sub>f</sub>. Concerning S1, the overall N amount detected on its surface (see Table 5) is considerably lower than for S6. However, the relative proportion of the different N-types is also remarkably different. In particular, a high amount of pyrrolic N is still detected (26.43 at. %), as well as a not negligible amount of nitrile and/or Fe-N<sub>x</sub> N type. Therefore, from these results, the Fe(II) presence seems to favor the formation of more pyridinic and pyrrolic N relative content, limiting the

formation of graphitic and oxidized N. Despite an almost constant overall N content, the relative amounts of pyridinic and pyrrolic N is further increased after the second heat treatment without further impregnation with  $\text{Fe}^{2+}$  ions (S7). This is associated with a remarkable decrease of graphitic N and by the disappearance of nitrile/ $\text{Fe-N}_x$  and oxidized N types.

**Table 6.** Relative contents of the different N types with the respective binding energies resulting from the deconvolution of the N 1s peak from XPS analysis (N1: pyridinic-N; N2: nitrile-N or  $\text{Fe-N}_x$ ; N3: pyrrolic-N; N4: graphitic-N; N5: oxidized-N).

| Sample | Atomic % / Binding Energy [eV] |                     |                      |                      |                      |
|--------|--------------------------------|---------------------|----------------------|----------------------|----------------------|
|        | N1                             | N2                  | N3                   | N4                   | N5                   |
| S5     | <b>6.15</b> / 397.8            | -                   | <b>65.48</b> / 399.9 | <b>20.95</b> / 400.8 | <b>7.42</b> / 405.8  |
| S6     | <b>31.72</b> / 398.3           | -                   | <b>2.47</b> / 399.7  | <b>39.94</b> / 400.8 | <b>25.87</b> / 403.5 |
| S1     | <b>33.61</b> / 398.2           | <b>4.22</b> / 399.3 | <b>26.43</b> / 400.1 | <b>30.81</b> / 401.2 | <b>4.95</b> / 402.3  |
| S7     | <b>43.94</b> / 398.3           | -                   | <b>39.68</b> / 400.5 | <b>16.38</b> / 401.9 | -                    |

Many authors attribute the electrocatalytic ORR activity to pyridinic and/or pyrrolic-N.<sup>40,49</sup> As can be found in the literature, pyridinic-N is usually situated in micropores<sup>50,51</sup>, which are more abundant in S7 than in S1 (see after). This fact could explain the higher ORR activity of S7 with respect to S1 in both acidic and alkaline conditions. As evidenced by the XPS analysis results, the amount of nitrogen incorporated, as well as the abundance of the different nitrogen species, is significantly influenced by the presence of Fe, as well as by the number of heat treatments.<sup>7,8</sup> Regarding the relative abundance of the different N types, the quantities found in our samples are comparable to the values found in the literature for similar Me-N-C electrocatalysts.<sup>37,45,52,53</sup>

Nitrogen doping occurring during a heat treatment at T between 700 and 1000 °C in presence of a transition metal ion is essential to significantly increase the ORR catalytic activity of carbon-based materials. However, neither the precise structure of the active sites, nor the exact role of the transition metal in them have been clearly identified so far.<sup>54</sup> In particular, no direct relation was found between total N and Fe content and catalyst electroactivity towards ORR. This suggests that even if nitrogen atoms are known to be part of active sites, their total amount is not the limiting factor for the ORR electroactivity.<sup>55</sup> The role of Fe is however essential, as suggested by the poor electroactivity of the catalyst pyrolyzed without having been impregnated with  $\text{Fe}^{2+}$  ions (S6), even if its total N content is higher. This could indicate that in this type of catalysts, iron could play an active role in the ORR electrocatalysis, as suggested by Yeager.<sup>54</sup> However, iron could also play only the role of intermediate during the pyrolysis, when the formation of the real active sites takes place. This is in accordance with the model of ORR active sites in Me-N-C catalysts proposed by Wiesener.<sup>54</sup>

Nitrogen physisorption isotherms were recorded for the most significant samples along the synthesis optimization process. Figure 7A shows the isotherms of the MPC support and the SBA-15 silica used as templating agent. According to the IUPAC classification, the SBA-15 isotherm shape belongs to type IV, which shows the typical hysteresis loop associated with capillary condensation taking place in mesopores.<sup>56</sup> The hysteresis loop shape is classified as type H1, with the presence of the two almost vertical and parallel branches, associated with materials having a narrow distribution of pore size like ordered mesoporous silica.<sup>38,56</sup> The MPC isotherm shape can also be classified as type IV. The hysteresis loop in this case is an intermediate between type H1 and H4, being more horizontal and extended over a wide range of  $P/P^0$ . In the low  $P/P^0$  range both isotherms have a strong type I character, that is indicative of microporosity. Some results of the porosimetry analysis are shown in Table 7. After the coating of the MPC with PPY (S5), the surface area and pore volume decrease dramatically. This is most likely due the occlusion of part of the pores by the PPY layer. After the first heat treatment (S1 and S6), regardless of the Fe addition, the micropores content significantly increases. However, this is not associated with a significant increase in the overall surface area in comparison with the support. The shape of the adsorption-desorption isotherms of the pyrolyzed samples remains similar to the one of the MPC coated with PPY (see Figure 7B). These isotherms can be classified as an intermediate between type IV and type II. Type II isotherms exhibit a steep increase at high  $P/P^0$  values, and are typical of non-porous or macroporous materials. The higher presence of macropores in the pyrolyzed samples is also confirmed by FESEM images.

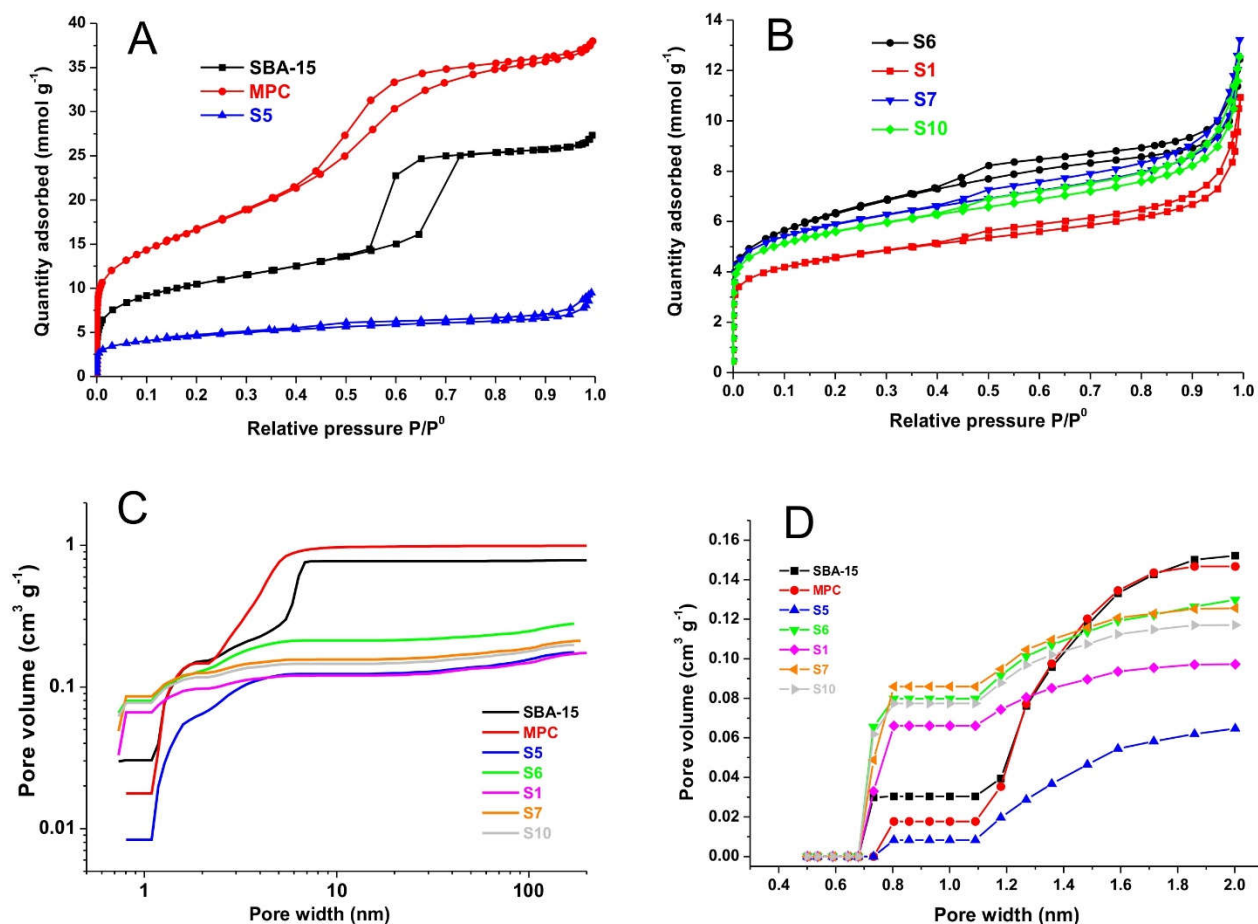
**Table 7.** Properties calculated from the nitrogen physisorption analysis for SBA-15 silica, MPC, S5, S6, S1, S7 and S10. ORR electrocatalytic activity in acid and alkaline conditions for the catalysts S1, S7 and S10.

| Sample | BET surface area [m <sup>2</sup> g <sup>-1</sup> ] | micropores area by t-plot [m <sup>2</sup> g <sup>-1</sup> ] | micropores area by DFT [m <sup>2</sup> g <sup>-1</sup> ] | total pore volume [cm <sup>3</sup> g <sup>-1</sup> ] | micropores volume by t-plot [cm <sup>3</sup> g <sup>-1</sup> ] | micropores volume by DFT [cm <sup>3</sup> g <sup>-1</sup> ] | BJH average pore width [nm] | ORR activity ACID @ 0.75 V vs RHE [A g <sup>-1</sup> ] | ORR activity ALKALINE @ 0.9V vs RHE [A g <sup>-1</sup> ] |
|--------|--|---|--|--|--|---|-----------------------------|--|--|
| SBA-15 | 796.9  | 247.9   | 255.0  | 0.912  | 0.120  | 0.152   | 4.9                         | -  | -  |
| MPC    | 1305.5   | 165.3   | 232.4  | 1.273  | 0.084  | 0.147   | 4.0                         | -  | -  |
| S5     | 340.9  | 87.6  | 100.4  | 0.268  | 0.049  | 0.064   | 5.0                         | -  | -  |
| S6     | 469.1  | 148.1   | 285.4  | 0.346  | 0.080  | 0.130   | 4.9                         | -  | -  |
| S1     | 326.0  | 161.6   | 217.9  | 0.290  | 0.086  | 0.097   | 7.4                         | 0.298  | 2.645  |
| S7     | 426.0  | 221.8   | 283.4  | 0.354  | 0.115  | 0.126   | 6.8                         | 0.998  | 3.914  |
| S10    | 405.6  | 186.2   | 265.8  | 0.339  | 0.099  | 0.117   | 6.8                         | 0.845  | 3.012  |

For all of the pyrolyzed samples, the contribution of micropores to the overall surface area and pore volume is extremely high. In fact, considering the data calculated by the DFT model, the microporous surface area represents a fraction between 67 and 61 % of the total BET surface area. For the microporous volume, this fraction ranges from 33 to 38 %. The cumulative overall and microporous

pore volume vs. pore size distribution calculated by the DFT model are shown in Figure 7C and 7D, respectively. The high microporosity of these materials is confirmed by the strong type I isotherm character at low  $P/P^0$  range (see Figure 7B). The hysteresis loops do not exhibit any limiting adsorption at high  $P/P^0$  values. Therefore, they can be classified as type H3 hysteresis. This is usually associated with aggregates of plate-like particles giving rise to slit-shaped pores, typical characteristic of graphene-like platelets<sup>40,41,46,57</sup>, as confirmed also by the results of TEM analysis.

Furthermore, it is evident that performing the second heat treatment leads to increase both overall and micropores surface area and volume. The formation of a microporous structure during the heat treatment is favorable to host the active sites for ORR, as mentioned in several literature works.<sup>5,50,55</sup> In particular, an interesting correlation must be pointed out between the overall and microporous surface area (and volume) and the ORR electroactivities of these Fe-N-C catalysts in both acidic and alkaline conditions (Table 7). The ORR electroactivity increases with the total and microporous surface area and volume, and the second pyrolysis causes an increase of both these factors. Analogous results were found by Jaouen et al. for different types of Me-N-C (Me = Fe, Co, Cu) electrocatalyst for ORR in acidic conditions. They found a direct correlation between the surface area of pores with diameter lower than 2 nm and the ORR activity in RDE.<sup>55</sup> Similarly to our results, there was not any relations between catalysts electroactivity and total N content. Moreover, there was a direct correlation between the bulk Fe content and the ORR electroactivity only up to a maximum Fe content of 0.1 wt. %.<sup>58</sup> This quantity is considerably lower than the Fe amount employed in the second optimization step of our synthesis procedure. This fact could confirm the uselessness of performing a further impregnation with  $\text{Fe}^{2+}$  ions before the second heat treatment.



**Figure 7.** (A) Nitrogen adsorption/desorption isotherms of SBA-15 silica, MPC and MPC<sub>f</sub> coated with PPY (S5). (B) Nitrogen adsorption/desorption isotherms of some of the pyrolyzed samples (S6, S1, S7 and S10). (C) Cumulative total pore volume vs. pore size by DFT model. (D) Cumulative pore volume vs. pore size restricted to the microporous zone.

#### 4. Conclusions

An optimization in two parts has been performed on the synthesis method of a Fe-N-C electrocatalyst for ORR using polypyrrole as N source, MPC as C support and Fe(II) acetate as Fe<sup>2+</sup> ions source. In the first part, the addition of a N-containing surfactant (PVP) during the wet impregnation with Fe(II) ions, and the pyrolysis of the MPC support coated with PPY before the impregnation were investigated. These two synthesis parameters were found to not be useful to get an ORR activity improvement in both acid and alkaline conditions. In the second part, the effect of a second pyrolysis at 800°C in inert atmosphere was evaluated, together with the effect of the impregnation with more Fe in different quantities. The second heat treatment was found to be beneficial for the catalyst ORR activity. Otherwise, the addition of further Fe(II) before the second pyrolysis was found to be not necessary. In fact, the catalyst pyrolyzed twice without any further Fe addition was the most active one under both acidic and alkaline medium. The catalysts morphology, physical properties and



chemical composition were characterized by many instrumental methods. In particular, the formation of an interesting structure containing carbon nanotubes-like and graphene-like structures in the heat-treated catalysts was detected. The presence of Fe-containing structures was also detected in the form of nanoparticles. The nitrogen fixation on the carbonaceous support under different binding types was also revealed by XPS analysis. The total N and Fe contents, were not found to be the limiting factor for the ORR activity in this type of catalysts. However, the ORR activity seems to be related to the relative amounts of both pyridinic and pyrrolic nitrogen, which are more abundant after the second pyrolysis. The results of the nitrogen physisorption and porosimetry analysis evidenced that the first heat treatment significantly increases the micropores content. Performing a second heat treatment causes an increase of both total and micropores surface area and volume. All of the pyrolyzed samples exhibit a very high amount of microporous surface area (between 50 and 65% of the total surface area). The increase of the microporosity in these Fe-N-C catalysts is in strict relation with the increase in ORR electrocatalytic activity.

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## Supporting Information

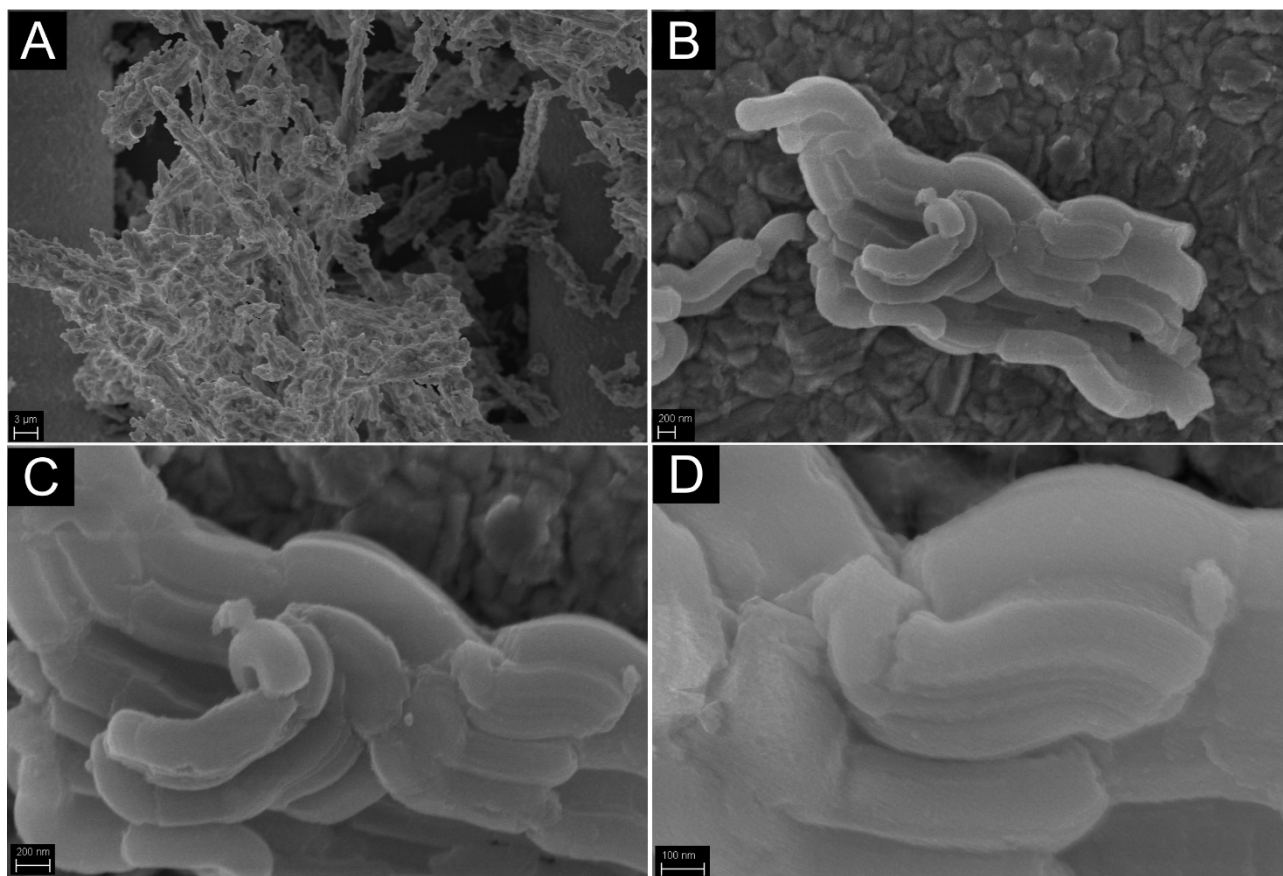


Figure S1. FESEM pictures at different magnifications of SBA-15 silica used for the synthesis.

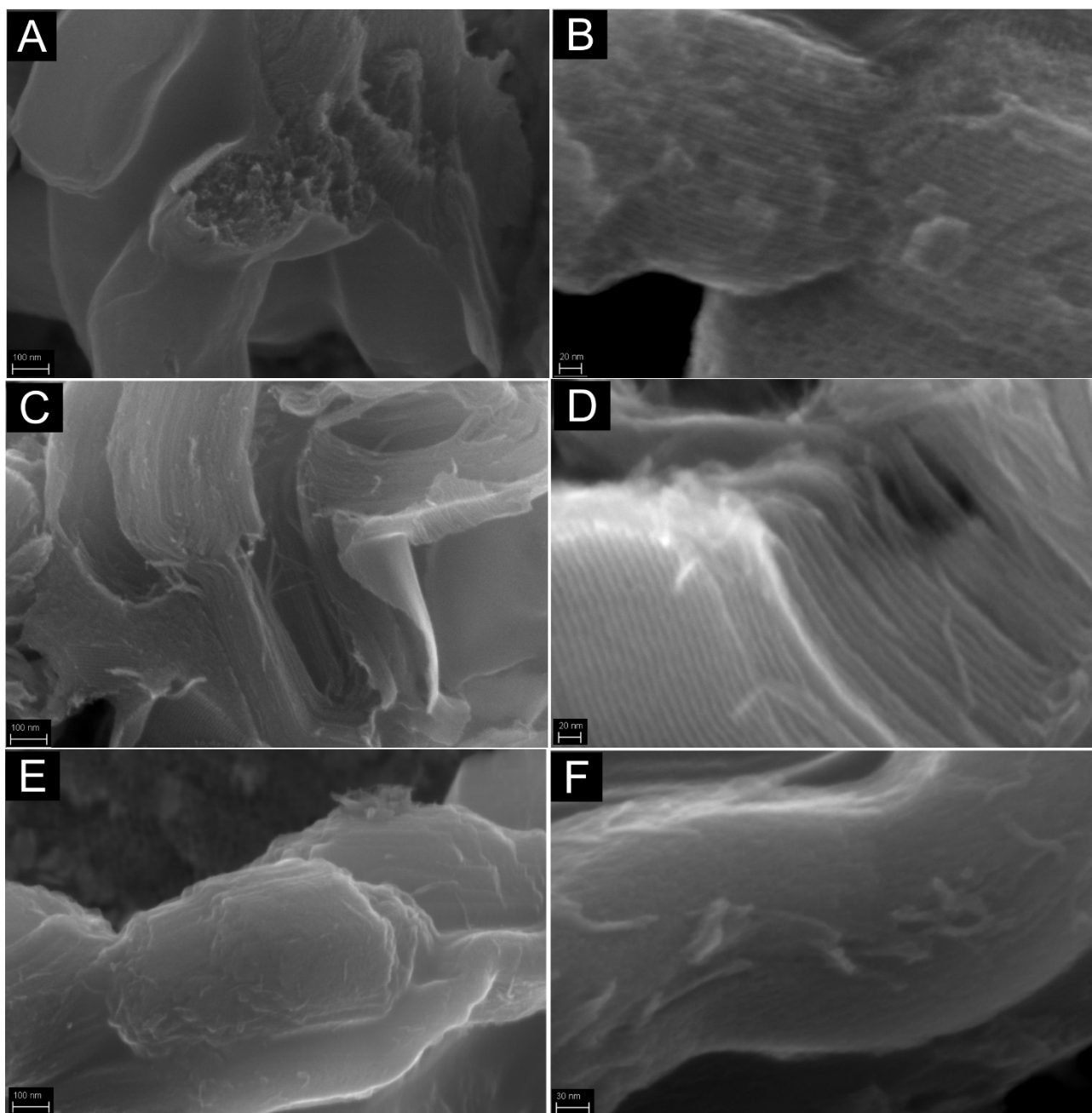


Figure S2. FESEM pictures at different magnifications of MPC (A-B), MPC<sub>f</sub> (C-D) and MPC-PPY (E-F).

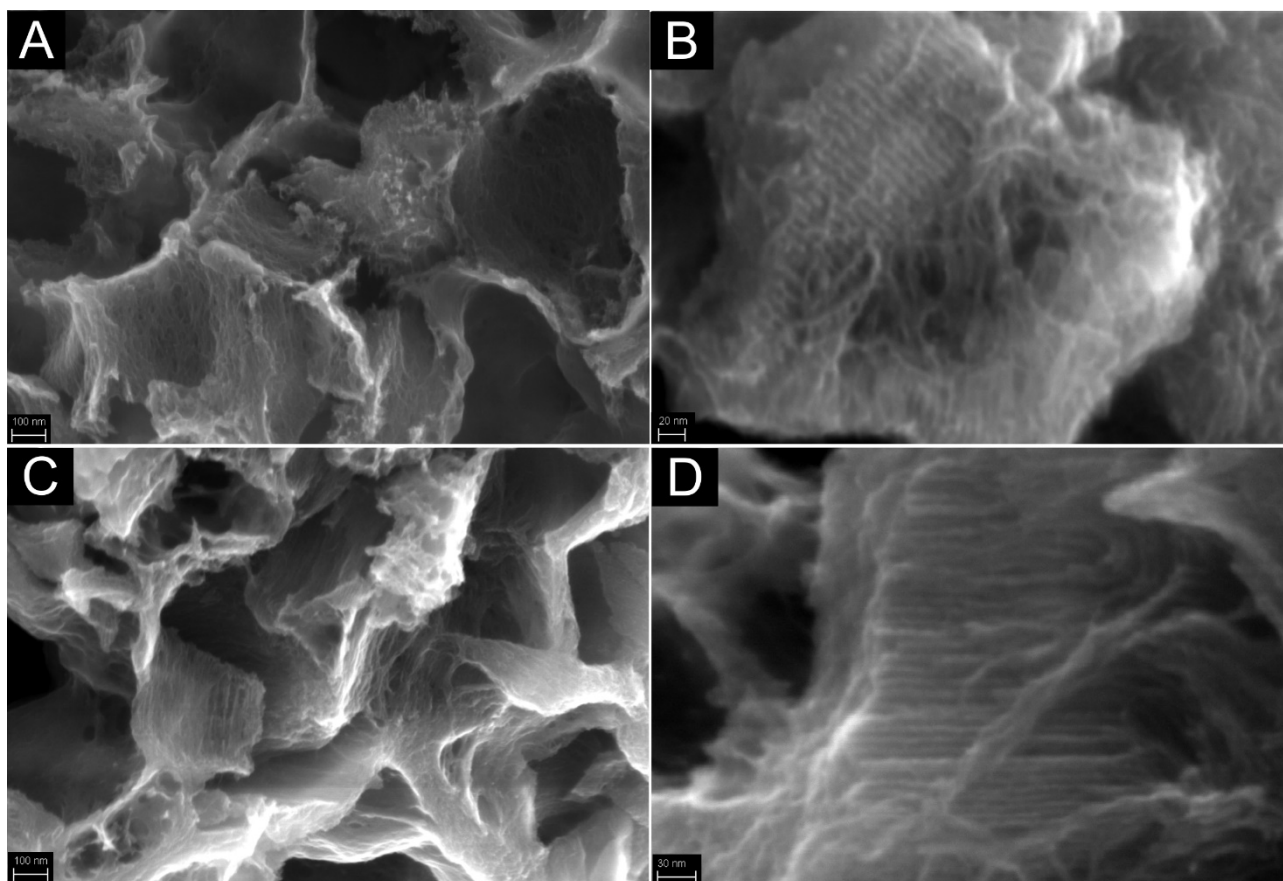


Figure S3. FESEM pictures at different magnifications of the catalysts S1 (A-B) and S7 (C-D).

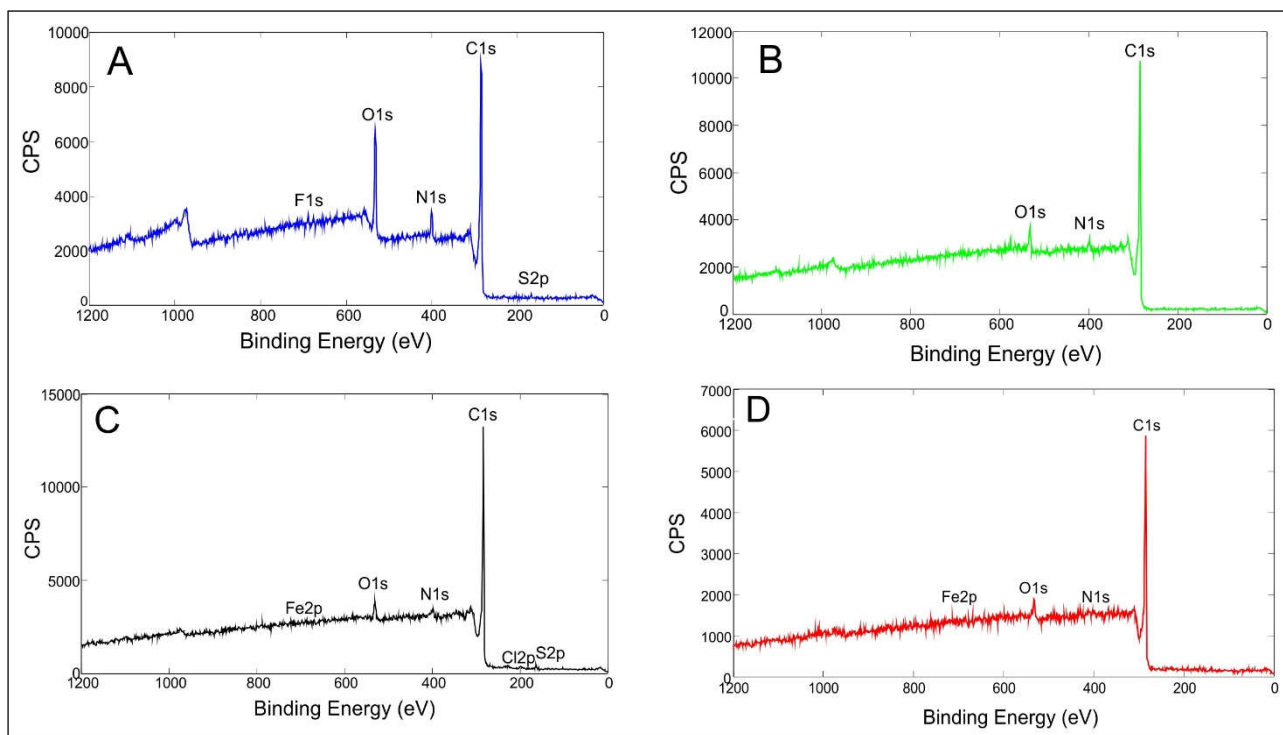


Figure S4. XPS survey spectra of S5 (A), S6 (B), S1 (C) and S7 (D).



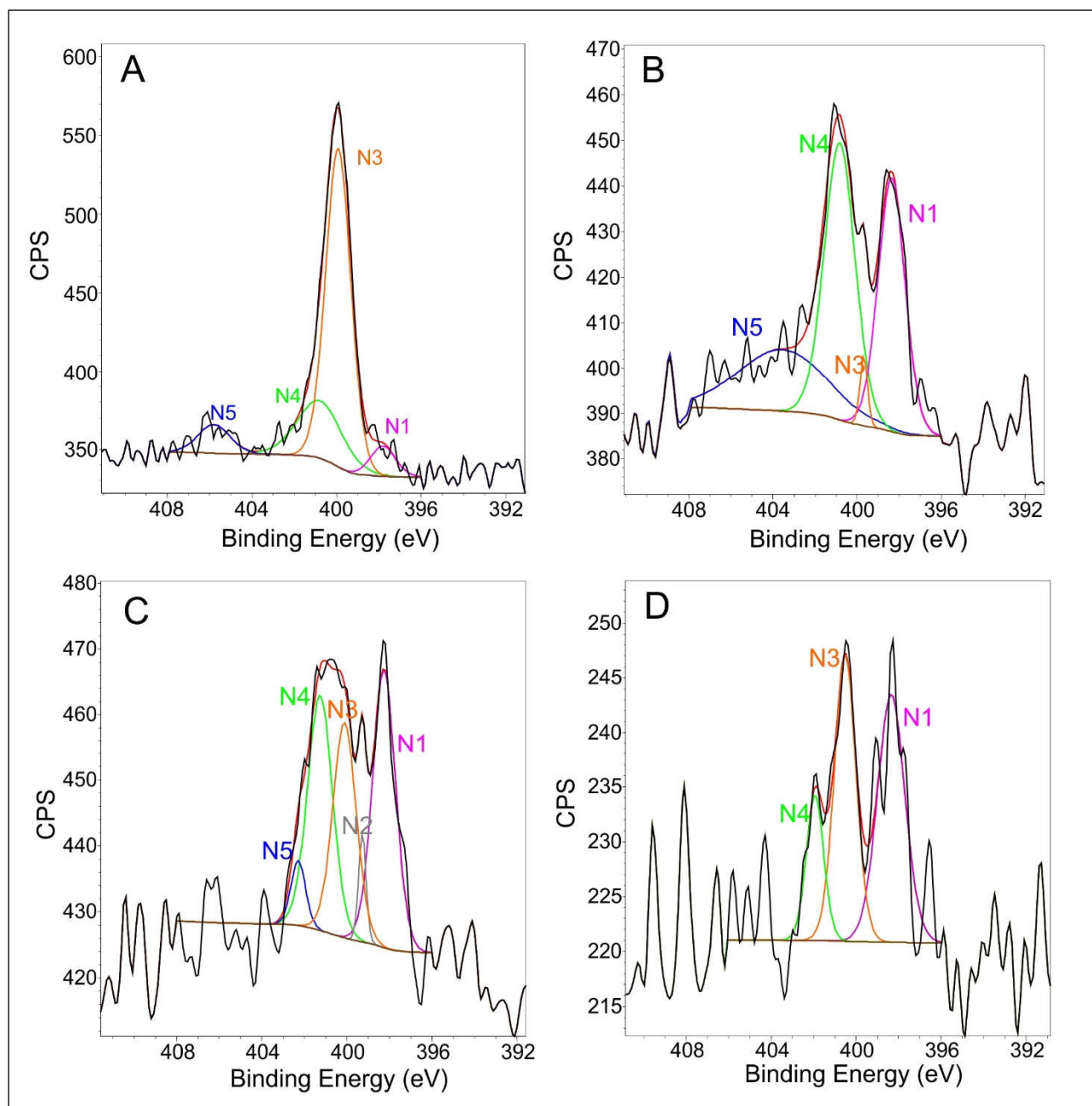


Figure S5. High resolution N 1s XPS spectra of S5 (A), S6 (B), S1 (C) and S7 (D). The black and red lines are the raw and the fitted spectra, respectively. The purple, grey, orange, green and blue lines respectively correspond to pyridinic (N1), nitrile/Fe-N<sub>x</sub> (N2), pyrrolic (N3), graphitic (N4) and oxidized (N5) nitrogen peaks resulting from the deconvolution. The brown line is the Shirley background.



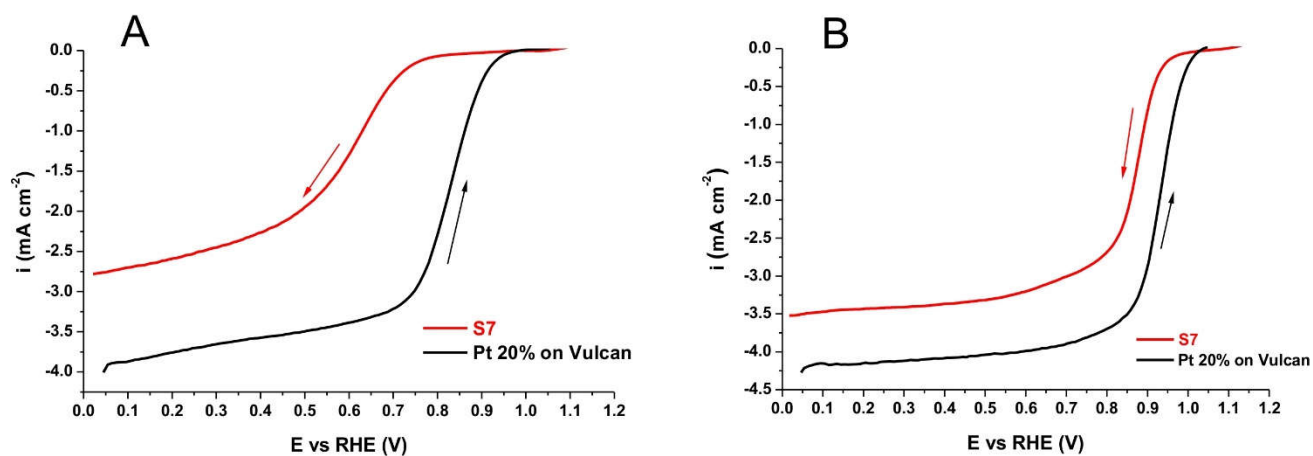
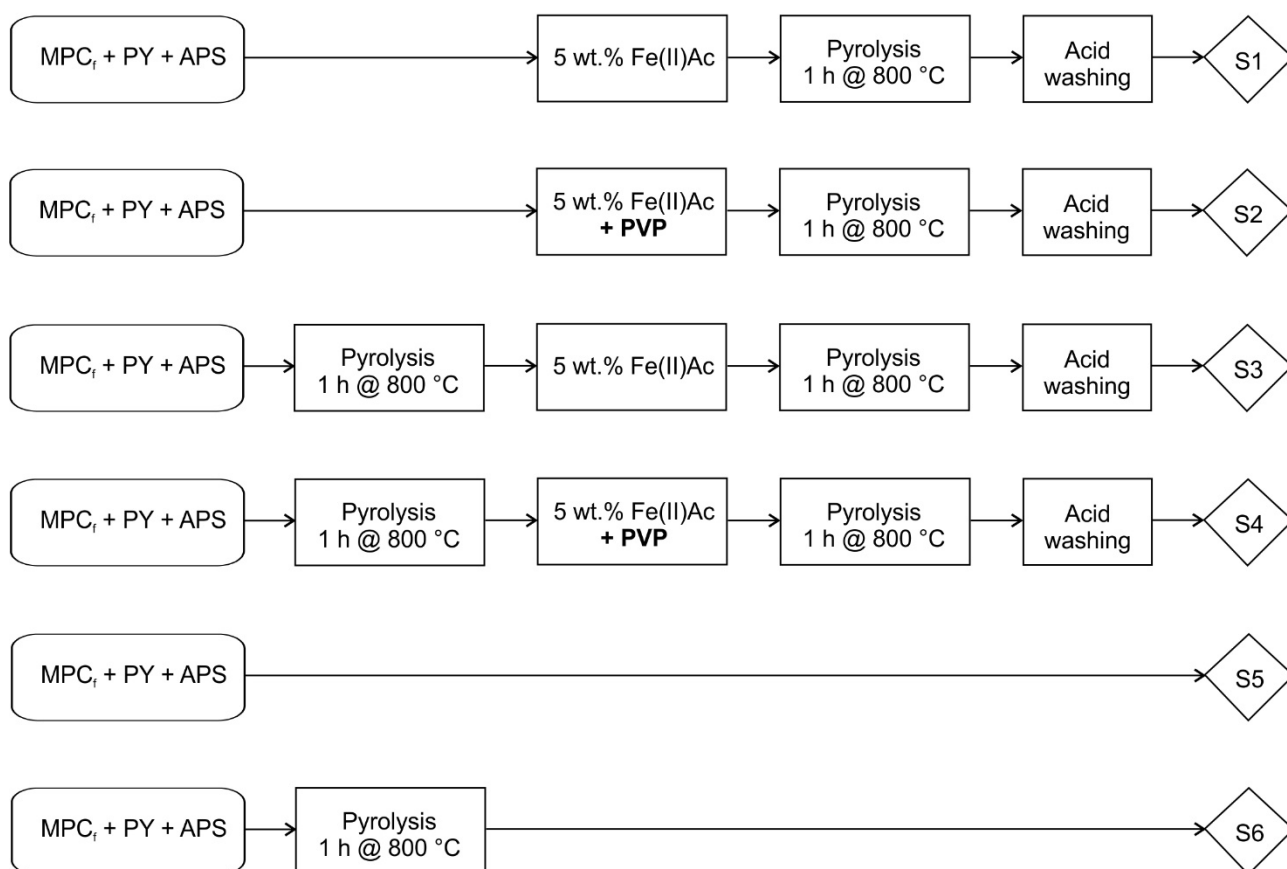


Figure S6. ORR comparison of the most performing catalyst synthesized in this work (S7) with a commercial Pt-based catalyst (20% Pt on Vulcan – Quintech) in acid (A) and alkaline (B) conditions. LSV recorded at  $5 \text{ mV s}^{-1}$  scan rate and with RDE rotation speed 900 rpm. For acid conditions the electrolyte was 0.5 M  $\text{H}_2\text{SO}_4$  for our catalyst and 0.1 M  $\text{HClO}_4$  for Pt-based catalyst. For alkaline conditions the electrolyte was 0.1 KOH for both catalysts.

### First optimization step



### Second optimization step

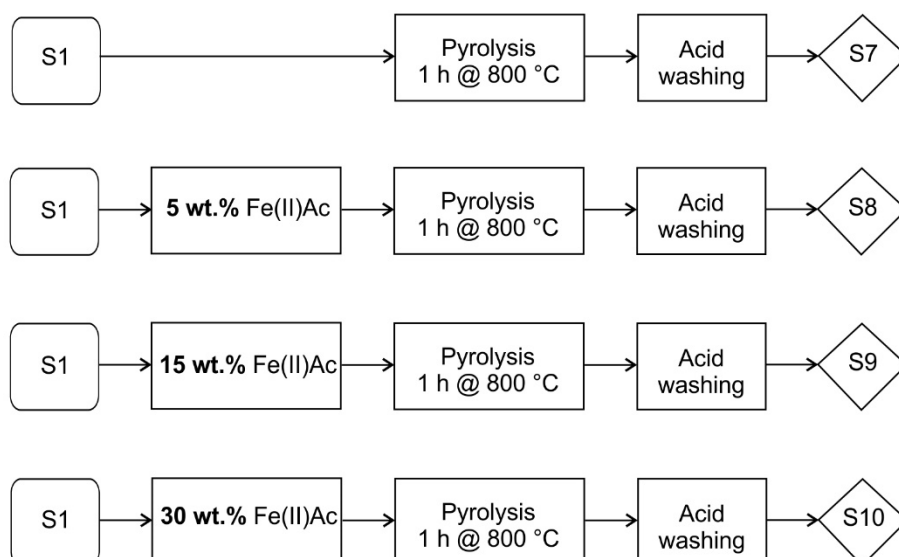


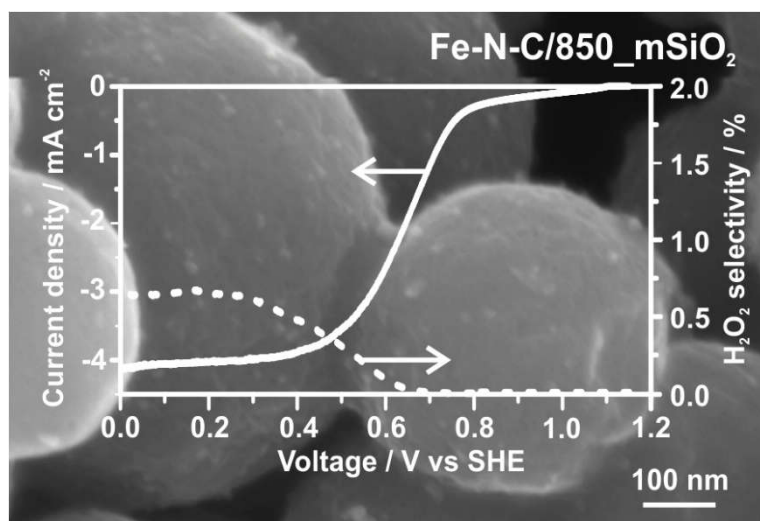
Figure S7. Scheme of the synthesis procedures for all of the different samples.



## CHAPTER 5. Varying the morphology of Fe-N-C electrocatalysts by templating Iron Phthalocyanine precursor with different porous SiO<sub>2</sub> to promote the Oxygen Reduction Reaction.

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### 1. Introduction

Platinum is one of the most effective element used in polymer electrolyte membrane fuel cell (PEMFC) catalysts due its unique electrocatalytic properties (low binding energy to O bond) promoting the oxygen reduction reaction (ORR) and oxidation of alcohols [1]. Unfortunately, its high cost for the preparation of cathodic ORR electrocatalysts makes PEMFC commercialization very difficult. It is proved that almost the 55% of the total cost of PEMFC is directly related to the catalyst-based electrode components [2,3]. One of the possible solutions to reduce the catalyst cost, is the use of non-noble electrocatalysts, such as transition metals chelates and macro cyclic complexes [4]. Typically catalysts such as Iron (III) tetra(pentafluorophenyl) (FeTPFPF), cobalt fluoro-phthalocyanine (CoHFPC), cobalt tetramethoxyphenylporphyrin (CoTMPP) and non-noble chalcogenide ORR electrocatalysts have been used during the last years because of their good electroactivity, but they are still far away from the performance of Pt-based catalysts [5–7]. One of the big challenge of non-noble catalyst is to determine the nature of the active sites as well as the mechanism how O=O bridge is broken, making difficult to achieve rational design of M-N-C

electrocatalysts for ORR [8]. Apart from the advanced research in this field, from several hundred millions of years nature performs the ORR process in a simple and elegant way, i.e., in green plants enzymes metabolizing oxygen [9]. Another natural process is the transport of dioxygen into human bodies through cytochrome C oxidase (CcO) reaction cycle, where a heme-Fe/O<sub>2</sub> and heme-Cu/O<sub>2</sub> couple (a mixture of Fe<sup>II</sup>-tetrakis(2,6-difluorophenyl)porphyrinate with Cu<sup>I</sup>-N,N-bis{2-[2-(N',N'-4-dimethylamino)pyridyl]ethyl}methylamine) reduces oxygen without peroxide production, located in the terminal oxidase of cellular respiration system [10]. This biological system presents a complex interaction, where five coordinated metal structures with an axial ligand from the back site are combined together. Several bio-inspired electrocatalysts for ORR have been studied including copper/heme-binuclear CcO model [11], multicopper complexes [12] and iron phthalocyanines [9,13]. In the case of the most used Pt-based electrocatalysts oxygen is reduced by breaking dioxygen (O=O bond, 498 kJ mol<sup>-1</sup>) by a “bridge cis” mechanism having 4 electron pathway and low overpotential [14].

Typically, electrocatalysts are produced by mixing an external carbon source, which acts as support, with a precursor of the active sites. Mesoporous carbons, carbons nano-network or nano-tubes, or carbon xerogels can be used as support [15–18]. The precursor could be either a macromolecule containing N, Fe and C, or a simple gaseous molecule as ammonia [19]. The use of an external carbon source implies that this carbon must undergo to a graphitization process, which proceeds in parallel with the graphitization of the carbon belonging to the Fe-N precursor. The different nature of the two types of carbon could have an influence on the overall graphitization process during the pyrolysis step, producing different morphological carbons. The morphology could negatively affects the electro-activity by reducing the accessibility of oxygen to the reactive sites during the ORR [20].

In this work, the use a non-noble metal catalyst based on a rich iron-nitrogen molecule, the iron phthalocyanine (FePc: C<sub>32</sub>H<sub>16</sub>FeN<sub>8</sub>), containing a Fe–N bridge, is used for the preparation of active electrocatalysts for ORR. The influence of the temperature and the morphology are studied to obtain a uniform structure able to increase the electroactivity and to reduce the peroxide production during the ORR. Considering the highly carbon content of the FePc molecule, the electrocatalysts are prepared without using any other external carbonaceous support to preserve their homogeneity and favor an homogeneous graphitization during the thermal treatment [21,22]. Here the morphology of the electrocatalysts is varied by means of different mesoporous silica templating agents to evaluate the effects on the porosity, electrocatalytic activity and stability [23].

## 2. Experimental part

### 2.1. Chemicals

Iron Phthalocyanine  $C_{32}H_{16}FeN_8$  (FePc), mesoporous Silica ( $mSiO_2$ ), Isopropanol with 99.5 wt. %, Hydrofluoric acid 48 wt. %, Hydrochloric acid 37 wt. %. Sulphuric acid with 97 wt. %, Nafion® solution containing 5 wt. % Nafion®, tetraethyl orthosilicate 98% and Pluronic® P123 were purchased from Sigma Aldrich. Nitrogen and Oxygen gases were supply in cylinders by SIAD with 99.999% purity. All aqueous solutions were prepared using ultrapure water obtained from a Millipore Milli-Q system with resistivity  $>18\text{ m}\Omega\text{ cm}^{-1}$ .

### 2.2. Electrocatalysts synthesis

#### 2.2.1. Synthesis of based Fe-N electrocatalysts

FePc was thermal treated in an inert atmosphere ( $N_2$ ) using a tubular quartz reactor. Different samples were prepared by varying the temperature from 600 to 900 °C. The desired temperature was reached with a heating rate of  $2.5\text{ }^{\circ}\text{C min}^{-1}$ , and maintained constant for 2 h. Then the furnace was switched-off and left cooling down naturally at room temperature. After the pyrolysis process, the catalysts prepared were acid washed with 1 M HCl under reflux at 80 °C for 3 h.

#### 2.2.2. Synthesis of silica template

Porous silica (SBA 15) was synthesized as described by Zeng *et al.* [24]. Typically, Pluronic® P123, deionized (DI) water, and HCl were added to an aqueous solution, and the mixture was stirred at 35 °C. After P123 was completely dissolved, tetraethyl orthosilicate was added and the solution was stirred for 24 h. The solution was heated at 150 °C for 24 h. The resulting white-colored precipitate was filtered and washed twice with DI water, and then dried in an oven at 60 °C for 24 h. Finally, the dried sample was calcined at 550 °C for 5 h in calm air.

#### 2.2.3. Synthesis of modified Fe-N-C electrocatalysts

Commercial mesoporous Silica ( $mSiO_2$ ) and SBA 15 in house prepared were used as template for altering the structure of basic Fe-N-C electrocatalysts. Silicon oxides were used in a 30 wt. % respect to the FePc, followed by a mixing process by with a mixer apparatus (Retsch Mixer Mill MM 200) for 1 h at 10 Hz. The precursors were thermal treated under the same conditions of basic Fe-N-C electrocatalysts, using a fixed temperature of 850 °C for 2 h. After pyrolysis, the powders were grounded and leached with 5 wt. % HF in order to remove the templating agent. A second acid treatment was conducted at 80 °C in 1 M HCl reflux bath in order to remove any other oxide and to functionalize the electrocatalysts, as well.

### 2.3 Chemical-physical characterization of the electrocatalysts

Specific surface areas ( $S_{BET}$ ) were determined using the Brunauer-Emmet-Teller (BET) method within the relative pressure range of 0.1–0.3 on an ASAP 2020 C Micromeritics Instrument. Nitrogen adsorption isotherms were recorded at  $-196\text{ }^{\circ}\text{C}$  within the relative pressure range of 0–1. Prior to adsorption, samples were placed in the cell and evacuated at  $130\text{ }^{\circ}\text{C}$  for 3 h under high vacuum. Field-emission scanning electron microscopy (FESEM JEOL-JSM-6700F instrument coupled with an Energy Dispersive X-ray Spectrometry (EDS) Detector (OXFORD INCA) were performed to analyze the morphology and EDS. Fourier transform infrared spectroscopy (FTIR) measurements were performed on catalysts mechanically mixed with KBr and pressed. IR spectra were collected in air at  $2\text{ cm}^{-1}$  resolution on a Bruker Equinox 55 FTIR spectrophotometer, equipped with a MCT (Mercury Cadmium Telluride) detector.

X-ray photoelectron spectroscopy (XPS) was performed to determine the elemental surface composition of the catalysts. The analysis was carried out using a Physical Electronics PHI 5000 Versa Probe electron spectrometer system with monochromated Al  $K\alpha$  X-ray source ( $1486.60\text{ eV}$ ) run at 15 kV and 1 mA anode current. The survey spectra were collected from 0 to 1200 eV. The narrow N 1s spectra were collected from 396 to 405 eV, the narrow Fe 2p spectra from 700 to 740 eV, and the narrow C 1s spectra from 280 to 293 eV. All of the spectra were calibrated against a value of the C 1s binding energy of 284.5 eV. Multipak 9.0 software was used for obtaining semi-quantitative atomic percentage compositions, using Gauss-Lorentz equations with Shirley-type background. A 70%/30% Gaussian/Lorentzian line shape was used to evaluate peaks position and areas of the high resolution N 1s spectra.

### 2.4. Electrochemical characterization of the electrocatalysts

The electrochemical evaluation of the electrocatalysts prepared was carried out in a conventional three-compartment electrochemical cell using a multi-potentiostat (Bio-Logic SP150), a Bipotentiostat (CH760E), and a rotating ring disk electrode instrument (RRDE-3A ALS Model 2323). The electrolyte was a 0.5 M  $\text{H}_2\text{SO}_4$  aqueous solution saturated with either  $\text{N}_2$  or  $\text{O}_2$  by direct bubbling the gas into the solution. For RDE measurements, the cell was equipped with a glassy carbon (GC) disk working electrode ( $0.1256\text{ cm}^2$  geometric area), a Pt helical wire counter electrode, and a saturated calomel (SCE) reference electrode. All of the electrode potentials were corrected and referred to the reversible hydrogen electrode (RHE). Different GC disk electrodes were arranged by preparing the ink using an ionomer-to-catalyst ITC mass ratio (mg of Nafion® over mg of catalyst) equal to 0.2 and a catalyst quantity of  $80\text{ }\mu\text{g cm}^{-2}$  [4]. The RDE rotation speed was set at 900 rpm. For RRDE measurements, a Pt ring-Glassy Carbon (rGC) disk electrode was employed. The ring

potential was kept at 1.2 V and the disk potential was scanned at a rate of 5 mV s<sup>-1</sup>. The working electrode was polished with 1 and 0.06 µm alumina powders to mirror-like finish its surface and sonicated to remove alumina particles before each experiment. The ORR onset potential was defined as a potential required for generating an ORR current density of 0.01 mA cm<sup>-2</sup>. The following equation was used to calculate the percentage of hydrogen peroxide released during ORR:

$$\%H_2O_2 = \frac{2 I_R/N}{I_D + (I_R/N)} \quad (1)$$

where  $I_D$  [mA cm<sup>-2</sup>] is the Faradaic current at the disk,  $I_R$  [mA cm<sup>-2</sup>] the Faradaic current at the ring and  $N$  is the H<sub>2</sub>O<sub>2</sub> collection coefficient at the ring (37%). The ORR kinetic current  $I_k$  was calculated taking into account the mass transport by using the relationship established by the Koutecky–Levich (K-L) theory:

$$I_k = \frac{I_{lim}I}{(I_{lim}-I)} \quad (2)$$

where  $I_k$  [mA cm<sup>-2</sup>] is the Faradic current,  $I_{lim}$  [mA cm<sup>-2</sup>] is the limiting current density, and  $I$  [mA cm<sup>-2</sup>] is the current density measured.

The best catalyst was tested also in a cell equipped with a gas diffusion working electrode (GDE), accessible to gaseous reactants. The GDE cell apparatus, fully described in Osmieri *et al.* [25], was equipped with a saturated Ag/AgCl reference electrode and a Pt plate counter electrode. The GDE working electrode geometric area was of 0.95 cm<sup>2</sup>. A 0.5 M H<sub>2</sub>SO<sub>4</sub> aqueous solution was used as electrolyte.

For the GDE preparation, small disks of 11 mm diameter of carbon cloth GDL (HT-ELAT from E-TEK, USA) were coated with the catalyst ink with an ITC mass ratio equal to 0.2 by brush deposition to obtain a catalyst loading of 2 mg cm<sup>-2</sup>, and referred to the geometrical area of the working electrode. An electrochemical impedance spectroscopy measurement was taken at OCV to quantify the resistance of the cell.



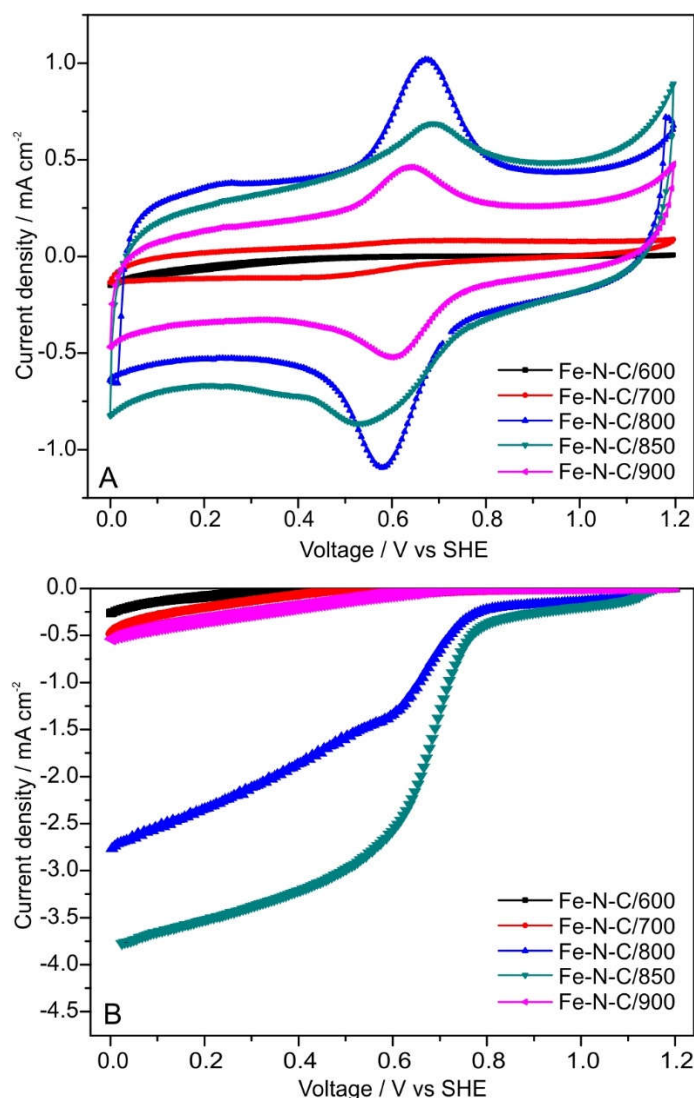
### 3. Results and discussion

#### 3.1. Heat-treatment temperature optimization for the preparation of basic Fe-N-C catalyst.

To study the effect of temperature on the preparation of the catalysts, cyclic voltammograms (CV) and linear sweep voltammetries (LSV) were employed.

Five different temperatures, 600, 700, 800, 850, and 900 °C, respectively, were selected and evaluated with the RDE apparatus. The potentiodynamic responses in acid medium of basic Fe-N-C electrocatalysts prepared at different temperatures (Fig. 1A) show that Fe-N-C catalysts pyrolyzed at temperatures higher than 700 °C exhibit a pair of well-defined redox peaks in the range 0.64–0.68 V in the anodic scan direction, and 0.55–0.60 V in the cathodic scan direction. The half-height width of these peaks is 100 mV. This is the value expected for a quasi-reversible one-electron process involving surface species [26,27]. The observed redox behavior can be ascribed to two different possible surface processes. The first one is the reduction/oxidation of the surface quinone-hydroquinone groups [28,29]. The second one is Fe<sup>III</sup>/Fe<sup>II</sup> reduction/oxidation process [30]. As mentioned in the literature, different factors could influence the capacitance of carbon materials: pore geometry, pore size distribution, electrical conductivity, wettability, and presence of surface electroactive species [31,32]. A clear increase in their capacity can be attributed to microporosity formation and graphitization of the carbon framework due to the thermal treatment, as mentioned even by other research groups [33,34]. Pseudo-capacitance effect of surface redox-sites must also be considered. In fact, at the carbon surface, apart from the electrostatic double layer capacitance, a significant pseudo-capacitance is often present. This can be due to both chemisorption phenomena with partial charge transfer and redox processes [35].

Figure 1B shows the influence of the temperature on promoting the ORR. The pyrolysis treatment at higher temperature improves the catalytic activity, resulted in more positive onset potential, showing the maximum shift at 850 °C. For heat treatment temperatures lower than 800 °C, the ORR activity is poor. Also for the sample heat-treated at 900 °C there is an important decrease in the activity. This suggests that the heat-treatment temperature is an important parameter to be optimized during the synthesis, existing a range between 700 and 900 °C where the optimum temperature is situated [19].



**Figure 1.** Basic Fe-N-C electrocatalysts synthesised at different temperatures. (A) CV recorded at 10 mV s<sup>-1</sup>. (B) LSV recorded at 5 mV s<sup>-1</sup>. Rotational speed set at 900 rpm. Experimental conditions for both series of tests: 0.5 M H<sub>2</sub>SO<sub>4</sub>, 0.2 ITC mass ratio, 80 µg cm<sup>-2</sup> catalyst loading.

### 3.2 Optimization of Fe-N-C/850 catalyst through the use of porous silica.

Selected the best Fe-N-C/850 catalyst, the influence of an external agent to modify its morphology was evaluated. Thus, new catalysts prepared by mixing FePc and the templating agents were prepared and pyrolyzed at 850 °C. Nitrogen adsorption/desorption analysis was performed on the Fe-N-C/850 on the modified catalysts. The two different silica templates (SBA15 and mSiO<sub>2</sub>) were also analyzed for comparison. The use of different porous silica as templating agent induces the formation of a different porous structure in the catalyst after the heat treatment (Fig.2A and Table 1), that could lead to increase the accessibility of the electrocatalyst.

**Table 1.** Surface characterization of F-N-C/850 catalysts and templating silica agents (n.d.: not detectable).

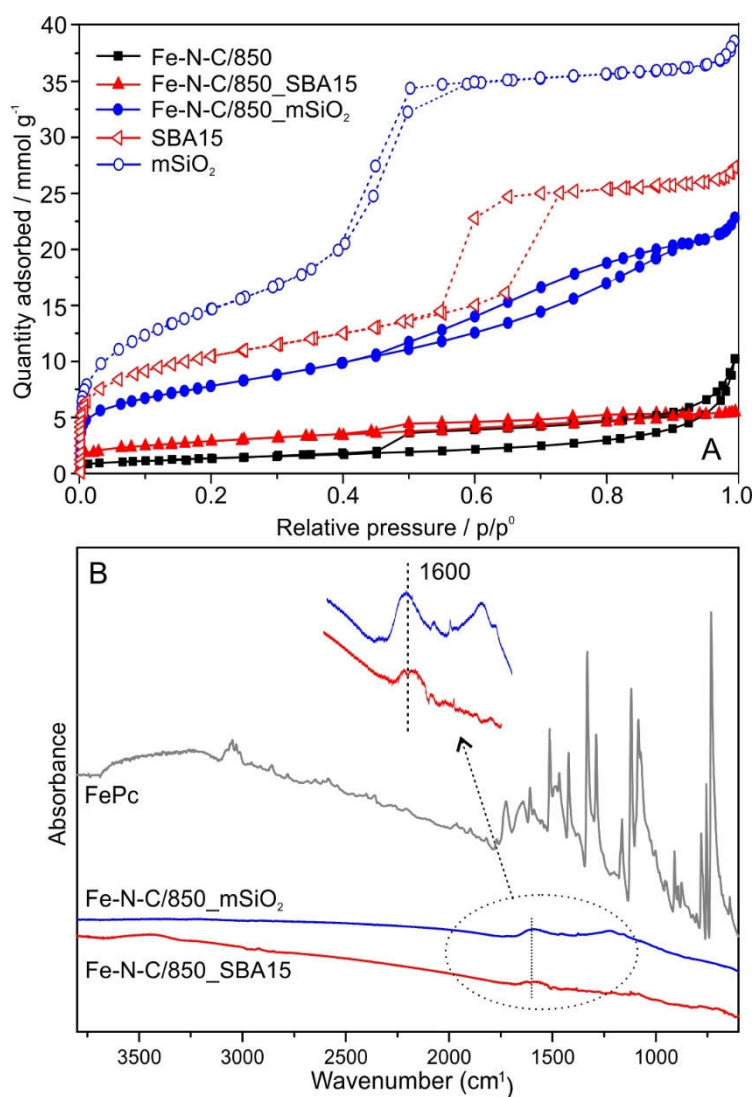
|                                   | $S_{\text{BET}}$<br>[m <sup>2</sup> g <sup>-1</sup> ] | Micropore area<br>[m <sup>2</sup> g <sup>-1</sup> ] | Pore volume<br>[cm <sup>3</sup> g <sup>-1</sup> ] | Average pore size<br>[nm] |
|-----------------------------------|---|---|---|---------------------------|
| <b>F-N-C/850</b>                  | 102   | 2   | 0.2   | 9                         |
| <b>F-N-C/850_SBA15</b>            | 221   | 31  | 0.8   | 3                         |
| <b>F-N-C/850_mSiO<sub>2</sub></b> | 601   | 70  | 0.9   | 5                         |
| <b>SBA15</b>                      | 806   | 157   | 1.3   | 4.5                       |
| <b>mSiO<sub>2</sub></b>           | 1148  | n.d.  | 0.9   | 4.4                       |

According to the International Union of Pure and Applied Chemistry (IUPAC) classification [36], the basic Fe-N-C/850 catalyst exhibits a Type II isotherm shape, with a very limited hysteresis loop. The Fe-N-C/850\_mSiO<sub>2</sub> exhibits a Type IV isotherm shape due to the presence of a more pronounced hysteresis loop. However, the limiting uptake at high  $p/p^0$  values is shorter compared to the shape of the sole mSiO<sub>2</sub> (isotherm assigned to Type IV, hysteresis loop H1 type), making the curve more similar to Type II. The hysteresis loop type can be classified as intermediate between H3 and H4. The type H3 loop does not exhibit any limiting adsorption at high  $p/p^0$  and is observed with aggregates of plate-like particles giving rise to slit-shaped pores. The type H4 loop is often associated with narrow slit-like pores, but with higher level of microporosity, as confirmed by the micropore area. Unlike the previous sample, the Fe-N-C/850\_SBA15 catalyst isotherm shape belongs to type II, which is commonly obtained with more macroporous materials. For this sample, the hysteresis loop is broader compared to the shape of the SBA15 (isotherm assigned to Type IV, hysteresis loop H2 type), but can also be classified as intermediate between H3 and H4 types.

The  $S_{\text{BET}}$ , the pore volume and the micropore area increase by employing the silica, reaching the maximum values with the mesoporous SiO<sub>2</sub> (Fig. 2A and Table 1). The formation of a microporous structure is favorable to host the iron coordinated with nitrogen, as mentioned by several groups [5,19].

FTIR spectra (Fig. 2B) were recorded on the two templated catalysts. FePc without thermal treatment was also analyzed for comparison. The FTIR spectrum of FePc shows stretching and bending vibration bands typical of metal phthalocyanines [37], including C–H (3054 cm<sup>-1</sup>) and C–C (1607 cm<sup>-1</sup>) stretching of aromatic rings, stretching of –N= mesoatoms (1513 cm<sup>-1</sup>), isoindole (1422 cm<sup>-1</sup>), and pyrrole (1331 cm<sup>-1</sup>) stretching plane (1287, 1163, 1081 cm<sup>-1</sup>) and out-of-plane (734, 780 cm<sup>-1</sup>) bending of C<sub>Arom</sub>–H. The bands attributed to the characteristic –N–H stretching (3240–3300 cm<sup>-1</sup>) and in-plane bending (1005 cm<sup>-1</sup>) vibration of pyrrolic nitrogen atoms, at 3240–3300 cm<sup>-1</sup>, typical of the pure Pc, are not detected [38]. The absence of the N–H bonds vibration is due to the complexation of Fe. In fact, in FePc the two pyrrolic hydrogens in the center of the molecule are not present, and all the four N atoms are bonded with the Fe atom [39]. The peaks and bands detected in

the wavenumber range 800–1800  $\text{cm}^{-1}$  could be ascribed to the coordination of Fe(II) in the center of the molecule [37].

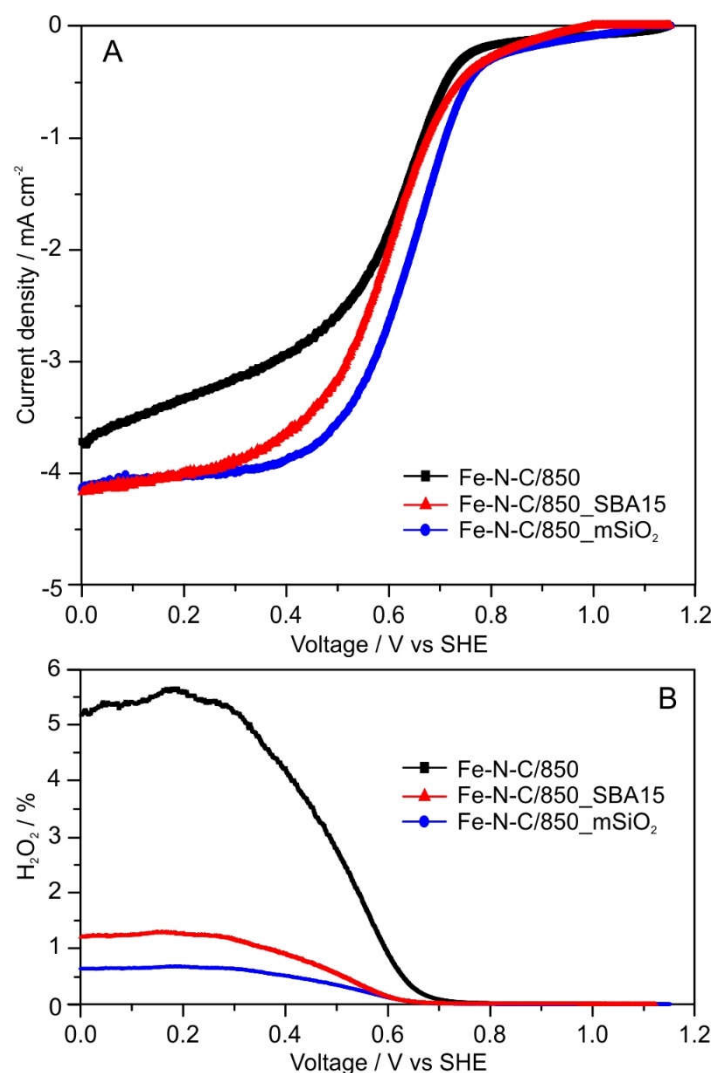


**Figure 2.** (A) Nitrogen adsorption/desorption isotherms for basic and templated Fe-N-C/850 electrocatalysts. (B) FTIR spectra of FePc precursor and templated Fe-N-C/850 electrocatalysts after the pyrolysis heat treatment at 850 °C.

For the Fe-N-C/850\_SBA15 and Fe-N-C/850\_mSiO<sub>2</sub> catalysts, regardless of the silica template the characteristic peaks of FePc completely disappear after the pyrolysis at 850°C. In fact, both catalysts exhibit almost flat spectra, very similar to the spectrum of a carbonaceous material. Similar features are reported in the literature [25,27,40], and suggest that total decomposition of the original molecule structure of the precursor occurred during the thermal treatment, with a substantial recombination of the chemical bonding. Indeed, FTIR spectra of both catalysts exhibit only weak and broad adsorption

bands at ca. 1600 and 1210  $\text{cm}^{-1}$  previously observed in N-containing carbon materials [41,42] and assigned to the pyridine-type C–N bonds.

Thus, the pyrolysis process favors the graphitization process, with a nitrogen-iron reengagement entailing a significant improvement in activity. This is evidenced by electrochemical evaluation in a three electrode configuration. An increase of currents density (Fig. 3A: from  $-1.85$  to  $-2.65 \text{ mA cm}^{-2}$  at  $0.6 \text{ V}$ ) as well by the positive shifts of the onset (from  $0.683$  to  $0.726 \text{ V}$  at OCV). Therefore, the starting nitrogen-carbon structure of the FePc precursor is helpful to synthesize F-N-C catalysts able to decrease overpotentials in ORR [27,40]. The reasonable explanation for this improvement could be the formation of pyridinic nitrogen and quaternary nitrogen-doped carbon after pyrolysis, which was proved by FTIR analysis, and also by XPS analysis (see following Section 3.4). However, the interactions of N with C cannot fully improve the electroreduction selectivity from  $\text{O}_2$  to  $\text{H}_2\text{O}$  through the expected four-electron route. The hydrogen peroxide production, measured with a series of RRDE measurements (Fig. 3B), diminished from 6 to 0.5 % at  $0.3 \text{ V}$  by templating the Fe-N-C/850 catalyst. In particular, the best selectivity was obtained with the mesoporous  $\text{SiO}_2$ .

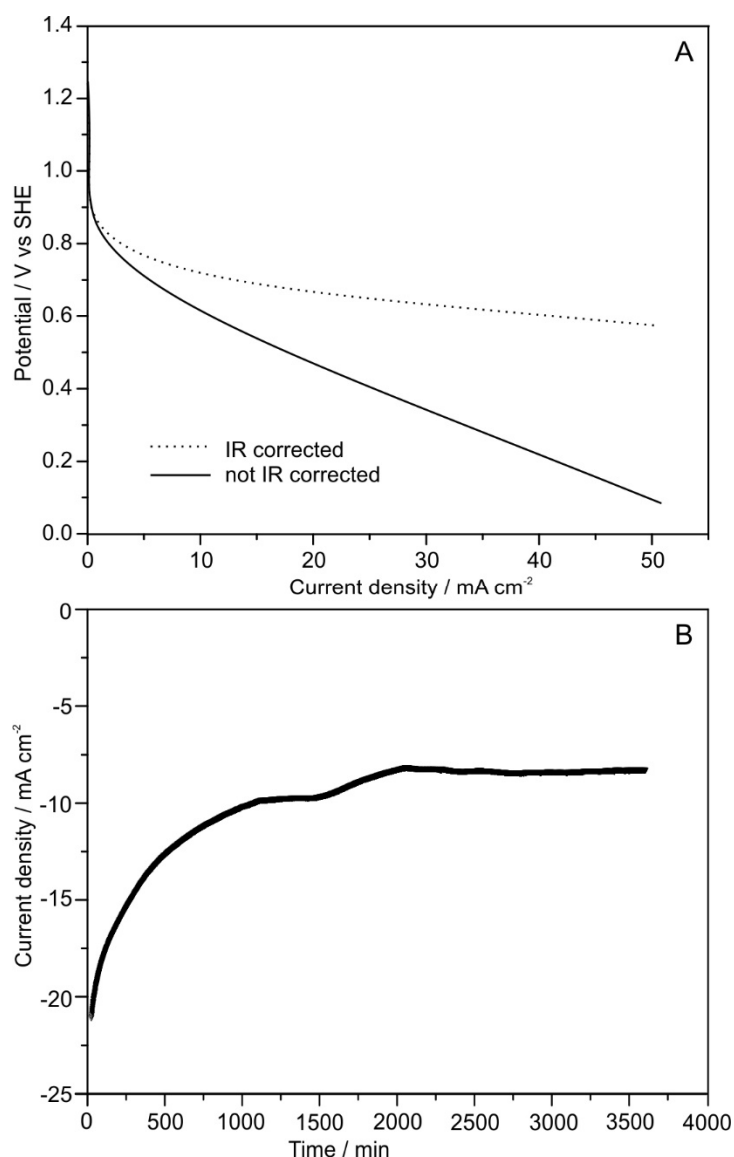


**Figure 3.** (A) LSVs from RRDE with  $\text{H}_2\text{O}_2$  formation (B) recorded at  $5 \text{ mV s}^{-1}$ . Experimental conditions:  $0.5 \text{ M H}_2\text{SO}_4$ ,  $0.2 \text{ ITC}$ ,  $80 \mu\text{g cm}^{-2}$  catalyst loading, ring potential  $1.2 \text{ V vs SHE}$ . Rotational speed set at  $900 \text{ rpm}$ .

### 3.3 Activity and stability of the *Fe-N-C/850\_mSiO<sub>2</sub>* catalyst.

Furthermore, the activity and stability of the *Fe-N-C/850\_mSiO<sub>2</sub>* catalyst were assessed in the GDE cell (Fig. 4). This specific type of cell allows the use of higher amount of catalyst compared to the RDE configuration, bypassing the limitations of thin electrode layers. In fact, the main advantage of the GDE cell is the direct supply of gaseous oxygen to the cathode, avoiding losses due to oxygen diffusion through the liquid electrolyte, thus increasing the amount of accessible oxygen. The *Fe-N-C/850\_mSiO<sub>2</sub>* catalyst shows an OCV of  $0.79 \text{ V vs RHE}$  with a catalyst loading of  $2 \text{ mg cm}^{-2}$  (Fig. 4A). The current density of the catalyst was  $-2.8 \text{ mA cm}^{-2}$  at  $0.8 \text{ V}$ , corresponding to a mass activity of  $-1.4 \text{ mA mg}^{-1}$ , under IR corrected conditions. This value is comparable to the activity of similar electrocatalysts in the literature [23,43,44].

In terms of stability (Fig. 4B), during the chronoamperometry at 0.47 V the catalyst shows a relatively fast decay of the current density during the first 5 h of the test, then it reaches a rather stable performance up to 60 h, mainly attributed to pyridinic and pyrrolic nitrogen like fixation [19], as described in Section 3.4.



**Figure 4.** Fe-N-C/850\_mSiO<sub>2</sub> catalyst. (A) ORR activity (original and iR-corrected) measured in GDE cell at 5 mV s<sup>-1</sup>. Experimental conditions: 0.5 M H<sub>2</sub>SO<sub>4</sub>, 0.2 ITC mass ratio, 2 mg cm<sup>-2</sup> catalyst loading. (B) ORR stability at a potential of +0.47 V vs SHE in O<sub>2</sub>-saturated 0.5 M H<sub>2</sub>SO<sub>4</sub> solution in the GDE cell.

### 3.4 Physico-chemical characterization of the Fe-N-C/850 electrocatalysts.

EDX and XPS analyses were used to investigate the elemental composition of the Fe-N-C/850 catalysts (Table 2). The wide XPS scan spectra for the three catalysts (not reported here) reveal the

presence of C, O, N and Fe on catalysts' surface. The iron content is very low, close to the detection limit of the instrument, similarly to the values of other Fe-N/C catalysts mentioned in the literature [43–45]. The low Fe atomic percentages are confirmed by EDX analysis. This is expected considering that the FePc precursor contains a theoretical Fe content equal to 1.75 at.%, and not all of the iron remains on the structure of the final electrocatalysts. No residual silica is detected, sign that the acid washing was effective in completely removing the templating agent.

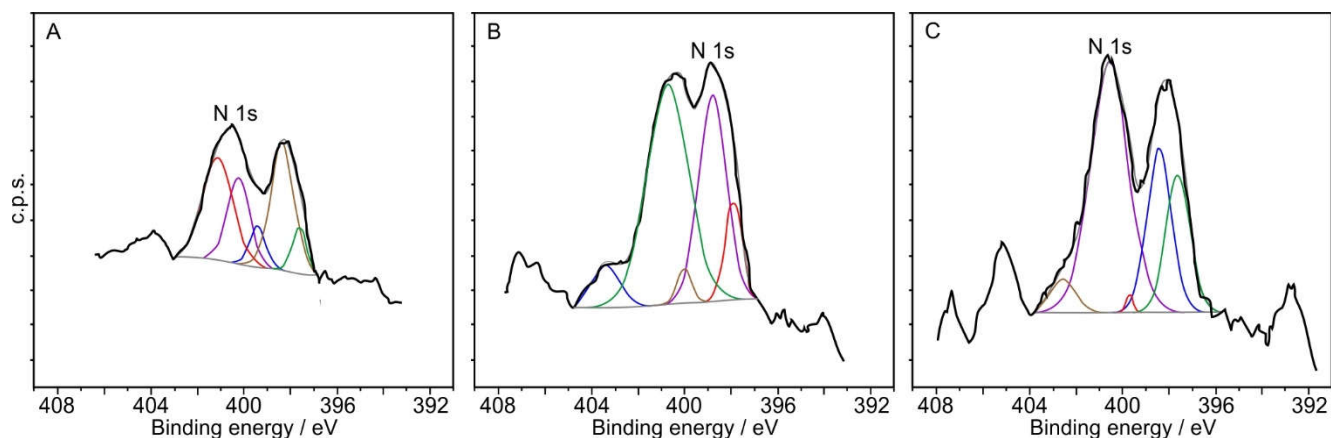
**Table 2.** Elemental composition of Fe-N-C/850 catalysts from EXD and XPS analyses. From the deconvolution of the high resolution N 1s spectra Nitrogen contents with relative intensities and binding energies are listed (N1: nitrile; N2: pyridinic-N; N3: Nx-Fe; N4: pyrrolic-N; N5: quaternary-N; N6: graphitic-N; n.d.: not detected).

|                                   | EDX    | XPS [at.%; eV] |      |      |      |               |               |              |               |               |              |
|-----------------------------------|--------|----------------|------|------|------|---------------|---------------|--------------|---------------|---------------|--------------|
|                                   | [at.%] | Fe 2p          | C 1s | O 1s | N 1s | N1            | N2            | N3           | N4            | N5            | N6           |
| <b>F-N-C/850</b>                  | 0.5    | 0.9            | 89.3 | 8.3  | 1.5  | 7.5<br>397.6  | 32.1<br>398.3 | 6.9<br>399.4 | 20.6<br>400.2 | 32.9<br>401.1 | n.d.         |
| <b>F-N-C/850_SBA15</b>            | 0.2    | <0.1           | 93.0 | 6.0  | 0.9  | 9.3<br>397.9  | 31.1<br>398.7 | 2.8<br>400.0 | 50.3<br>400.7 | n.d.          | 6.5<br>403.3 |
| <b>F-N-C/850_mSiO<sub>2</sub></b> | 0.1    | <0.1           | 88.0 | 10.0 | 2.0  | 18.5<br>398.1 | 22.8<br>398.9 | 0.7<br>400.0 | 53.3<br>400.8 | n.d.          | 4.7<br>403.1 |

The high resolution N 1s spectra of the catalysts (Fig. 5) are fitted into six peaks correspond to six types of nitrogen, such as nitrile N1 (398 eV), pyridinic N2 (398.6 eV), Nx-Fe N3 (399.6 eV), pyrrolic-N N4 (400.7 eV), quaternary N5 (401.8 eV) and graphitic N6 (403 eV) [45]. The peak with the lowest binding energy (398.7 eV) is due to the imine-like (=N–) structure, and the peak centered at 399.8 eV is attributed to the amine-like nitrogen atoms (–NH–). The peak centered at 401.6 eV can be assigned to cationic nitrogen atoms on the polymer backbone, and the peak with highest binding energy (402.8 eV) is due to the protonated amine units [46]. The high content of pyrrolic-like N4 (Table 2), belonging to the catalyst Fe-N-C/850\_mSiO<sub>2</sub>, can be attributed to the first to electrons responsible of the reduction of oxygen [45]. The pyridinic N2 and the pyrrolic N4, which are predominant in this catalyst, have the nitrogen atoms bonded to two adjacent carbon atoms in the graphene lattice with one/two p-electron(s) localized in the  $\pi$  conjugated system [47,48]. According to the literature, the electrocatalytic ORR activity can be attributed to pyridinic-N (N2) and/or pyrrolic-N (N4) [49–53], whereas other authors suggested that graphitic-N (N6) is more important for the electrocatalytic activity of N-doped carbon based electrocatalysts [54,55]. In our case, both

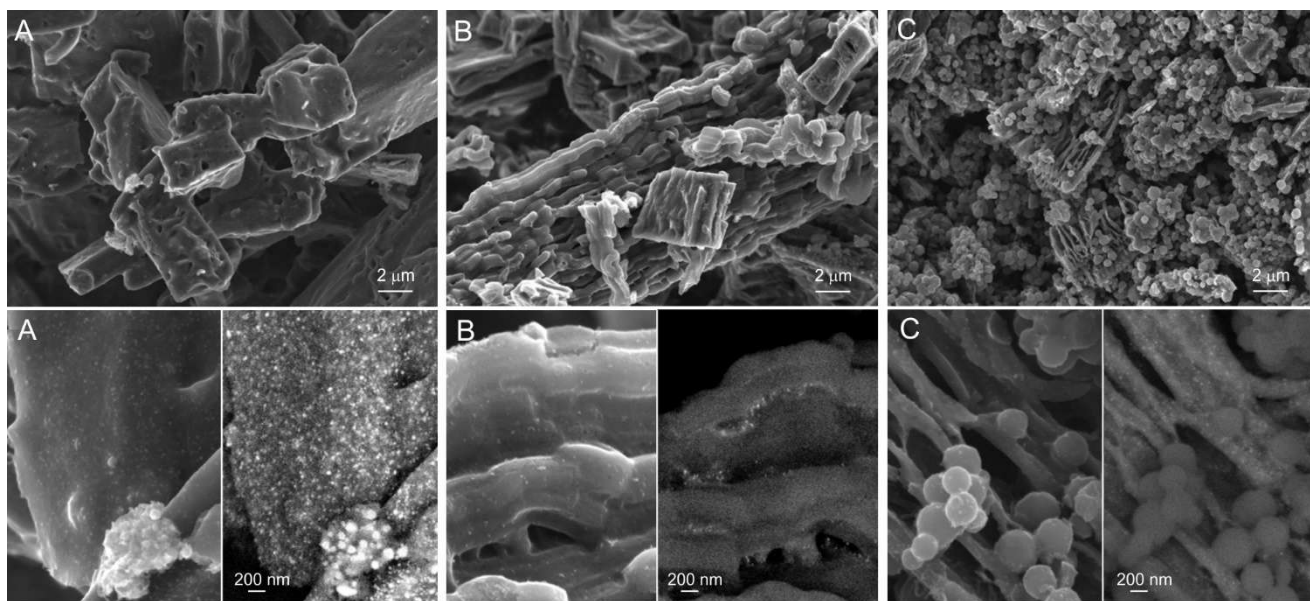


catalysts templated with porous silica, shows higher content of pyrrolic-N (N4), more than the double compared to the basic F-N-C/850 catalyst.



**Figure 5.** XPS deconvolution of the high resolution N 1s spectra of Fe-N-C/850 (A), Fe-N-C/850\_SBA15 (B), and Fe-N-C/850\_mSiO<sub>2</sub> (C) catalysts.

The effects of the use of different templating agents on the morphology of the catalysts surface after the heat treatment at 850 °C are evaluated by FESEM analysis (Fig. 6). The F-N-C/850 catalyst (Fig. 6A) presents a block-like structure, with iron finely dispersed on the surface in an inhomogeneous way, showing various agglomerates, as enlightened by the higher magnification backscattered image. The use of the in house SBA15, which presents a typical rod-shape morphology, caused the modification in the shape of the F-N-C/850\_SBA15 catalyst (Fig. 6B) to a worm-like structure that favored a better distribution of the iron, without the formation of agglomerates. The commercial mSiO<sub>2</sub>, presenting a typical spherical-shape of the structure, favored a globular shape mixed with root-like filaments of the F-N-C/850\_mSiO<sub>2</sub> particles (Fig. 6C). Here the mixed structure could be due to the 3:1 weight ratio between the FePc precursor and the mSiO<sub>2</sub> templating agent. The presence of the spheres-like particles could explain the higher  $S_{BET}$  of this catalyst (Table 1), avoiding the agglomeration of the iron, not seen even in other parts of the sample examined.



**Figure 6.** FESEM images of Fe-N-C/850 (A), Fe-N-C-/850\_SBA15 (B), and Fe-N-C/850\_mSiO<sub>2</sub> (C) at low and high (backscattered) magnification.

By concluding, when comparing the activity of different Fe-N-C catalysts templating with different types of silica, the well-defined limited current density plateau of the Fe-N-C/850\_mSiO<sub>2</sub> (Fig. 3A) suggests that more catalytic sites, or better distributed catalytic sites, were available for the ORR. Generally, the current plateau in RRDE measurements for ORR is dependent on the distribution of the electrocatalytic sites on the electrode surface [56]. In fact, when the distribution of active sites is less uniform and the electrocatalytic reaction is slower, the current plateau would become more inclined [4,34,56] and not a plateau value as expected. More active sites, or better distributed active sites, can be formed during the heat treatment. This could be due to the possible interactions between iron and nitrogen or iron and carbon during the pyrolysis process. Therefore on the Fe-N-C/850\_mSiO<sub>2</sub> catalyst the presence of micropores (Table 1), that is accessibility, and a uniform distribution of iron (Fig. 6), not only significantly improved the catalytic activity for ORR (Fig. 3A), but also reduced the percentage of hydrogen peroxide production (Fig. 3B), letting the reaction proceed through an almost four-electron pathway.

#### 4. Conclusions

Fe-N-C catalysts were synthesized by pyrolysis treatment of iron phthalocyanine at various temperatures under inert atmosphere. The heat treatment at 850 °C favored the preparation of a catalyst with the highest activity towards ORR. The morphology of this catalyst was on purpose modified with the use of different porous silica (SBA15 in house prepared and commercial mesoporous SiO<sub>2</sub>) as templating agent during synthesis. The physico-chemical characterization

confirmed the presence of both Fe and N in the catalysts prepared. The use of the templating agent allowed to drastically increase the specific surface area and the microporosity the catalysts, especially with the use of the commercial mesoporous SiO<sub>2</sub>.

The electrocatalytic activity towards ORR of the catalysts in acid conditions was assessed by RRDE apparatus and a GDE cell. In both testing approaches, the Fe-N-C/850\_mSiO<sub>2</sub> catalyst exhibited higher electroactivity. In particular, in the GDE configuration this catalyst reached a current density of  $-2.8 \text{ mA cm}^{-2}$  at 0.8 V, corresponding to a mass activity of  $-1.4 \text{ mA mg}^{-1}$ , under IR corrected conditions. The chronoamperometry performed at 0.47 V vs SHE up to 4500 min showed relatively good stability values. The higher electroactivity and stability of the Fe-N-C/850\_mSiO<sub>2</sub> catalyst could be ascribed to an increase of the microporosity.

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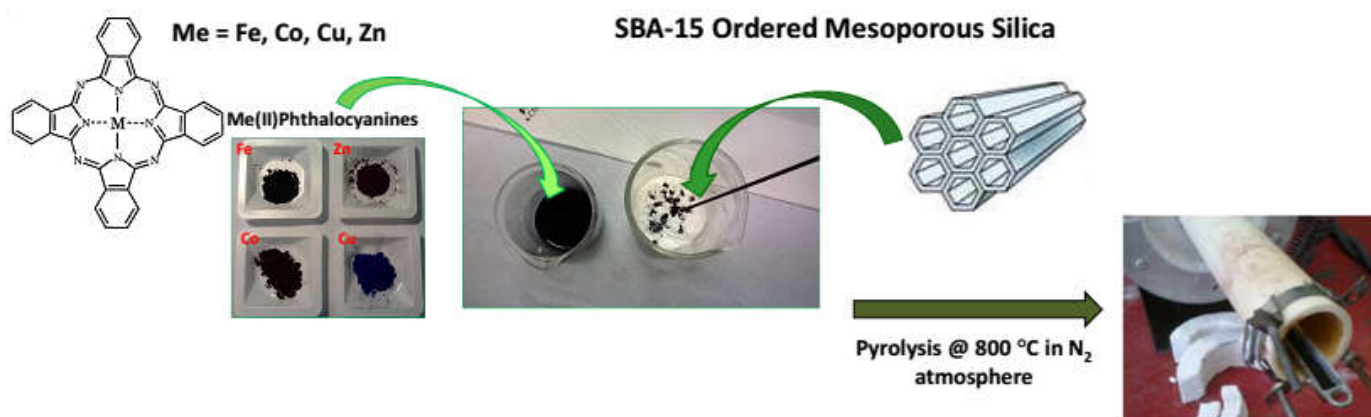
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## CHAPTER 6. The influence of different transition metals (Me = Fe, Co, Cu, Zn) on the properties and ORR electroactivity of Me-N-C catalysts synthesized from Me(II)-Phthalocyanine precursors.

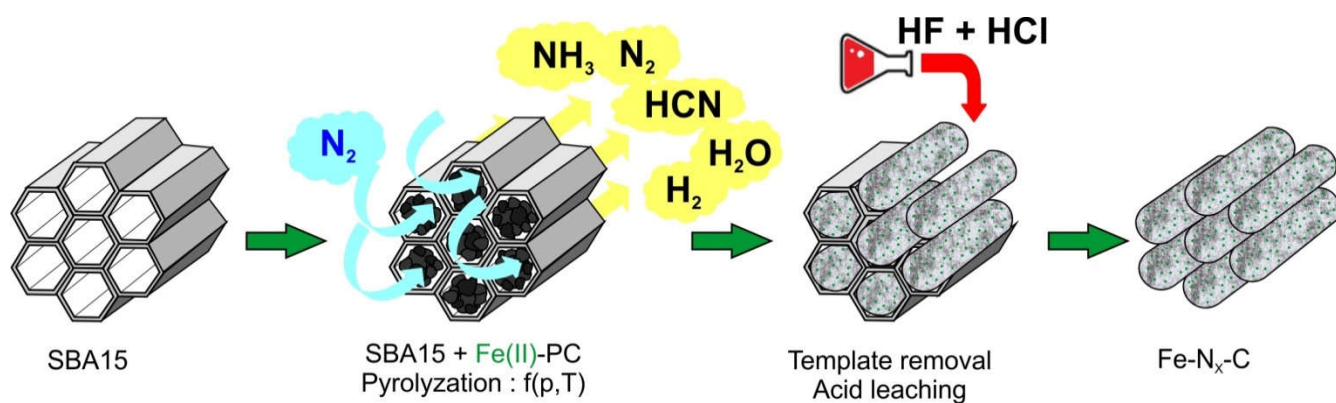


### 1. Introduction.

Several efforts have been made recently to synthesize new non-precious metal catalysts without using a carbonaceous support [1,2]. The basic idea lies in the use of sacrificial supports, to be mixed with macromolecules containing nitrogen, carbon, and the transition metal together. The template is removed during or after the pyrolyzation step, resulting in a self-supported Me-N-C catalyst with high pore volume and, consequently, high density of active ensembles.

The porosity can be tuned by using the sacrificial supports (silica, alumina, zirconia, etc.) as templating agents [3,4], with an approach similar to that used when producing mesoporous carbon by hard templating method [5]. In general, the templating agent hosts N-C, or Me-N-C precursors, inside its structure, as illustrated in Figure 0. The templating agent, SBA-15 silica as an example, can be imagined as a series of ordered packed tubular (or hexagonal) open “microreactors”, which is hosting the precursors complex. When the pyrolysis starts, the decomposition process of the precursors takes place inside each SBA-15 “micro-reactor”: the temperature raises, decomposition gases are released, and contemporary pressure increases locally as well, forming a very porous carbon structure and favoring its nitrogen-iron doping. The templating agent is then removed by strong acid leaching. The resulting non-precious metal catalyst is self-supported, highly porous and homogeneous, with better accessibility to reactants, and densely populated of active ensembles.





**Figure 0.** Schematic representation of the formation of self-supported non-precious metal catalysts by hard templating method using SBA-15 as sacrificial agent, and Fe-phthalocyanine as Fe-N-C source.

## 2. Experimental

### 2.1. Chemicals.

Tetraethyl orthosilicate (TEOS,  $\geq 98\%$  purity), Hydrochloric acid (HCl, 37 wt. %), Pluronic P123® triblock copolymer, Perchloric acid ( $\text{HClO}_4$ , 70 wt. %), Sulfuric acid ( $\text{H}_2\text{SO}_4$ , 98 wt. %), Hydrofluoric acid ( $\text{HF}$ ,  $\geq 40$  wt. %), Potassium Hydroxide (KOH, 99.0% purity), Ethanol ( $\geq 99.8\%$  purity), Acetone ( $\geq 99.8\%$  purity), Isopropanol ( $\geq 99.7\%$  purity), Nafion® 5 wt. % hydroalcoholic solution, Iron(II) Phthalocyanine  $\text{C}_{32}\text{H}_{16}\text{N}_8\text{Fe}$  (Fe-Pc, 90% purity), Cobalt(II) Phthalocyanine  $\text{C}_{32}\text{H}_{16}\text{N}_8\text{Co}$  (Co-Pc, 97% purity), Copper(II) Phthalocyanine  $\text{C}_{32}\text{H}_{16}\text{N}_8\text{Cu}$  (Cu-Pc, 90% purity), Zinc(II) Phthalocyanine  $\text{C}_{32}\text{H}_{16}\text{N}_8\text{Zn}$  (Zn-Pc, 97% purity) and 29H,31H-Phthalocyanine  $\text{C}_{32}\text{H}_{18}\text{N}_8$  (H-Pc, 98% purity) were purchased from Sigma Aldrich. Methanol ( $\geq 99.9\%$  purity) and Hydrogen Peroxide (33 wt. %) were purchased by Panreac. Nitrogen and oxygen gases were supplied in cylinders by SIAD with 99.999% purity. All aqueous solutions were prepared using ultrapure deionized water obtained from a Millipore Milli-Q system with resistivity  $>18 \text{ M}\Omega \text{ cm}^{-1}$ .

### 2.2. Synthesis.

#### 2.2.1. Synthesis of silica template.

Mesoporous silica SBA-15 was prepared following the procedure reported by Zeng et al. [5,6], using the triblock copolymer  $\text{EO}_{20}\text{PO}_{70}\text{EO}_{20}$  (Pluronic P123) as surfactant and TEOS as silica source.

In detail, 8.3 g of P123 was dissolved into 312 mL of 1.6 M HCl solution under stirring at 40 °C. Then, 19 mL of TEOS was added and the solution was stirred for 20 h keeping the temperature constant at 40 °C. Then, the temperature was increased at 100°C and maintained constant for 24 h.

The product was filtered, washed with deionized water, and calcined in oven at 550 °C for 10 hours in air to completely remove the residuals of Pluronic surfactant.

### *2.2.2. Synthesis of Me-N-C catalysts.*

Four different Me-N-C catalysts were prepared, using four different Me(II)-phthalocyanine (MePc) precursors (Me = Fe, Co, Cu, Zn). As a comparison, a further catalyst was prepared in the same way using as precursor the phthalocyanine molecule without metal center (29H,31H-Phthalocyanine, HPc).

First, 500 mg of Me(II)-phthalocyanine was dissolved in 7.8 mL of an ethanol-water 1:1 vol. solution and left under stirring for 1 hour.

SBA-15 silica was used as template for the synthesis of the Me-N-C electrocatalysts in a 1:1 wt. ratio with respect to the phthalocyanine precursor. In detail, 500 mg of SBA-15 silica was wet-impregnated by slowly pipetting the Me(II)-phthalocyanine solution on it. Then, a viscous slurry was formed, and it was left under mild stirring at room temperature overnight, to let the phthalocyanine precursor to completely fill the SBA-15 silica pores. Subsequently, the slurry was heated on a hot plate at 100°C until complete evaporation of the solvent. The precursor powder was recovered and homogenized in a mortar and it was placed in quartz boat to perform the pyrolysis heat treatment. The pyrolysis treatment consisted in heating the sample in a tubular quartz furnace under nitrogen atmosphere (N<sub>2</sub> gas flux set at 80 NmL min<sup>-1</sup> with a mass flow controller from Bronkhorst, ELFLOW series) with a heating rate of 10 °C min<sup>-1</sup> until 800 °C. The temperature was kept constant at this value until 3 hours have passed from the starting of the heat treatment. Then the furnace was switched-off leaving the apparatus cooling down naturally to room temperature.

The catalysts synthesized from FePc, CoPc, CuPc, ZnPc and HPc were named Fe-N-C, Co-N-C, Cu-N-C, Zn-N-C and H-N-C, respectively.

### *2.3. Physico-chemical characterization.*

Nitrogen adsorption-desorption isotherms for all of the Me-N-C catalysts and for SBA-15 silica, were recorded using an ASAP 2020 Instrument (Micromeritics) at 77 K, within the relative pressure range of 0 – 1. Before the analysis, all of the samples were placed into a glass burette and degassed under vacuum for 3 hours at 150 °C. The specific surface area of the samples was calculated using the Brunauer–Emmett–Teller (BET) method within the relative pressure range 0.1 – 0.3. The average pore size was obtained with the Barrett–Joyner–Halenda (BJH) method. The micropores area and volume and the differential surface area distribution were obtained by a Density Functional Theory (DFT) model calculation included in the Micromeritics ASAP 2020 instrument software.

Scanning electron microscopy coupled with energy-dispersive X-ray spectroscopy (SEM-EDX FEI-Quanta™ Inspect 200 with EDAX PV 9900 instrument working at 15 kV), was performed to detect the presence of the transition metal (Fe, Co, Cu or Zn) in the bulk of the Me-N-C catalysts.

A field emission scanning electron microscope (FESEM, model JEOL JSM 6700F) was used to investigate the morphology of the SBA-15 silica and the Me-N-C catalysts.

Fourier transform infrared spectroscopy (FTIR) analysis was conducted on all of the Me-N-C catalysts samples. Before the measurements, powder samples were mechanically mixed with KBr and pressed. IR spectra were collected in air at  $2\text{ cm}^{-1}$  resolution on a Bruker Equinox 55 FTIR spectrophotometer, equipped with a MCT (Mercury Cadmium Telluride) detector.

X-ray photoelectron spectroscopy (XPS) was performed to determine the elemental surface composition of the catalysts samples, in particular to detect the presence of N and transition metals. The analysis was carried out using a Physical Electronics PHI 5000 Versa Probe electron spectrometer system with mono-chromated Al  $K_{\alpha}$  X-ray source (1486.60 eV) run at 15 kV and 1 mA anode current. Survey scans as well as narrow scans (high resolution spectra) were recorded with a spot of 100 nm size. For all of the samples, the survey spectra were collected from 0 to 1200 eV and the narrow N 1s spectra were collected from 390 to 412 eV. Before the measurements, all of the samples were placed in an ultrahigh vacuum chamber at  $2 \cdot 10^{-10}$  mmHg, and calibrated against a value of the C 1s binding energy of 284.5 eV. CasaXPS software was used to obtain the N 1s peaks deconvolution and the semi-quantitative atomic percentage compositions, using Gauss – Lorentz equations with Shirley-type background. A 70% Gaussian / 30% Lorentzian line shape was used to evaluate peaks position and areas.

Raman spectroscopy was performed for the Fe-N-C, Co-N-C and Cu-N-C catalysts (being these samples the ones which show the best ORR activities) to evaluate the ordered/disorder degree of their carbon-based crystalline structure. The instrument used was a  $\mu$ -Raman Spectroscopy ( $\mu$ RS Renishaw InVia spectrometer equipped with a Leica DMLM confocal microscope and a CCD detector with an excitation wavelength of 785 nm, Renishaw plc, Gloucestershire, United Kingdom). The Raman scattered light was collected in the spectral range  $100\text{--}1000\text{ cm}^{-1}$ . At least ten scans were accumulated in four different positions of the catalyst to ensure a sufficient signal to noise ratio.

Thermogravimetric analysis (TGA/SDTA 851e - Mettler Toledo) coupled to mass spectrometry (Blazers Prisma QME 200 - Pfeifer vacuum) were performed under Ar flow ( $50\text{ NmL min}^{-1}$ ) in the  $25\text{--}800^{\circ}\text{C}$  temperature range. The heating rate ( $10^{\circ}\text{C min}^{-1}$ ) and dwell time (1h) were the same used in the pyrolysis treatment carried out during the synthesis of the catalysts.

## 2.4. RDE-RRDE measurements.

### 2.4.1. Ink formulations.

For the RDE test of Me-N-C catalysts the ink was prepared by dispersing a given mass of catalyst ( $m_{cat}$ , typically around 10 mg) in a solution obtained mixing known volumes of isopropanol, deionized water and a 5% wt. Nafion ionomer hydro-alcoholic solution. An ink formulation is characterized by its mass ratio of Nafion ionomer to catalyst, or Nafion-to-catalyst-ratio (NCR). The volumes (in  $\mu\text{L}$ ) of Nafion solution, deionized water and isopropanol to use to prepare the ink are calculated as follows:

$$V_{naf} = \frac{NCR \cdot m_{cat} \cdot d_{naf}}{0.05}$$

$$V_{H_2O} = 15 \cdot m_{cat}$$

$$V_{isop} = 50 \cdot m_{cat} - V_{H_2O} - V_{naf}$$

Where  $m_{cat}$  is expressed in mg and  $d_{naf}$  is the density of the Nafion 5% wt. solution expressed in  $\text{g mL}^{-1}$ . With this formulation, the catalyst density in the ink is  $0.02 \text{ mg } \mu\text{L}^{-1}$ . The ink is kept under sonication (130W, Soltec 2200M3S sonicator) for 30 min to achieve a good dispersion. To have the desired catalyst loading, a proportional volume of ink is pipetted on the RDE electrode surface.

As a purpose of comparison, a Pt-based catalyst was also tested. The catalyst used was a commercial 20 wt. % Pt supported on Vulcan XC-72 carbon black (QuinTech, Göppingen, Germany). For this catalyst, the ink prepared by dispersing 10 mg of catalyst (mass of Pt and C), 33  $\mu\text{L}$  of 5 wt% Nafion solution, 734  $\mu\text{L}$  of isopropanol and 20  $\mu\text{L}$  of deionized water. This formulation led to have 2.5  $\mu\text{g}$  of Pt per  $\mu\text{L}$  of ink. After 30 minutes under sonication, a proportional volume of ink was pipetted to have a Pt loading on the electrode of  $38 \mu\text{g cm}^{-2}$ .

### 2.4.2. Electrochemical characterization.

The electrochemical tests were conducted in a conventional three-electrodes electrochemical cell configuration, using a rotating disk electrode equipment (RRDE-3A ALS) and a multi-potentiostat (Bio-Logic SP-150). The cell was equipped with a glassy carbon disk – Pt ring working electrode (disk diameter 4 mm, ring outer diameter 7 mm, ring inner diameter 5 mm), a Pt helical wire counter electrode, and a saturated calomel reference electrode (SCE). For tests in acidic conditions the electrolyte was an aqueous solution of  $\text{H}_2\text{SO}_4$  in different concentrations depending on the test. For tests in alkaline conditions, a 0.1 M KOH solution was used. The electrolytes were saturated with pure  $\text{N}_2$ , pure  $\text{O}_2$  or with mixtures of both gases in different proportions, depending on the type of test, by direct gas bubbling into the solution. The  $\text{N}_2$  and  $\text{O}_2$  flows were carefully controlled through two mass flow controllers (Bronkhorst, ELFLOW series), maintaining constant the total flow rate at  $150 \text{ NmL min}^{-1}$ . Once the saturation was achieved, the gas inlet tube was lifted above the electrolyte

solution level. For the RRDE measurements, the ring potential was kept at 1.2 V vs RHE. At this potential, the  $\text{H}_2\text{O}_2$  oxidation reaction is under diffusion control [7]. The RRDE tests were conducted using a bi-potentiostat (Mod. CH760E). The background current measured at the ring at potentials higher than the reaction onset (above  $\sim 0.8$  V vs RHE for acid conditions and  $\sim 0.9$  V vs RHE for alkaline conditions) was subtracted from the ring signal throughout the whole scanned potential range [8].

Prior to start tests, 50 cyclic voltammetry (CV) cycles at  $100 \text{ mV s}^{-1}$  scan rate were performed in the potential window 0.0 - 1.2 V vs RHE in  $\text{N}_2$  saturated electrolyte, in order to obtain an electrochemically clean and stable working electrode surface [9].

For the ORR activity measurements, staircase voltammetries were recorded from 1.2 to 0.0 V vs RHE in oxygen-saturated electrolyte with a potential step of 0.01 V and a holding time at each potential of 30 s. After this time, the background capacitive current had passed, and a steady-state value of the faradaic current was measured. In this way steady-state polarization curves were obtained [10]. The RDE rotation speed was set at 900 rpm.

For the Koutecky-Levich experiment, linear sweep voltammetries (LSV) were recorded at different RDE rotation speeds (200 – 500 – 900 – 1600 – 2500 and 3600 rpm ) and  $5 \text{ mV s}^{-1}$  scan rate.

For activation energy calculation experiments, LSV were recorded at  $5 \text{ mV s}^{-1}$  scan rate and with a RDE rotation speed of 900 rpm at different temperatures (10 – 15 – 20 – 25 – 32 – 40 – 50  $^{\circ}\text{C}$ ) by placing the cell inside a thermostatic bath, which temperature was regulated and controlled by a water heating-cooling system (Mod. CRIOTERM 190, I.S.CO. s.r.l., Italy).

The methanol tolerance tests were carried out in a three-electrodes electrochemical cell configuration at room temperature. The electrolyte was a 0.5 M  $\text{H}_2\text{SO}_4$  solution saturated with  $\text{O}_2$ . Methanol was progressively added to the solution to reach different concentrations (0.01 – 0.1 – 1 and 2 M). The electrochemical cell was equipped with a saturated Ag/AgCl reference electrode and a graphite rod counter electrode. A rotating disk electrode (PINE) with a glassy carbon disk diameter of 5 mm was used as working electrode. An AutoPG potentiostat-galvanostat (Mod. EG&G273A) was used to control the electrode potential.

A LSV at  $5 \text{ mVs}^{-1}$  scan rate and 900 rpm was recorded without methanol and with methanol in the solution for each methanol concentration.

At the end of each test, an electrochemical impedance spectroscopy measurement was done at the open circuit voltage (OCV), with a wave amplitude of 10 mV and frequencies in the range of 10 kHz – 100 mHz. The high frequency resistance value was used to subtract the ohmic drop contribution from the linear sweep voltammetry curves [7,11].

The electrode potentials hereafter were corrected and referred to the reversible hydrogen electrode (RHE). The current densities were normalized to the geometric area of the glassy carbon disk electrodes.

## *2.5. Single fuel cell measurements.*

### *2.5.1. Acid-DMFC test.*

The Fe-N-C catalyst performance as ORR cathodic catalyst was evaluated in a 4 cm<sup>2</sup> active area DMFC single cell. A commercial Nafion 117 membrane (Dupont) was used as electrolyte. Before use, the membrane was cleaned by boiling in 3 wt% hydrogen peroxide solution for 1 hour and then rinsed in boiling deionized water for 1 hour. Then, to be adequately protonated, the membrane was boiled in 0.5 M H<sub>2</sub>SO<sub>4</sub> solution for 1 hour and rinsed in boiling deionized water for 1 h [12]. A commercial Pt-Ru/C catalyst (Johnson Matthey, 30 wt% Pt-Ru, Pt:Ru 1:1 atomic ratio) was used as anodic catalyst. As a purpose of comparison, the performance of a DMFC using a commercial Pt/C catalyst (Johnson Matthey, 40 wt % Pt) at the cathode was also evaluated.

The electrodes were prepared by spraying the catalyst ink onto a Teflon-treated carbon cloth (ELAT GDL-LT 1200 W) gas diffusion layer (GDL) by means of an air-brush. The inks were prepared by mixing the catalysts powder with an isopropanol/deionized water solution (2:1 vol.) and a Nafion ionomer solution (5 wt. %) under sonication until getting a homogeneous suspension. The Nafion solution amount was in accordance to the desired amount of Nafion in the dry catalytic layer. Different Fe-N-C cathodes were prepared varying the Nafion content on the dry electrode and the catalyst loading. Electrodes with a Nafion content of 4 – 35 – 50 and 66 wt. % were prepared, while the Fe-N-C catalyst loadings used were 2.5 and 5 mg cm<sup>2</sup>. For preparing the Pt-Ru and Pt based electrodes, the Pt loading on the electrodes was set to 1 mg cm<sup>-2</sup>, with a Nafion content of 4 wt. %. The MEA was obtained by hot pressing the anode and the cathode on the membrane at 100 °C temperature and 60 bar pressure for 3 minutes.

For the DMFC test, the MEA was mounted into a 5 cm<sup>2</sup> single cell (Electrochem Inc.). A 5 cm<sup>2</sup> carbon cloth backing layer (ELAT GDL-LT 1200 W, the same used as GDL) was also placed on both anode and cathode before closing the bipolar plates. The fuel cell hardware was then connected to a fuel cell test bench (MITS Pro-FCTS, Arbin Instruments). For the polarization experiments, the cell was controlled with an electrical load system. The DMFC anodic compartment was fed with 2 M methanol solution preheated at 80 °C with a flow rate of 1 min<sup>-1</sup> and a pressure of 0.33 bar (relative). The cathodic compartment was fed with a 200 NmL min<sup>-1</sup> pure O<sub>2</sub> flow preheated at 80 °C with no humidification. The O<sub>2</sub> backpressure was set to 3 bar. The temperature of the cell was maintained at 90 °C during the experiments. The cell is let at open circuit potential (OCP) while reactants flow at

the electrodes for about 15 min until the OCP stabilizes. The polarization curve is recorded by scanning the cell potential starting down to 0.0 V at a scan rate of 10 mV s<sup>-1</sup>.

The DMFC is activated by recording successive polarization curves until they show no significant variation.

A short-term durability test was carried out to test the stability of the MEA fabricated with the most performing cathodic formulation. The test consisted into a 2 or 3 hours chronoamperometric experiment at 0.4 V conducted in the same operating conditions described above for the polarization curve experiments with a flow rate of the methanol solution at the anode of 5 mL min<sup>-1</sup> [12]. A polarization curve is recorded regularly every 30 minutes, to evaluate the performance variation with time.

#### 2.5.2. Acid H<sub>2</sub> / O<sub>2</sub> PEMFC test.

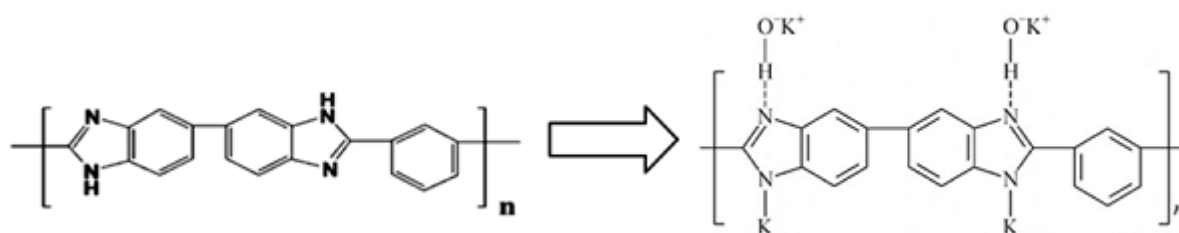
A further test of Fe-N-C catalyst was made in PEMFC using H<sub>2</sub> as fuel. The same 4 cm<sup>2</sup> active area single cell described in section 2.5.1 was used. In this case a commercial Nafion 112 membrane (Dupont) was used as electrolyte. Before use, the membrane was submitted to the same treatment described previously for Nafion 117 membranes.

Fe-N-C cathode was prepared using a Nafion content on the dry electrode of 50 wt. % and a catalyst loading of 2.5 mg cm<sup>-2</sup>. At the FC anode, a commercial Pt/C catalyst (Johnson Matthey, 40 wt% Pt) with a Pt loading of 0.3 mg cm<sup>-2</sup> was used. As a purpose of comparison, the performance of a PEMFC prepared using a commercial Pt/C catalyst (Johnson Matthey, 40 wt % Pt) with a Pt loading of 0.6 mg cm<sup>-2</sup> at the cathode was also evaluated [13]. In the case of Pt/C catalytic layer preparation, the Nafion content on the dry electrode was 4 wt. % for both anode and cathode. For the MEA preparation, the same hot pressing procedure described before was used. Anodic and cathodic compartment were fed with a 200 NmL min<sup>-1</sup> pure H<sub>2</sub> and pure O<sub>2</sub> flow, respectively. Both gas flows were preheated at 80 °C with and fed with a backpressure of 3 bar (relative). H<sub>2</sub> flow was fully humidified, while O<sub>2</sub> was fed without humidification. The temperature of the cell was maintained at 60 °C during the experiments.

#### 2.5.3. Alkaline DEFC test.

Fe-N-C was also tested as ORR catalyst in a direct ethanol fuel cell (DEFC) with an alkaline electrolyte membrane. In this case the single cell active area was 2.89 cm<sup>2</sup>. A commercial polybenzimidazole (PBI) membrane (Danish Power Systems) was used as electrolyte. In order to dope the membrane with OH<sup>-</sup> functionalities to induce in it the anionic conductivity, it was treated during 7 days into 6 M KOH solution. After this treatment, the membrane ionic conductivity get a value of around 0.01 S cm<sup>-1</sup> [14].

After the treatment in 6 M KOH, the PBI structure is modified as show in Figure 1.



**Figure 1.** Structure modification of PBI after treatment with 6 M KOH.

A commercial Pt-Ru/C catalyst (Johnson Matthey, 45 wt% Pt-Ru, Pt:Ru 1:1 atomic ratio) was used as anodic catalyst. As a comparison, the performance of a DEFC with a commercial Pt/C (Johnson Matthey, 40 wt % Pt) as cathodic catalyst was also evaluated. The electrodes were prepared by air-brushing the catalyst ink on a carbon cloth GDL in the same way as described in paragraph 2.5.1.

Fe-N-C cathodes were prepared with different Nafion content on the dry electrode: 4 – 33 – 50 wt. %. The catalyst loading was 2.5 mg cm<sup>2</sup>. For the Pt-Ru anode the Pt loading was 1.33 mg cm<sup>-2</sup> and the Nafion content on dry electrode was 4 wt. %. For the Pt cathode the Pt loading was 1 mg cm<sup>-2</sup> and the Nafion content was 4 wt. %. The electrodes and the membrane were assembled without hot pressing, by direct sandwiching at room temperature in the cell hardware [cit. Journal of Power Sources 196 (2011) 133–139]. The DEFC single cell polarization curves were performed as described in paragraph 2.5.1. The anode was fed with 2 M methanol and 2 M KOH solution preheated at 80 °C with a flow rate of 1 mL min<sup>-1</sup> and a pressure of 0.33 bar (relative). The cathode was fed with a 200 NmL min<sup>-1</sup> pure O<sub>2</sub> flow preheated at 80 °C with no humidification at 3 bar backpressure. The temperature of the cell was maintained at 90 °C during the experiments.

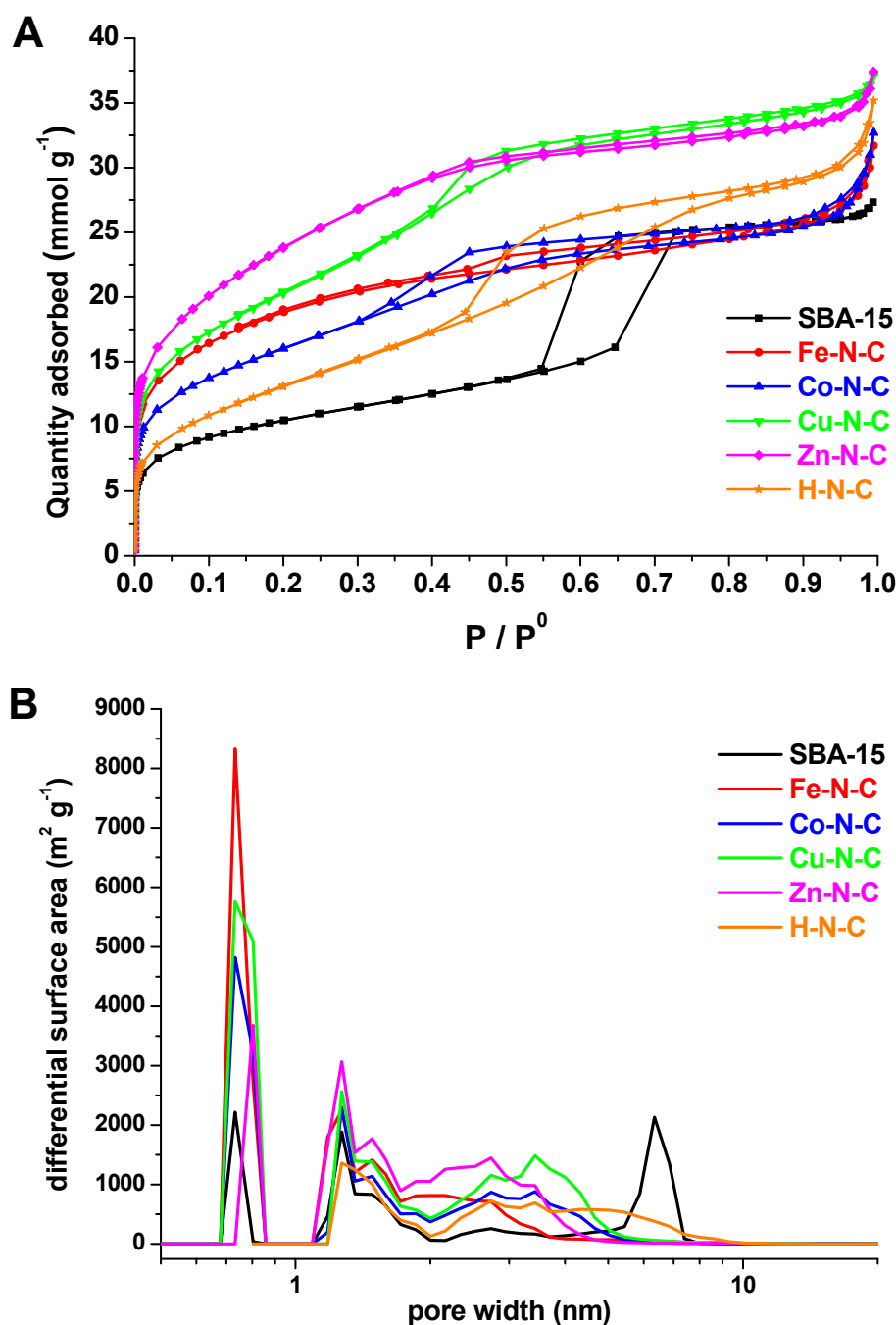
### 3. Results and discussion

#### 3.1. Physico-chemical characterization.

##### 3.1.1. N<sub>2</sub> adsorption-desorption analysis.

Nitrogen adsorption/desorption analysis was performed for all of the Me-N-C catalysts and for the SBA-15 silica used as template. The adsorption-desorption isotherms are shown in Figure 2A.





**Figure 2.** (A) N<sub>2</sub> adsorption and desorption isotherms of Me-N-C catalysts and SBA-15 silica. (B) Differential surface area distribution by DFT model.

According to the International Union of Pure and Applied Chemistry (IUPAC) classification, the SBA-15 isotherm shape belongs to type IV (a), which shows the typical hysteresis loop associated with capillary condensation taking place in mesopores [15,16]. The hysteresis loop shape can be classified as type H1, with the presence of the two almost vertical and parallel branches, associated with materials having a narrow distribution of pore size like ordered mesoporous silica.

The Me-N-C isotherms shape is typical of carbonaceous materials comprising all types of pores [17]. The isotherms can be classified as type I(b) at  $P/P^0 < 0.05$ , where filling of the micropores by the

adsorbate occurs. Type I(b) isotherm character is typical of microporous materials having pore size distributions over a broad range of size including narrow mesopores ( $< \sim 2.5$  nm) [16]. At  $P/P^0$  values  $> 0.05$  the isotherms become similar to type II. The hysteresis loops types do not belong to any of the IUPAC classification categories. They have an intermediate character between type H1 and H4, being more horizontal and extended over a wide range of  $P/P^0$ . Moreover, the presence of hysteresis is more evident for H-N-C, while it is almost inappreciable for Zn-N-C.

The BET surface areas and the micropores areas and volumes of all the samples are shown in Table 1. Materials with a high specific surface area and a high micropores content are obtained as negative replica of the SBA-15 silica template. However, the presence/absence and the type of transition metal in the phthalocyanine precursor molecule have an important influence on the surface area, micropores content and pore size distribution (see Figure 2B) of the final material. In particular, regarding the pore size distribution, for the catalyst synthesized starting from precursor without metal (H-N-C), no micropores with diameter less than 1 nm are formed. On the contrary, for the phthalocyanine precursors containing a metal, a certain amount of micropores with diameter in the range 0.5 – 0.8 nm are detected, as well as micropores with diameter between 1 and 2 nm and mesopores in the range 2 – 5 nm.

**Table 1.** Properties calculated from the nitrogen physisorption analysis for the Me-N-C catalysts and the SBA-15 silica template.

| Sample | BET surface area<br>[m <sup>2</sup> g <sup>-1</sup> ] | Micropores surface area by DFT<br>[m <sup>2</sup> g <sup>-1</sup> ] | % of microporosity | Micropores volume by DFT<br>[cm <sup>3</sup> g <sup>-1</sup> ] |
|--------|---|---|--------------------|--|
| SBA-15 | 797   | 255   | 32.0               | 0.152  |
| Fe-N-C | 1508  | 730   | 48.4               | 0.394  |
| Co-N-C | 1260  | 512   | 40.7               | 0.275  |
| Cu-N-C | 1624  | 647   | 39.8               | 0.342  |
| Zn-N-C | 1948  | 533   | 27.4               | 0.352  |
| H-N-C  | 1078  | 167   | 15.5               | 0.123  |

The presence of different metals in the precursor molecule induces the formation of a different porous structure in the material during the heat treatment, although the silica template used is the same. This could influence the accessibility of the reactants to the electrocatalytic active sites, as well as the formation of the same active sites. This could also explain the results of the TGA-mass spectroscopy, where many differences have been found between the different samples (see Paragraph 3.1.7). The

importance of the pore size for the kinetic activity in this type of NPMC was outlined in several works [17,18]. In particular, the formation of a microporous structure is favorable to host the ORR active sites [19–22]. However, no direct relation between the ORR activity and the BET surface area or the microporous surface area were found. In this case, the ORR activity in both acidic and alkaline conditions (see Paragraphs 3.2.2 and 3.3.1) seems to increase as the % of microporosity (calculated as ratio between the microporous surface area and the overall BET surface area) of the sample increases.

### 3.1.2. FESEM pictures.

The morphology of all the Me-N-C catalysts and the SBA-15 silica template was investigated by FESEM analysis. The SBA-15 silica exhibits the typical uniform rod-like morphology [23]. These short rod-like particles have an average length of about 1  $\mu$ m and an average thickness of about 200 nm, and they are joined together to form larger agglomerates (see Figure S1 A-B-C-D in Chapter 4). Pictures of the Me-N-C catalysts are shown in Figure 3 – 4 – 5 – 6 and 7. As can be seen, all of the samples exhibit a rod-like / agglomerate morphology, similarly to the silica template.

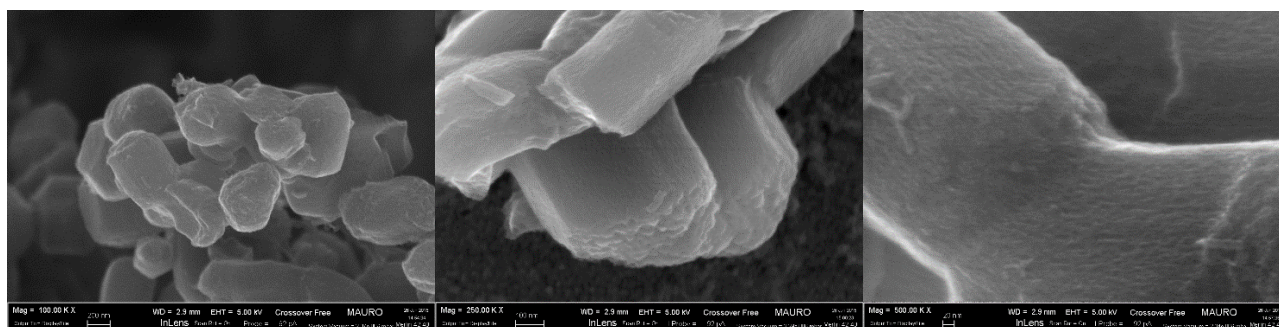
Similar morphologies were obtained by other groups for materials obtained by hard-templating method of SBA-15 silica [24,25].

However, considering the dimensions, one can notice that the average thickness of the particles is similar to the SBA-15 (about 200 nm). Otherwise, the average length of the particles appears to be lower in comparison with the SBA-15 template. The channel-like pores of the SBA-15 silica lie along the length direction. Therefore, the lower length of the Me-N-C catalysts particles can be explained as an incomplete filling of the empty space inside the channels by the Me-phthalocyanine precursor during the wet-impregnation. In this way, the negative replica of the template occurred only partially along the channel-like pores length direction, giving rise to shorter carbonaceous particles the removal of the SBA-15 template.

The effect of the use of different Me-phthalocyanines (Me = Fe, Co, Cu, Zn, or no metal) precursors on the morphology is also evident. The Fe-N-C catalyst has a composite morphology where different zones can be identified (see Figure 3 A). The rod-like particles originated from the SBA-15 structure replica are surrounded and interconnected by a less uniform and disordered structure. Observing the pictures taken at higher magnification, this disordered region appears to be formed by two different parts. The first one, shown in Figure 3 B, has the shape of root-like filaments. The second one are tangled carbon nanotubes that originate from the surface of the filaments and the rod-like particles. The average diameter of these nanotubes is of about 10 nm (see Figure 3 C).

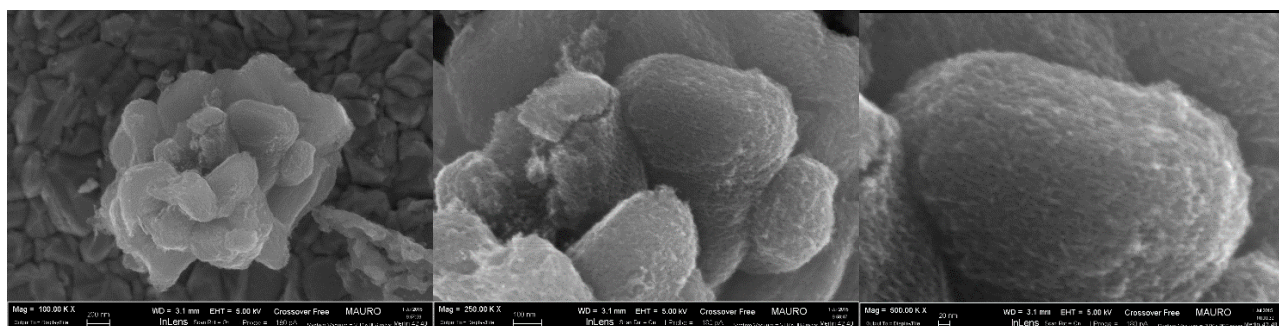


Almost no irregularities are present on the surface of the Zn-N-C catalyst. The rod-like particles in this catalyst are more regular and round-shaped (see Figure 6 A), and the surface appears to be smoother in comparison with the previous samples. In the pictures taken at higher magnifications (Figure 6 B-C), traces of the regular channel-like structure typical of the SBA-15 silica template can be observed.



**Figure 6.** FESEM images of Zn-N-C catalyst at different magnifications.

Finally, analyzing the morphology of the catalysts synthesized starting from the metal-free phtahalocyanine (H-N-C), we can notice that the particles agglomerates shapes are regular, similarly to Zn-C-N, and do not show the presence of nanotubes or other different structures. However, unlike the Zn-N-C, the surface is more wrinkled and rough, being the channel-like structure more evident. Moreover, unlike all the other samples, the presence of pores on the surface is more evident. Therefore, these surface pores should be of bigger size in comparison with the ones of the other Me-N-C catalysts. This fact could confirm the lower microporosity of this sample (Table 1), as well as the results of the pore size distribution analysis (Figure 2B).



**Figure 7.** FESEM images of H-N-C catalyst at different magnifications.

### 3.1.3. EDX analysis.

All of the catalysts synthesized using a phthalocyanine molecule containing a metal were analysed by EDX. The purpose of the analysis was to determine the metal content in each sample. The probe depth for EDX ( $\geq 1 \mu\text{m}$ ) makes it possible to consider the results of this analysis as bulk composition [28]. The results are shown in Table 2. For all of the samples the transition metal atomic content is lower than in the Me(II)-phthalocyanine molecule precursor (1.75 atomic %). This indicates that not all of the initial metal content remains stably incorporated into the final catalyst structure. Some of the metal in the form of moieties not strongly linked to the catalysts structure, could have been washed away during the HF washing for the silica template removal. No Si or F impurities have been detected, sign that the HF washing is very effective in removing the silica template and it does not alter the chemical composition of the catalysts. However, all of the samples exhibit a not negligible oxygen content, despite no oxygen is contained in the Me(II)-phthalocyanines precursors molecules. This fact can be attributed to two different reasons. First, considering that the only oxygen source present into the pyrolysis reactor is the silica template, some of its O atoms could have been incorporated into the catalysts structure due to the high temperatures reached during the pyrolysis. The second reason could be the presence of some leaching in the sealing system of the tubular reactor used for the pyrolysis, from which atmospheric air could have entered, causing a partial oxidation of the carbonaceous material.

**Table 2.** Elemental analysis by XPS (surface composition) and EDX (bulk composition) of the Me-N-C catalysts.

|        | Chemical composition – <b>XPS</b> / <b>EDX</b> [atomic %] |                   |                |                   |                       |
|--------|---|-------------------|----------------|-------------------|-----------------------|
| Sample | C   | O                 | N              | M                 | Tot                   |
| Fe-N-C | <b>89.5</b> / 93.10                                       | <b>5.4</b> / 6.26 | <b>5.0</b> / - | <b>0.1</b> / 0.64 | <b>100.0</b> / 100.00 |
| Co-N-C | <b>90.1</b> / 92.37                                       | <b>4.4</b> / 7.11 | <b>5.1</b> / - | <b>0.4</b> / 0.52 | <b>100.0</b> / 100.00 |
| Cu-N-C | <b>87.3</b> / 93.80                                       | <b>4.7</b> / 5.95 | <b>7.9</b> / - | <b>0.1</b> / 0.25 | <b>100.0</b> / 100.00 |
| Zn-N-C | <b>89.0</b> / 95.62                                       | <b>2.2</b> / 3.82 | <b>8.3</b> / - | <b>0.5</b> / 0.56 | <b>100.0</b> / 100.00 |
| H-N-C  | <b>92.9</b> / -   | <b>3.6</b> / -    | <b>3.5</b> / - | <b>0.0</b> / -    | <b>100.0</b> / 100.00 |

### 3.1.4. XPS analysis.

All of the samples were analyzed by XPS after the removal of the SBA-15 silica template by HF washing. The XPS analysis was conducted in order to determine more precisely the chemical composition of the catalysts surface, detecting the presence of nitrogen. The influence of the different

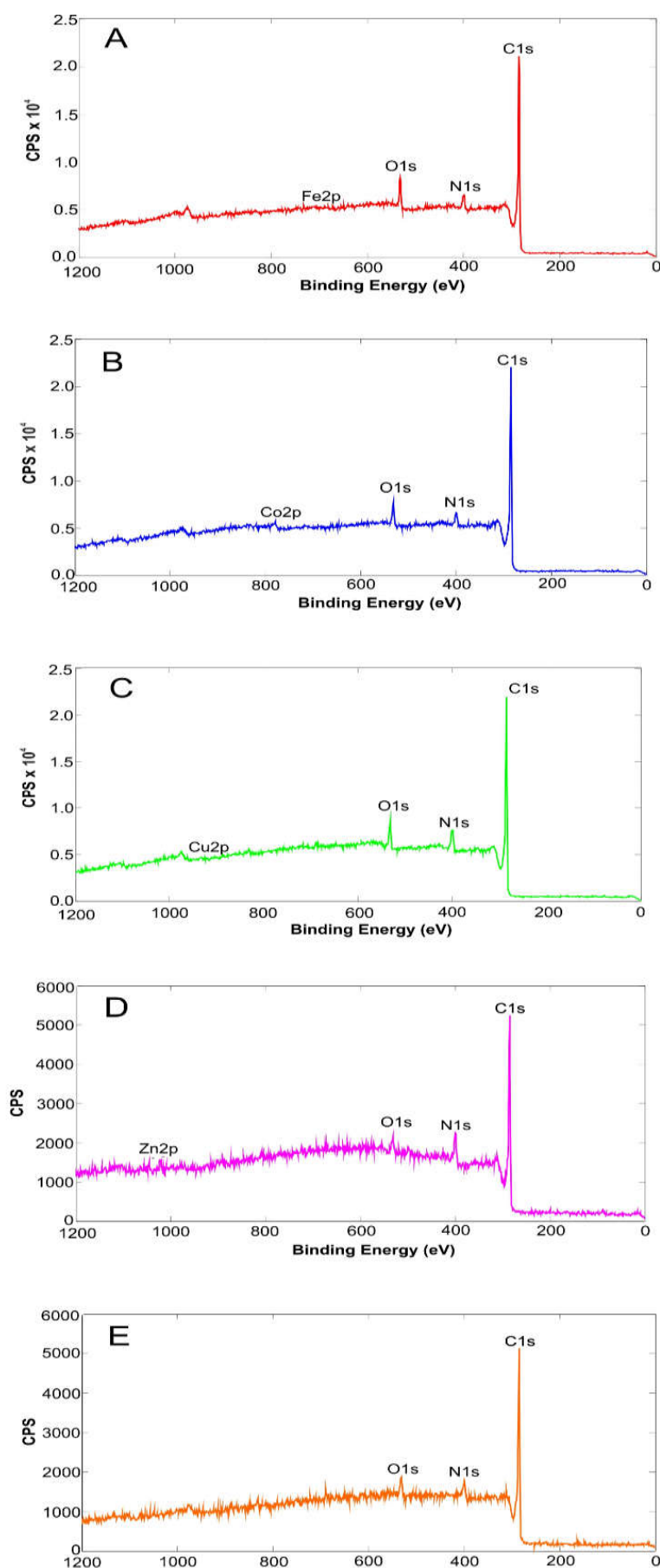


transition metals in the MePc precursor on the composition of the catalyst can be also noticed. The XPS survey spectra are shown in Figure 8, and the overall surface elemental compositions are summarized in Table 2.

In all of the samples, the main component is C (total content of about 90 at. %, total C content in the precursor molecule is 56 at. %) confirming a good carbonization of the precursor occurring during the pyrolysis. O was also detected in not negligible percentages even if lower in comparison with EDX results. N was detected in all the five samples, and its content varies from 3.5 to 8.3 at. %. These amounts are lower than the original N content of the precursor molecule (14 at. %). Therefore, some of the nitrogen is lost during the pyrolysis in the form of N-containing gas molecules (see discussion in Paragraph 3.1.7). It is evident how the different transition metals seem to have the capacity of fixing different quantities of nitrogen during the pyrolysis under inert atmosphere, leading to the obtainment of different levels of N-doping in the final carbonaceous material. More in detail, the “ability” of fixing the nitrogen seems to decrease in the order  $\text{Zn} > \text{Cu} > \text{Co} > \text{Fe}$ . The presence of a metal seems to be beneficial in any case. In fact, using the H-Pc molecule as a precursor, the lower N-doping level was obtained.

Concerning the transition metal content, in Fe-, Co- and Cu-N-C catalysts the amount detected by XPS is lower than the amount detected by EDX. Considering that XPS is a surface sensitive technique (the depth of the analysis being about 5 – 6 nm) [29], these results suggest that a certain quantity of the metal remains incorporated in the bulk of the carbonaceous structure of the catalysts, not being exposed to the surface. On the contrary, for the Zn-N-C catalyst, there is a good matching between the Zn amounts detected by EDX and XPS. This could suggest that Zn is mainly located on the catalyst surface or close to the surface.

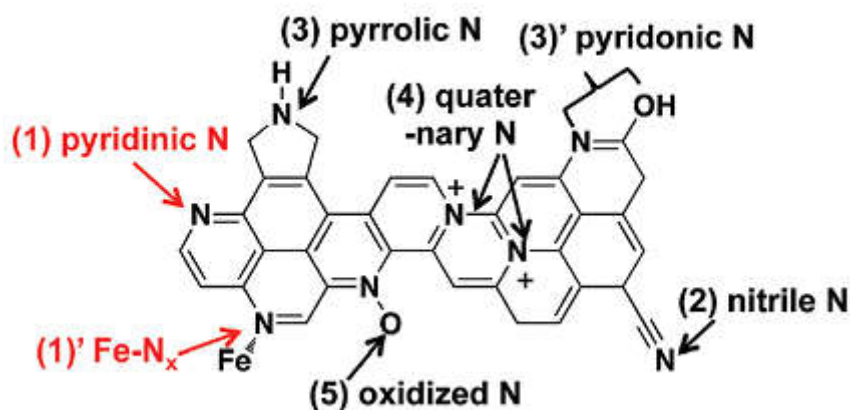
However, the transition metals contents detected are too low to allow the determination of the metal valence state via deconvolution of the high-resolution Me 2p peaks (not reported here). Therefore, the valence state of the metals in these catalysts remains unclear. We can hypothesize some of the metal atoms being coordinated to N atoms in the form of Me-N<sub>x</sub> moieties, forming some of the ORR catalytic active sites [21]. For example, for the Fe-N-C catalysts, some presence of Fe-N<sub>x</sub> bonds results from the N 1s peak deconvolution analysis. The transition metals could also be present in the form of Me-nitrides or Me-carbides encapsulated inside the carbon structure of the catalysts [30–32]. No impurities of other elements such as Si or F are detected, confirming the goodness of the washing treatment with 5 wt. % HF solution for the removal of the templating agent.



**Figure 8.** XPS survey spectra of Fe-N-C (A), Co-N-C (B), Cu-N-C (C), Zn-N-C (D) and H-N-C (E) catalysts.



The high resolution spectra N 1s peaks were analyzed by deconvolution. Five different components have been identified, corresponding to imine or nitrile (N1), pyridinic (N2) nitrogen bonded to metal (N3), graphitic or pyrrolic (N4) and oxidized (N5) [17, 33–35].



**Figure 9.** Different nitrogen bonding types that can be detected by deconvolution of the XPS high resolution N 1s peak [36].

The relative and total (referred to the overall nitrogen content of the sample, see Table 2) amounts of the different nitrogen bond types are shown in Table 3, with their respective binding energy.

The relative content of the different nitrogen types differs from catalyst to catalyst. This suggests that, apart from the total N content, the presence of a different metal in the precursor affect the incorporation of the N in different forms.

**Table 3.** Relative and total contents of the different N types with their respective peak binding energies resulting from the deconvolution of the high-resolution N 1s peak from XPS analysis (N1: nitrile-N; N2: pyridinic-N; N3: Me-N<sub>x</sub>; N4: graphitic- or pyrrolic-N; N5: oxidized-N).

| <i>Binding energy [eV]</i><br><b>Relative content [atomic %]</b><br>Total content [atomic %] |                             |                             |                            |                             |                             |
|--|-----------------------------|-----------------------------|----------------------------|-----------------------------|-----------------------------|
| Sample   | N1                          | N2                          | N3                         | N4                          | N5                          |
| Fe-N-C   | 397.9<br><b>12.5</b><br>0.6 | 398.6<br><b>26.9</b><br>1.3 | 399.6<br><b>2.0</b><br>0.1 | 400.5<br><b>41.6</b><br>2.1 | 403.4<br><b>17.0</b><br>0.9 |
| Co-N-C   | 398.3<br><b>31.3</b><br>1.6 | 399.1<br><b>14.2</b><br>0.7 | -<br>-<br>-                | 400.8<br><b>43.1</b><br>2.2 | 404.2<br><b>11.5</b><br>0.6 |
| Cu-N-C   | 398.1<br><b>31.8</b><br>2.5 | 399.2<br><b>8.5</b><br>0.7  | -<br>-<br>-                | 400.6<br><b>36.6</b><br>2.9 | 403.0<br><b>23.1</b><br>1.8 |
| Zn-N-C   | 398.0<br><b>29.8</b><br>2.5 | 398.6<br><b>2.2</b><br>0.2  | -<br>-<br>-                | 400.0<br><b>67.7</b><br>5.3 | 404.1<br><b>4.2</b><br>0.3  |
| H-N-C  | 398.1<br><b>33.6</b><br>1.2 | 399.1<br><b>5.1</b><br>0.2  | -<br>-<br>-                | 400.6<br><b>61.3</b><br>2.1 | -<br>-<br>-                 |

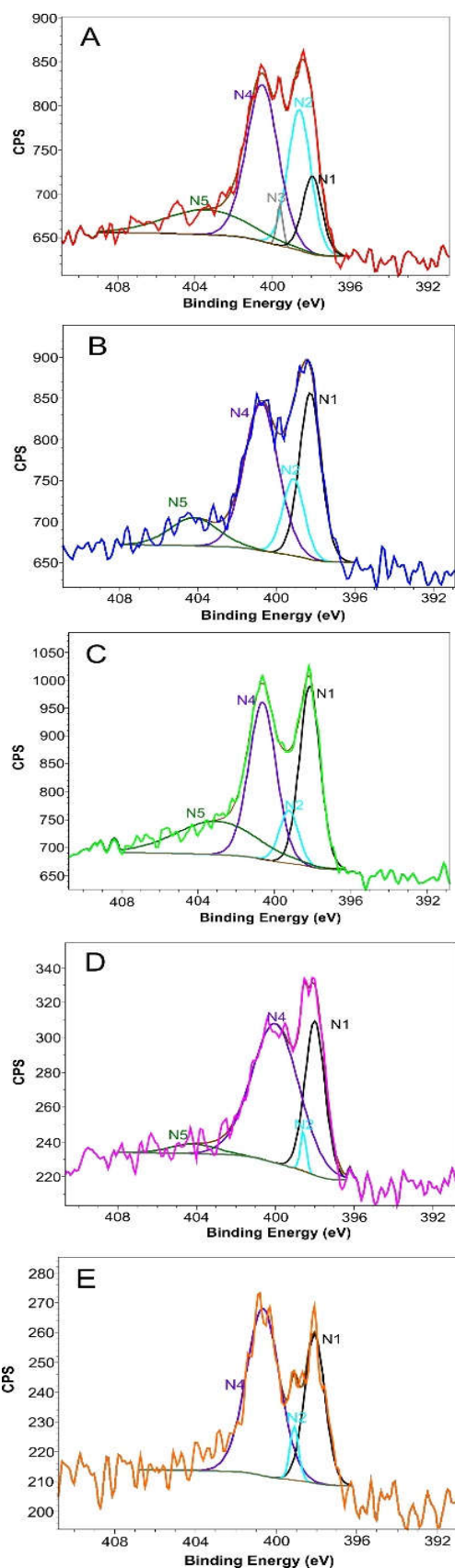
In particular, Fe-N-C is the catalyst with the highest content of pyridinic-N, in both relative and absolute terms. On the contrary, its relative content of nitrile or imide-like N is the lowest (12.6 %), while for the other catalysts it is around 30 %. Fe-, Co- and Cu-N-C catalysts have a similar relative content of graphitic-N (around 40 %). For Zn- and H-N-C the graphitic-N is more abundant (67.7 and 61.3 % respectively). A certain amount of oxidized N is detected in all the samples, except for H-N-C. For Co-N-C the amount of pyridinic-N is still remarkably high (14.2 %), but it tends to decrease in Cu-N-C (8.5 %), and even more in Zn-N-C and H-N-C.

Therefore, the different metals seem to favor the formation of pyridinic-N defects in the order Fe > Co > Cu > Zn. This order reflects the % of microporosity of the samples.

Nitrogen-doping is with an increase of the ORR catalytic activity of carbon based materials in both acidic and alkaline conditions [37–39]. However, the role of the real “electrocatalytically active sites” is still not clear [21]. Regarding the different types of N bonding, in many studies, the electrocatalytic activity is attributed to pyridinic-N [18,26,40].

The number of available doping sites for N-doping is greater in the basal plane of graphitic carbon than in the edge. Therefore, the nitrogen-doping occurring in a basal plane of carbon should be more favorable than in edge sites [41]. The different transition metals actuate each one in a different way during the pyrolysis process, when the N is actually incorporated into the carbon structure of the

catalysts. Each metal seems to favor in a different way the formation of the different nitrogen bonds types. This, together with the final catalyst morphology and porous structure, have an important influence on the formation of effective ORR catalytic sites. For example, the location of the ORR active sites in micropores, as proposed by many groups [17,18,22], being the active site a pyridinic-N atom in the edge-of-plane coordinated or not with a transition metal, could be confirmed by these results. In fact Fe-N-C is the most active catalyst, and also the catalyst with the highest microporosity and the highest pyridinic-N content.



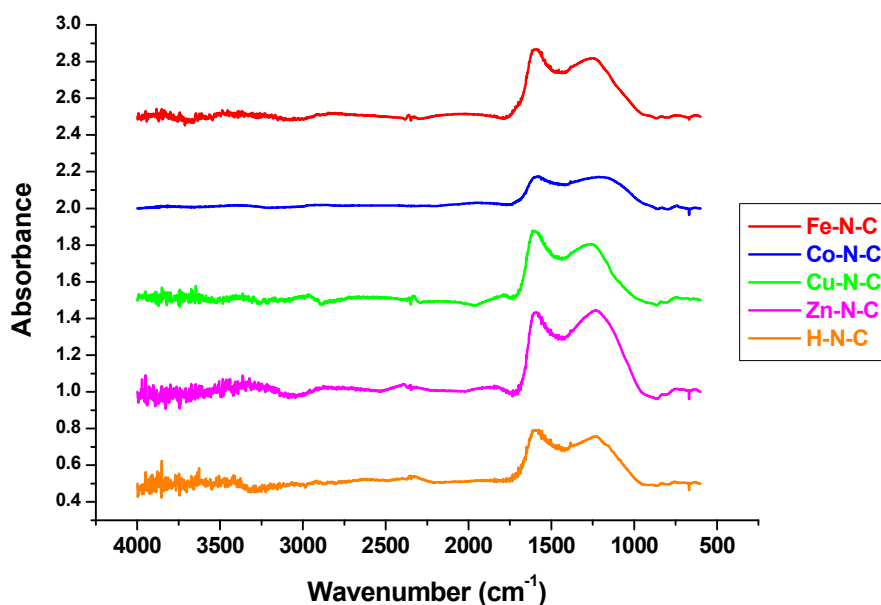
**Figure 10.** High resolution N 1s XPS spectra of the catalysts Fe-N-C (A), Co-N-C (B), Cu-N-C (C), Zn-N-C (D) and H-N-C (E) with the peak deconvolution analysis in the different N-bonding types. The black, light blue, grey, violet and dark green lines correspond to nitrile (N1), pyridinic (N2), Me-N<sub>x</sub> (N3), graphitic/pyrrolic (N4) and oxidized (N5) nitrogen bondings, respectively.

By concluding, using Fe- and Co-phthalocyanine precursors, more active ORR catalysts are obtained. These catalysts exhibit a lower total N content detected by XPS. Nevertheless, they have a higher relative and total content of pyridine-N, and this could be related with their enhanced ORR electroactivity. The pyridinic-N is located on the edge of a carbon plane and a carbon vacancy and it has a lone electron pair in the plane of the carbon matrix. This can increase the electron-donor property of the catalyst which will weaken the O–O bond via the bonding between oxygen and nitrogen and/or the adjacent carbon atom, facilitating the ORR [42].

Cu- and Zn-phthalocyanine precursors are able to incorporate more N, but mainly in form of graphitic, nitrile and oxidized type. These N types are less likely to be involved in ORR active sites [43,44]. Cu presence gives rise to a catalyst with a lower ORR activity, especially in acidic conditions (see Paragraph 3.2.2). The influence of Zn on the formation of ORR active sites in particular seems to be insignificant, being Zn-N-C activity almost identical to the activity of H-N-C catalyst in both acid and alkaline media (see Electrochemical characterization results in Paragraphs 3.2.2 and 3.3.1).

#### 3.1.5. FTIR analysis.

FTIR analysis was performed for all the five catalysts after the silica template removal, and the resulting spectra are shown in Figure 8. After pyrolysis, most of the peaks characteristic of the phthalocyanine molecule in the “fingerprint” wavenumber region between 1700 and 700  $\text{cm}^{-1}$  (not reported here, see Figure 2B in Chapter 5) disappear. All of the pyrolyzed Me-N-C catalysts spectra have a similar shape, resembling the typical spectrum of carbonaceous materials, which are highly transparent to the IR radiation in the region between 400 and 4000  $\text{cm}^{-1}$  [25]. The FTIR spectra of Me-N-C catalysts exhibit only two broad absorbance peaks in the ranges 1650–1500  $\text{cm}^{-1}$  and 1350–1150  $\text{cm}^{-1}$ . These peaks can be attributed to C=N bonding (i.e. pyridine-type) and N–H bonding found on N-containing carbon materials [45]. Similar results are reported in the literature for different types of pyrolyzed Me-N-C electrocatalysts [46,47]. This finding suggests that the original phthalocyanine structures of the precursors are totally decomposed during the pyrolysis process, with a substantial recombination of the chemical bonding. A small peak at about 2300  $\text{cm}^{-1}$  is detected in some samples, and it can be attributed to the presence of nitrile  $\text{C}\equiv\text{N}$  functional groups [48], as also found by XPS analysis (see Paragraph 3.1.4). However, no significant differences are observed between the spectra of the different Me-N-C catalysts with this analysis technique.



**Figure 8.** FTIR spectra of the Me-N-C catalysts after the silica template removal.

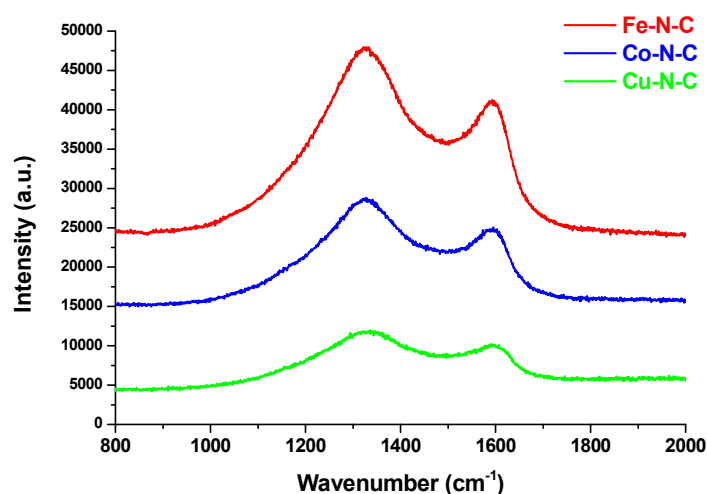
### 3.1.6. Raman analysis.

The Raman spectra were recorded for Fe-N-C, Co-N-C and Cu-N-C, that is, for the three more electroactive catalysts. This analysis was conducted to evaluate the order/disorder degree of the crystalline carbon structure. The G band (with peak intensity at  $\sim 1300\text{ cm}^{-1}$ ) is a characteristic feature of graphitic layers, while the D band (with peak intensity at  $\sim 1600\text{ cm}^{-1}$ ) corresponds to disordered carbon or defective graphitic structures [45]. The results are shown in Figure 9. From the ratio between the intensities of the D band and the G band, the ratio between the disordered and the graphitic carbon structure can be estimated. Therefore, a high  $I_D/I_G$  band intensity ratio indicates the presence of high amounts of defects [49]. These defects can be caused by the incorporation of hetero-atoms (e.g., nitrogen or oxygen) and/or of  $\text{sp}^3$ -hybridized carbon atoms in  $\text{sp}^2$  graphene lattices [27,50,51].

No presence of any additional peak between G and D band, attributed to incomplete carbonization [45], was detected for these catalysts, suggesting that the phthalocyanine precursors get a good degree of carbonization during the pyrolysis process. In particular, during this heat treatment at high temperature under inert atmosphere, two phenomena take place: the precursor graphitization forming a carbonaceous structure, and the simultaneous doping of this structure with some of the N atoms present in the precursor molecule [27]. The former is responsible of the electronic conduction of the material, and the latter of the formation of the ORR active sites.

The graphitization process leads to a lower  $I_D/I_G$  ratio [52], while the doping with nitrogen causes an increase of defects in the carbon phase, that leads to an increase of the  $I_D/I_G$  ratio, as well as to a

broadening of D and G peaks [53]. Thus, the final value of the  $I_D/I_G$  ratio is the net effect of the sum of its decrease due to further graphitization and its increase due to nitrogen introduction in the structure. The  $I_D/I_G$  ratios calculated from Figure 9 are 1.22, 1.19 and 1.11 for Fe-N-C, Co-N-C, and Cu-N-C, respectively. These values are very similar to each other, suggesting that Fe, Co and Cu have a similar influence on the graphitization and N-doping level during the pyrolysis, as also confirmed by XPS and FTIR results.

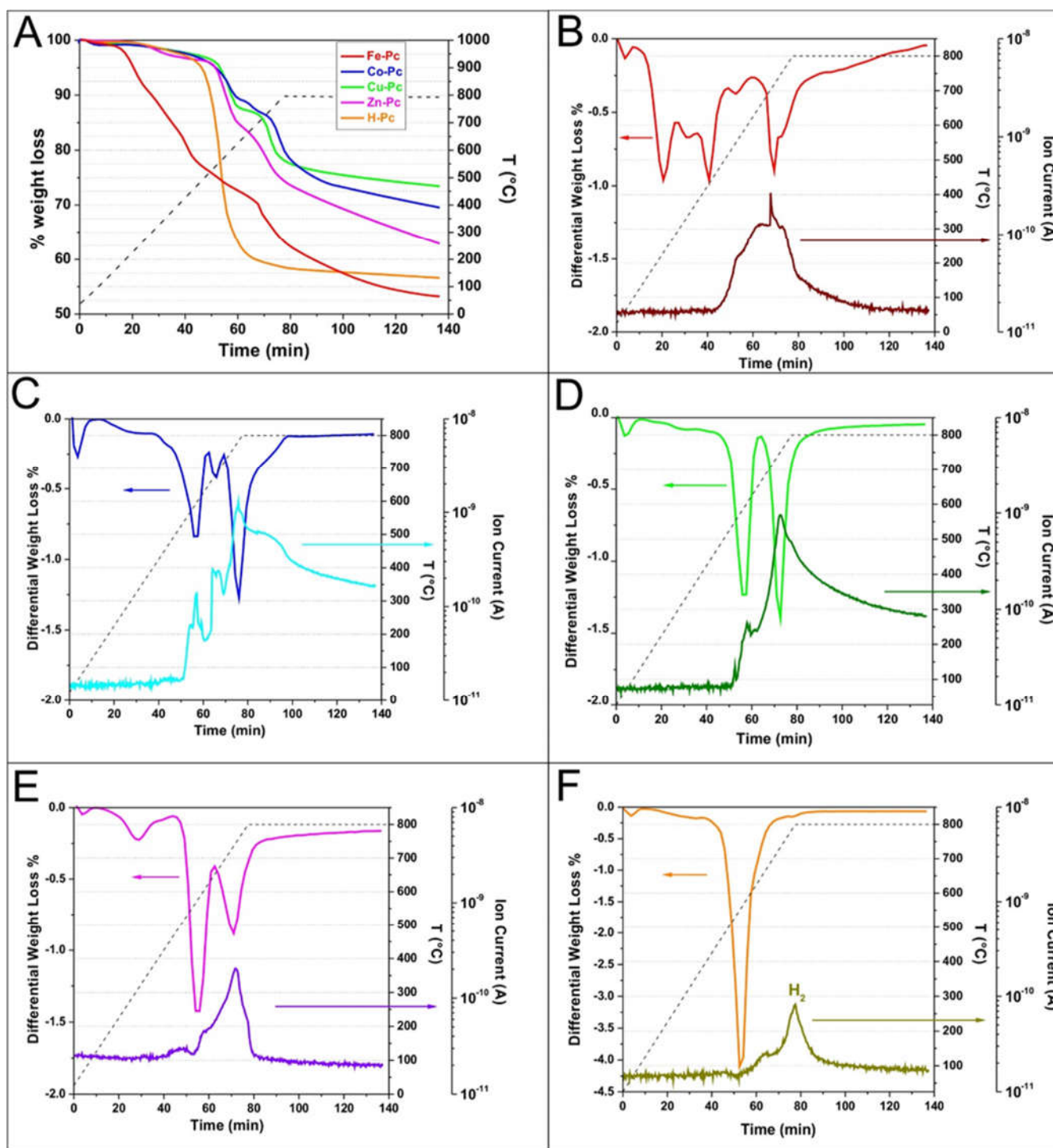


**Figure 9.** Raman spectra of Fe-N-C, Co-N-C and Cu-N-C catalysts.

### 3.1.7. Thermogravimetric analysis coupled with mass spectroscopy.

A thermogravimetric analysis (TGA) was conducted under inert atmosphere on all of the Mepthalocyanine samples after the impregnation on the SBA-15 silica. The outlet of the TGA chamber was connected to a mass-spectroscopy analyzer. The purpose was to simulate the pyrolysis process [54] and investigate the behavior of the different Me-Pc precursors during the thermal treatment, detecting the weight loss as well as the type and amounts of gases evolved. In order to get semi-quantitative data from the mass-spectroscopy analysis, a fixed amount of each sample was introduced in the TGA chamber at the beginning of the experiment.

If we observe the integral TGA curves in Figure 10 A, and the respective differential plots (Figure 10 B-C-D-E-F) we can approximately identify four main different weight loss regions, corresponding to the main differential peaks.



**Figure 10.** (A) TGA plot of the different phthalocyanines precursors. Derivative TGA curve with ionic current detected at the mass-spectrometer associated with  $H_2$  for Fe-Pc (B), Co-Pc (C), Cu-Pc (D), Zn-Pc (E) and H-Pc (F).

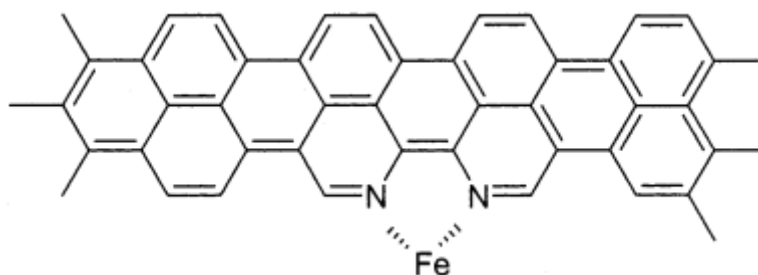
- 1) 100 °C: adsorbed moisture evaporation [37, 54–56].
- 2) 250 – 450 °C: sublimation of phthalocyanine precursors on SBA-15 surface and/or partial phthalocyanine decomposition. Similar to other macrocycles, macromolecules or polymers (i.e. hemicellulose, pectine, cellulose), phthalocyanine can suffer partial decomposition in this



temperature range [55,56,58]. Molecules at lower molecular weight can be formed, with the possible formation of a sort of char [59,60].

3) 500 – 600 °C: sublimation of phthalocyanine precursors inside SBA-15 pore channels and / or further phthalocyanine decomposition. Decomposition of organic macromolecules and polymers like lignin can occur in this range of temperature, also overlapping with the previous stage [54]. Also the char formed at lower temperatures could undergo volatilization [56]. The evolution of H<sub>2</sub> and other gaseous molecules containing nitrogen (i.e. NH<sub>3</sub> and HCN, see Figure 12) occurs.

4) 650 – 800 °C: formation of cracking products due to reducing conditions. In this last decomposition step, further dehydrogenation and elimination of nitrogen containing molecules takes place. Aromatization of the carbonaceous structure (graphitization process) is occurring in this step [56]. At temperatures around 700 °C, the pyrolysis of Me-phthalocyanines can produce fragments containing transition metal bound to C and N on the catalyst surface. Some of these fragments may be involved in the N-4 ORR active sites [61,62].



**Figure 11.** Proposed moiety of the ORR catalytic site formed at high temperature [61].

Despite this basic general classification, some differences have been detected between the different Me-phthalocyanines precursors in the TGA diagram shape and in the evolution of pyrolysis gas products as well. This fact confirm that this pyrolysis process under inert atmosphere is strongly dependent on the transition metal coordinated in the macrocycle precursor center.

Considering the differential TGA curve of the H-Pc precursor (Figure 10 F), it exhibit only one very sharp peak at 550 °C, suggesting that in the absence of any coordinated transition metal ion, H-Pc rapidly decomposes and / or sublimates in the temperature range between 500 and 600 °C. This behavior is similar to other macrocycles and nitrogen containing ligand molecules without coordinated metal ion [37,63]. The hypothesis of the sublimation is supported by the general decrease of the carrier gas flow (Ar) detected by the mass-spectrometer analyzer in correspondence of the differential TGA peak (not reported here). The sublimated molecules, in fact, could have condensate inside the mass-spectrometer inlet tube, causing a partial occlusion and a consequent decrease of the total inlet flow.

Considering the Me-phthalocyanine molecule structure ( $C_{32}H_{18}N_8Me$ ) the pyrolysis gas products that have been considered for the detection by the mass-spectrometer are  $H_2$ ,  $N_2$ ,  $NH_3$ ,  $HCN$  and  $CH_4$ , that is, low molecular weight molecules containing C, N and H atoms. However, the ionic currents associated with  $NH_3$  and  $HCN$  masses registered by the mass-spectrometer are of about one order of magnitude lower than the currents associated to  $H_2$ . The carrier gas (Ar) and  $H_2O$  coming from the adsorbed moisture have also to be considered.

In the case of H-Pc,  $HCN$  and  $NH_3$  peaks have been detected in correspondence of the weight loss peak at  $550\text{ }^{\circ}C$  (see Figure 12), while  $H_2$  generation has been detected between  $700$  and  $800\text{ }^{\circ}C$ , corresponding to the dehydrogenation – graphitization process occurring in this temperature range.

If one looks at the differential TGA curve of the phthalocyanines precursors containing a transition metal, they have a more complicated behavior. In these samples, the weight loss occurs in different steps more evidently. Examining more in detail the TGA for each Me-Pc it can be noticed that all of them exhibit the peak of adsorbed water release at about  $100^{\circ}C$ . Regarding the weight loss in the range  $250 - 450\text{ }^{\circ}C$ , Co-, Cu- and Zn-Pc show a lower mass loss of less than 5 %. On the contrary, the mass loss of Fe-Pc in this zone is more marked, reaching about 20 %. For all of these samples, as also for H-Pc, no peaks related with the formation of  $NH_3$  and  $HCN$  (see Figure 12) and  $H_2$  (see Figure 10) have been detected. This confirms that the weight loss in this region could be related to the decomposition / sublimation of the phthalocyanine.

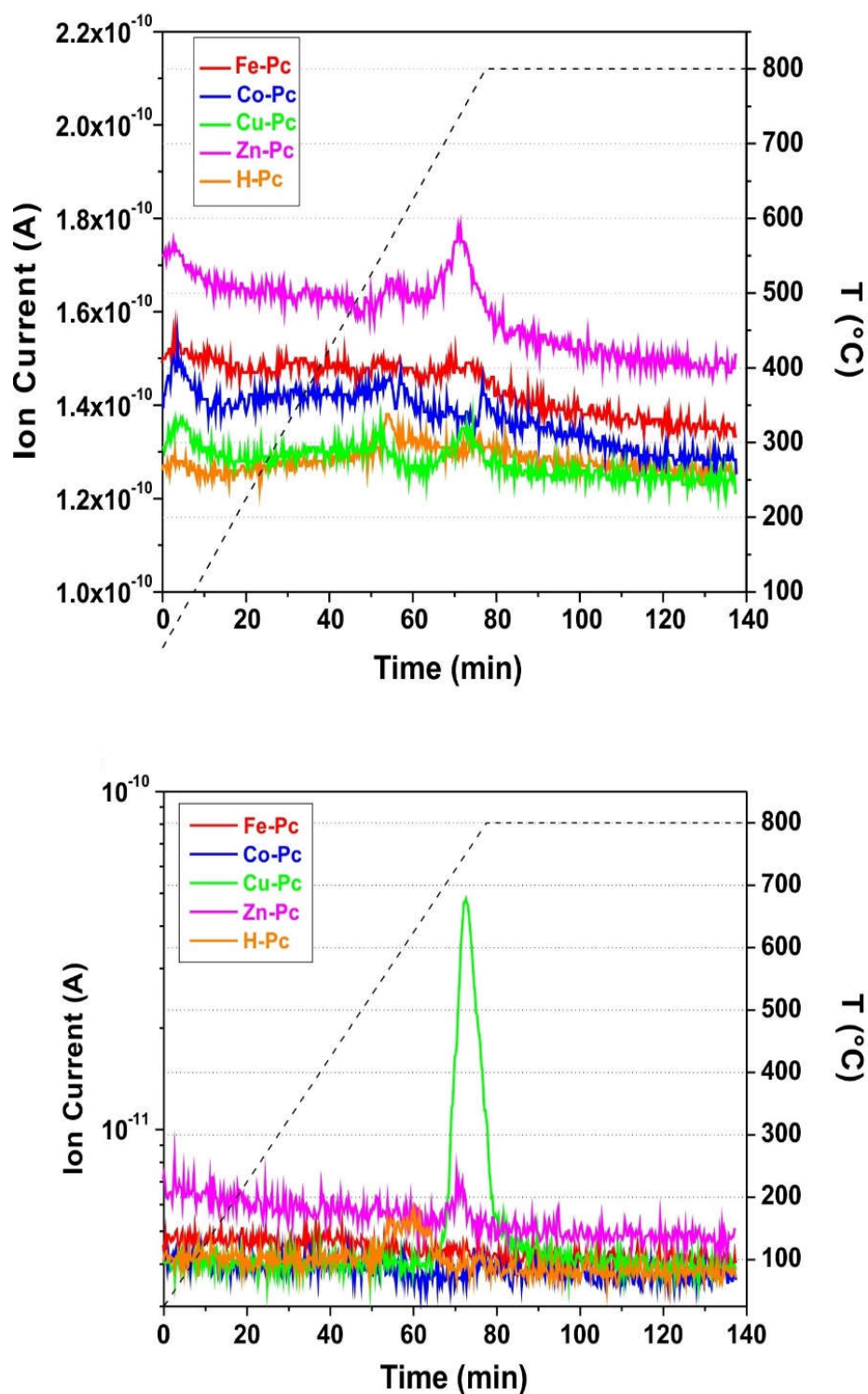
Some differences are noticed also in the temperature range  $550 - 800\text{ }^{\circ}C$ . In particular, for Zn-Pc (Figure 10 E), two major weight loss peaks are observed at  $550$  and  $700\text{ }^{\circ}C$ . The first peak is higher, and associated with the formation of  $H_2$  and few  $NH_3$ , while during the second one  $H_2$ ,  $NH_3$  and  $HCN$  is detected.

Cu-Pc (Figure 10 D) exhibits the two major differential weight loss peaks at  $600$  and  $750\text{ }^{\circ}C$  with almost the same intensity. The peak at  $600\text{ }^{\circ}C$  is associated with the formation of  $H_2$  and  $NH_3$ . The peak at  $750\text{ }^{\circ}C$  is associated with the presence of  $H_2$ ,  $NH_3$  and  $HCN$  (big peak) formation detected by the mass spectrometer.

Co-Pc (Figure 10 C) shows three peaks corresponding to  $600$ ,  $700$  and  $800\text{ }^{\circ}C$ . All these three peaks are associated with evolution of  $H_2$ , as evident in Figure 10 C. No peaks associated with the production of other gases are detected.

Regarding Fe-Pc (Figure 10 B), its behavior is similar to Co-Pc, with the presence of three differential peaks. Nevertheless, in this case, a first intense peak is registered at  $450\text{ }^{\circ}C$ , the second smaller peak is detected at  $550\text{ }^{\circ}C$ , while the third peak, having almost the same intensity of the first one, is registered at  $700\text{ }^{\circ}C$ . At the same time, a broad  $H_2$  generation peak is registered starting from  $450\text{ }^{\circ}C$  until about  $800\text{ }^{\circ}C$ . An intense top-peak is detected exactly in correspondence with the  $700\text{ }^{\circ}C$

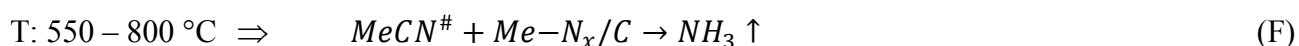
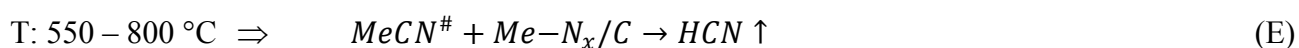
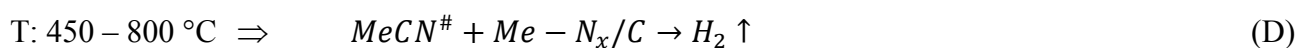
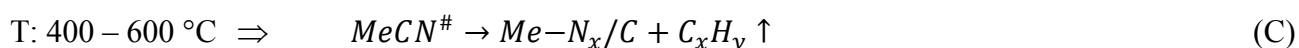
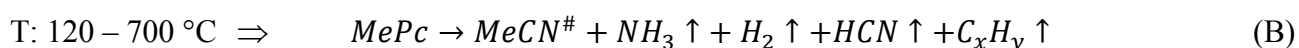
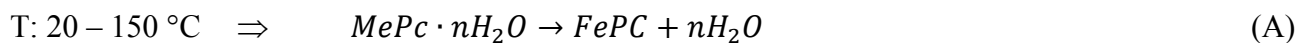
differential weight loss peak. Like in the case of Co-Pc, no presence of  $\text{NH}_3$  and HCN is detected during Fe-Pc precursor pyrolysis.



**Figure 12.** Ionic currents associated with  $\text{N}_2$  (A),  $\text{NH}_3$  (B) and HCN (C) detected at the mass-spectrometer during TGA for the different Me-Pc precursors.

By concluding, the presence of the different transition metals ions coordinated with N atoms in the phthalocyanine macrocycle center influences the morphology, the chemical composition and the ORR catalytic activity of the final catalysts. These properties are related with different trends of the weight loss and with the formation of gaseous products in different amounts and at different temperatures during the pyrolysis. However, until now there is a lack in the literature about detailed in-situ studies of the pyrolyzation of C-, N- and transition metals-containing precursors for the preparation of NPMC for ORR. Therefore, further investigation on other precursors is necessary in order to understand if the behavior during the pyrolysis in terms of weight loss and gas products is a key factor towards the synthesis of more active M-N-C catalysts.

More generally, some considerations can be made about the decomposition during the pyrolysis process of Me-N-C containing macromolecules used as precursor. To produce active ORR non-precious metal catalysts, it is crucial to have a clear understanding of the process forming active ensembles during pyrolyzation (decomposing of the macromolecules). The macrocyclic complex can generally contain atoms of transition metal (Fe, Co, etc.), nitrogen, hydrogen, carbon. Sulfur and oxygen atoms could also be present in some precursors. During the decomposition of a macromolecule complex, for example a Me-Pc, different reactions occur in presence of an inert gas [30,57,64].



In a first step, reaction (A), the water adsorbed by the macromolecule is released by evaporation in the temperature range of 20-150 °C.

After water evaporation, sublimation of the macromolecule complex occurs, in a temperature range depending on the nature of the macromolecule itself. Contemporary to the sublimation, the macromolecule undergoes to a partial decomposition of its structure in the range of 120-700 °C, reaction (B), with the release of gases as ammonia, HCN, hydrogen, volatile short hydrocarbons (C<sub>x</sub>H<sub>y</sub> like compounds).

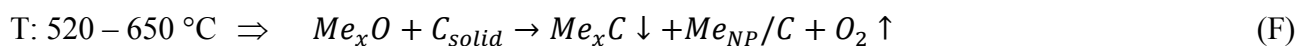
In parallel to reaction (B), various recombinations of carbon and nitrogen (and oxygen if present in the starting macromolecule) give rise to different nitrogen-doped carbon structures, generally indicated as MeCN<sup>#</sup>.

According to the literature [32,64], the formation of Fe-N<sub>x</sub>/C active ensembles require the coordination of Me(II) with pyridinic nitrogen over a  $\pi$ - $\pi$  type carbon sheet in the range of 400 – 600 °C, reaction (C). The decomposition of the nitrogen-doped carbon structures FeCN<sup>#</sup> continues even at higher temperatures, with the release of hydrogen in the range of 450 – 800 °C, reaction (D), of HCN in the range of 550 – 800 °C, reaction (E), of ammonia in the range 550 – 800 °C, reaction (F). These steps are experimentally visible by the differential thermogravimetric plus mass spectroscopy analysis (TGA-MS) of Me-Pc macrocyclic complexes pyrolyzed under inert atmosphere up to 800 °C (Figure 10 and 12).

The structural rearrangement of the catalyst at high temperature as per reactions (D) to (F) involves the partial loss of active ensembles already formed. Since forming active ensembles is the major task in the synthesis of these NPMC, a natural question arises: why do not stop the pyrolyzation in the range of 400 – 600 °C, as per reaction (C) ? The answer is not obvious. The forthcoming processes in the temperature range of 450 – 800 °C, reactions (D) to (F), release gases that actually can perforate the nitrogen-doped carbon matrix of the forming catalyst, by further increasing porosity on the catalyst itself. This is a crucial step to increase accessibility of the reactants for ORR. Thus, the compromise between increasing accessibility through the raise of the porosity, and destroying part of the already formed active ensembles is a key-factor to have good electrochemical activity. In an ideal situation, the formation of active ensembles should be concurrent with porosity formation. A good approach to preserve as much as possible active ensembles should be the use of macromolecules able to form the pores at lower temperatures, to reduce the temperature of the pyrolyzation process.

Considering the morphology of the catalyst, a variety of carbon structures/configurations can be obtained during the pyrolyzation, because of the action of the gases released. The carbon growing mechanism depends upon to the graphitization process, the metal used, and the pyrolyzation temperature as well, as shown in the literature [19]. The use of various metals (Fe, Co, Zn, Cu, etc.) influences the formation of the active ensembles, as well: each metal can act as a “catalyst” itself, to enhance or depress the release of gases during the pyrolysis, leading to a final catalyst structure with higher or lower porosity, and more or less active toward ORR.

Another process that can occur during the pyrolyzation is the metal carbide formation, together with metal encapsulation into carbon sheets, as reported by [31,32,64,65]. This process takes place in the range of 520 – 650 °C, as shown in reaction (F), if oxygen atoms are already available in the starting macromolecule used to synthesize the catalyst:



Metal carbides do not play an active role in the ORR reaction mechanisms, whereas encapsulated metal nanoparticles Me<sub>NP</sub>/C can be considered as active ensembles as well, together with Me-N<sub>4</sub>/C

active ensembles, in acid environment. Specifically, according to the literature, on Fe-N<sub>x</sub>-C catalysts, the Fe(II)-N<sub>4</sub>/C active ensemble is involved in the starting process of oxygen adsorption [66–68]. If on this site the partial 2 electrons reduction to H<sub>2</sub>O<sub>2</sub> occurs, the intermediate H<sub>2</sub>O<sub>2</sub> requires a second active site, to ensure the subsequent reduction to the 4 electrons product (H<sub>2</sub>O), otherwise H<sub>2</sub>O<sub>2</sub> desorbs directly [68]. This site can be the encapsulated Fe<sub>NP</sub>/C, which must be adjacent to a Fe(II)-N<sub>4</sub>/C active ensemble.

Furthermore, the particle size of the Fe<sub>NP</sub> metal in the catalyst can be controlled by tuning the heating scan rate during the pyrolyzation [69]. In fact, the particle size (iron in this case) results smaller if fast heating is applied (usually more than 10 °C min<sup>-1</sup>), as reported in the literature [1,18,46,68,70].

### 3.2. RDE measurements – Acid medium.

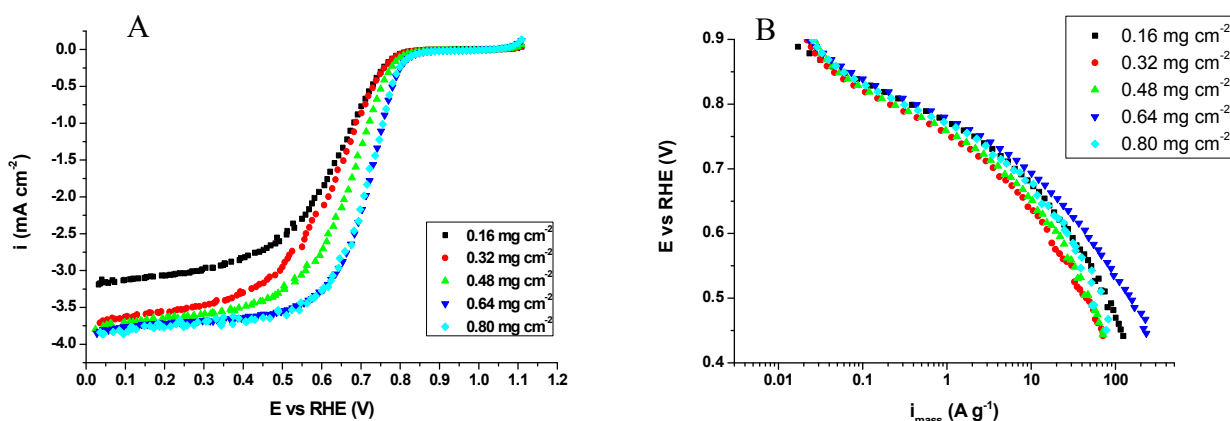
#### 3.2.1. Preliminary electrode optimization: catalyst loading on the electrode and Nafion-to-catalyst ratio in the ink.

A preliminary test on the preparation of the working electrode for RDE tests was performed using the Fe-N-C catalyst. The first part of the optimization was the testing of different catalyst loadings deposited on the glassy carbon surface of the RDE. The chosen amounts were determined from the ink density, that is, the catalyst mass content per volume of ink (mg mL<sup>-1</sup>). The catalyst ink was prepared as described in the experimental section (Paragraph 2.4.1). Therefore, according to this ink formulation, five different electrodes were prepared, by pipetting 1 – 2 – 3 – 4 and 5 µL of ink on the RDE. These ink volumes result in 0.16 – 0.32 – 0.48 – 0.64 and 0.80 mg of ink per cm<sup>2</sup> geometric electrode area. Then, electrode polarization curves were recorded in O<sub>2</sub>-saturated electrolyte with a rotation speed of 900 rpm. As shown in Figure 13 A, better results were obtained with increasing the catalyst loading from 0.16 to 0.64 mg cm<sup>-2</sup>. Then, no more improvement was obtained with a further increase to 0.80 mg cm<sup>-2</sup>.

To eliminate the effects of the mass transport limitations, the kinetic currents were calculated using equation (1) [39,71]:

$$i_k = -\frac{i_L \cdot i}{i_L - i} \quad (1)$$

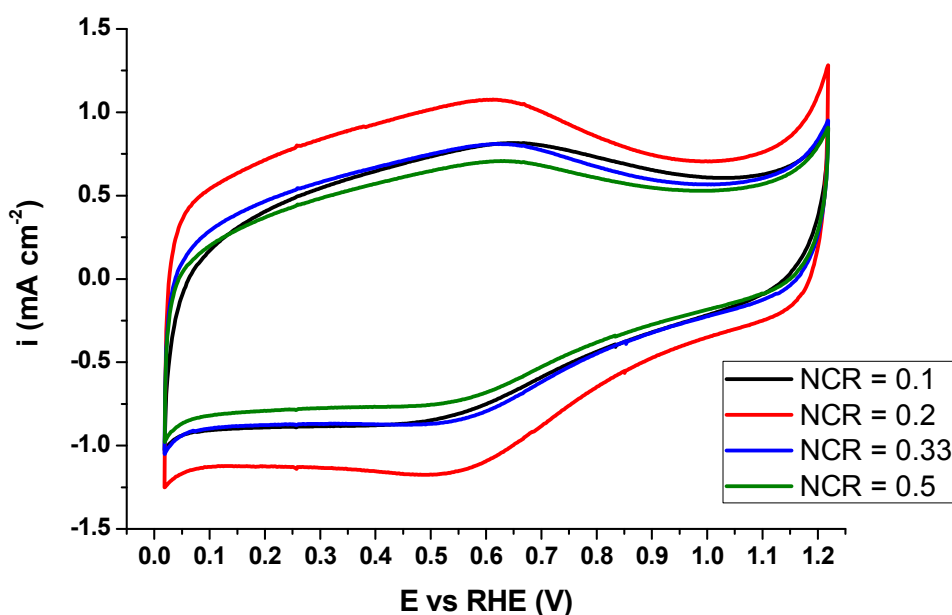
Where:  $i_k$  is mass transport-corrected current density,  $i$  is the measured current density, and  $i_L$  is the limiting current density measured in the plateau region of the polarization curve at high overpotential. A correction for the ohmic drop was also done, based on the resistance values obtained by the impedance measurements as described in the experimental section. The as-calculated  $i_k$  values can be transformed in specific mass current densities (A g<sup>-1</sup>), simply dividing by the catalyst loading on the electrode (mg cm<sup>-2</sup>). The as calculated potential vs logarithm of specific mass current density plot is shown in Figure 13 B.



**Figure 13.** (A) Staircase voltammetries (10 mV potential step, 30 s holding time) of Fe-N-C catalyst in O<sub>2</sub>-saturated 0.5 M H<sub>2</sub>SO<sub>4</sub> at 900 rpm with different catalyst loadings and catalyst ink with NCR = 0.2. (B) Tafel plot obtained from polarization curves in Figure 13 A after mass-transport correction and normalization per mass of catalyst deposited on the electrode.

It can be noticed that the differences found in the ORR measurements with different catalyst loadings (Fig. 13A) was reduced after the mass transport correction and the current density normalization per mass of catalyst, see Figure 13B. These results are also found by Chlistunoff [72], and will be explained more in detail afterwards in Paragraph 3.2.2. However, observing Figure 13 B, the results with 0.64 mg cm<sup>2</sup> catalyst loading are still slightly better than the others. Therefore, if not differently stated, the catalyst loading used hereafter for the RDE experiments will be 0.64 mg cm<sup>2</sup>.

In the second part of the optimization study, the effect of the Nafion-to-Catalyst ratio (NCR) was investigated, maintaining fixed at 0.64 mg cm<sup>2</sup> the catalyst loading on the electrode. Different inks were prepared, as it was described in the experimental section, according to the desired NCR. Four different NCR were used: 0.1 – 0.2 – 0.33 and 0.5. As shown in Figure 14, in spite of the constant catalyst loading, the capacitive currents vary changing the NCR, having a maximum for NCR = 0.2. The influence of the Nafion ionomer on the capacitive current could be linked to the pseudo-capacitance phenomena, to modifications of the contact interface between the carbon surface and the electrolyte [73,74]. However, the Nafion ionomer not only provides proton conductivity but, and maybe more importantly in the RDE system, also acts as a binder for the catalytic particles, causing modifications of the percolating network for electrons and/or protons within the catalyst layer [74]. Therefore, the decrease in the capacitive current density with the increase of NCR can be explained by the formation of a thick Nafion film which encapsulate some of the catalytic particles, causing a loss of electrical contact with the electrolyte. Similar results were also found in the literature [38].

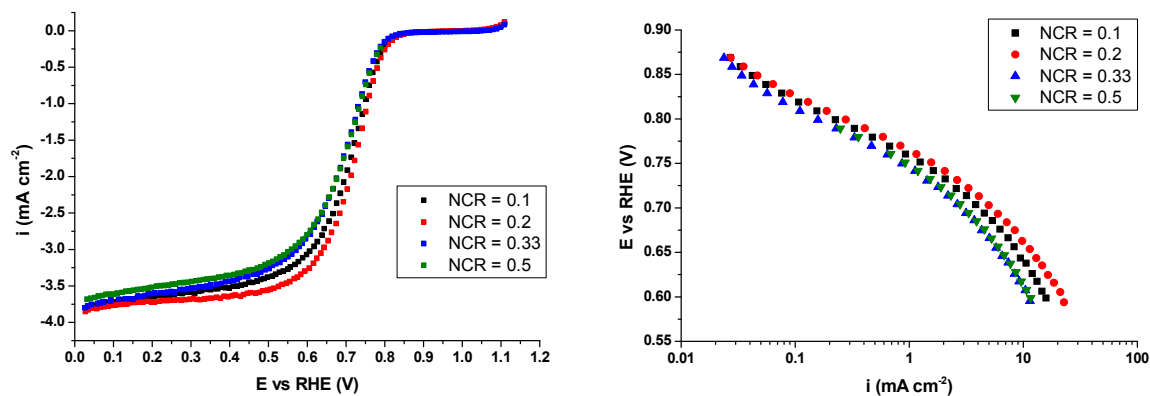


**Figure 14.** CV of Fe-N-C catalyst with ink prepared with different NCR recorded in  $N_2$ -saturated 0.5 M  $H_2SO_4$  solutions at  $10\text{ mVs}^{-1}$  potential scan rate. Catalyst loading  $0.64\text{ mg cm}^{-2}$ .

The ORR tests (Figure 15) show that the different NCR also cause variations in the ORR activity of the Fe-N-C catalyst. The better performance is obtained with  $NCR = 0.2$ . The mass-transport corrected kinetic current density was also calculated using equation (1) as described before. The results are shown in Figure 15 B. The differences between the different NCR are less evident in the kinetically controlled region (low overpotentials), but they become more evident in the mixed kinetic-diffusion controlled region and in the diffusion-limited current density region at higher overpotentials. By increasing the NCR to 0.33 and 0.5, the diffusion-limited current density slightly decreases. This effect can be explained by the formation of a thick Nafion film around catalytic particles, which limits adsorption/desorption phenomena [38]. Also with a lower NCR of 0.1, the performance was worse. This fact could be likely related with the binding-effect of the Nafion in the catalyst layer. In the literature, the effect of NCR on ink formulation has been studied, with the NCR mass ratio varying from 0.1 to 1.5 [36,38,74–76]. The optimum NCR for ORR activity depends on the nature of the different catalysts characteristics (i.e. active sites, porosity), which play a crucial role in the final activity.

Since the highest activity for this Fe-N-C catalyst was obtained with a NCR value of 0.2, this NCR was used for all of the tests in the present work, considering that the other Me-N-C catalysts have similar morphological characteristics.

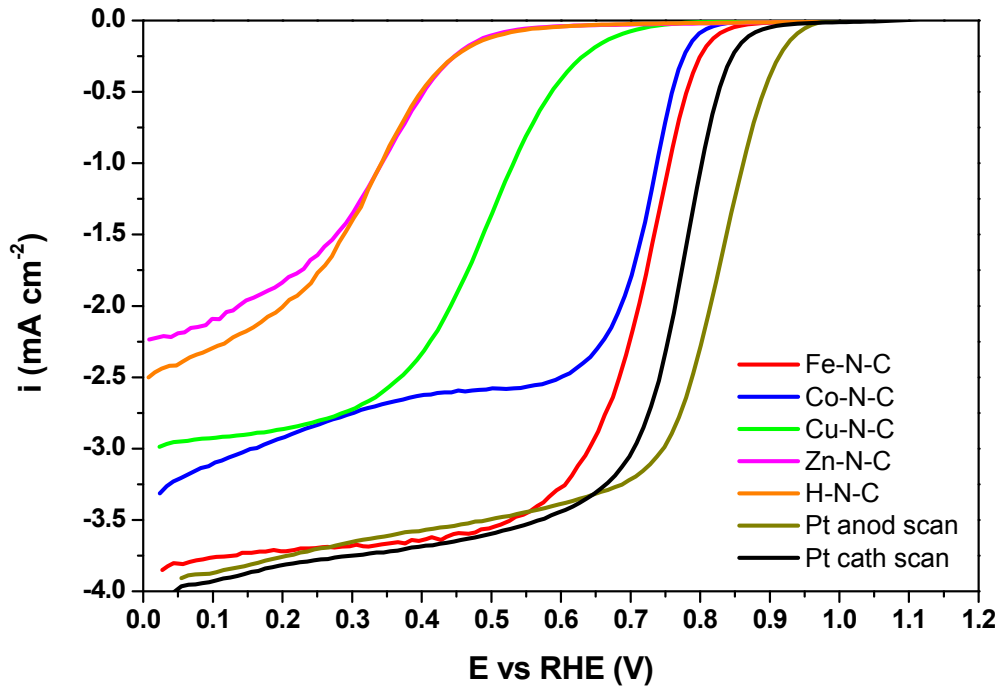




**Figure 15.** (A) Staircase voltammetries (10 mV potential step, 30 s holding time) of Fe-N-C catalyst with ink prepared with different NCR. O<sub>2</sub>-saturated 0.5 M H<sub>2</sub>SO<sub>4</sub> and 900 rpm RDE rotation speed. (B) Tafel plot obtained from polarization curves in Figure 15 A after mass-transport correction.

### 3.2.2. ORR activity.

The ORR activity of the Me-N-C electrocatalysts in acidic conditions was assessed by recording steady-state polarization curves with a potential step of 0.01 V and a holding time at each potential of 30 s in 0.5 M sulfuric acid solution. After 30 s, the background capacitive current had passed, and in this way, a steady-state value of the faradaic current was measured [10]. In order to compare the performance of our catalysts with a standard commercial Pt-based catalyst, the same test was conducted for a Pt 20 wt. % supported on Vulcan. For this catalyst, HClO<sub>4</sub> solution was used instead of H<sub>2</sub>SO<sub>4</sub>, to avoid the detrimental effect of SO<sub>4</sub><sup>2-</sup> and HSO<sub>4</sub><sup>-</sup> ions adsorption on Pt. In fact, HClO<sub>4</sub> is a non-specifically adsorbing electrolyte for Pt [7].



**Figure 16.** Staircase voltammeteries (10 mV potential step, 30 s holding time) of the Me-N-C catalysts (Me = Fe, Co, Cu, Zn, H) recorded in O<sub>2</sub>-saturated 0.5 M H<sub>2</sub>SO<sub>4</sub> at 900 rpm RDE rotation speed. The staircase voltammetry of a commercial Pt catalyst (Pt 20 wt. % on Vulcan, Quintech®) in both cathodic and anodic scan directions is also shown for comparison. For Pt catalyst the electrolyte solution was 1 M HClO<sub>4</sub>.

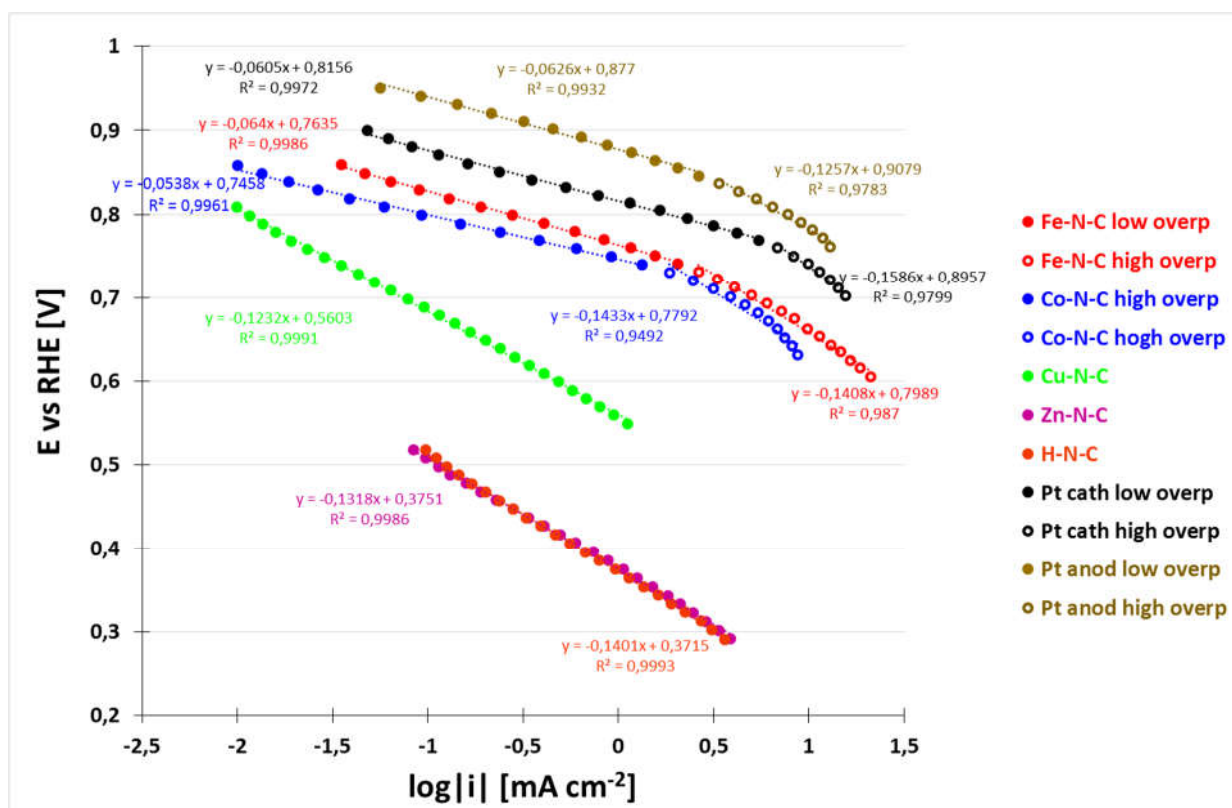
Starting from the data in Figure 16, Tafel slopes, after correction for mass-transport limitation (as described in Paragraph 3.2.1), cathodic transfer coefficients and exchange current densities of the different catalysts were calculated and these results are summarized in Table 4.

According to the IUPAC definition [77,78] the cathodic transfer coefficient  $\alpha_c$  is defined as follows:

$$\alpha_c = -\frac{RT}{F} \frac{d \ln|i_c|}{dE} \quad (2)$$

Where: E is the applied potential, R is the gas constant, T is the absolute temperature, F is the Faraday constant and  $i_c$  is the cathodic current density. Since the symbol  $\ln|i_c|$  implies that the argument of the logarithm is of dimension one, the  $i_c$  value is ideally divided by the corresponding unit, e.g.,  $\ln(|i_c| / \text{mA cm}^{-2})$ . Therefore, in practice,  $\alpha_c$  is defined as the reciprocal of the corresponding Tafel slope,  $-dE/d\ln|i_c|$ , made dimensionless by the multiplying factor  $RT/F$  [cit. IUPAC recommendation].

Other important parameters which define the performance of an ORR catalyst are the onset potential ( $E_{\text{on}}$ ) and the half-wave potential ( $E_{1/2}$ ).  $E_{\text{on}}$  is defined as the potential required to generate a current density of 0.1 mAcm<sup>-2</sup> in a steady-state RDE experiment [46].  $E_{1/2}$  is the potential required to have half the maximum current density in the polarization curve.



**Figure 17.** Plot representing the linear zones of the potential vs logarithm of the mass-transport corrected current densities. Straight trend lines with their respective equations used for the calculations of  $\alpha_c$  and  $i_0$  are also shown.

**Table 4.** ORR kinetic parameters for all of the Me-N-C catalysts and for the Pt commercial catalyst.

| Sample  | $E_{on}$<br>[V vs RHE] | $E_{1/2}$<br>[V vs RHE] | Tafel slope<br>low $\eta$<br>[mV/dec] | $\alpha_c$ low $\eta$ | $i_0$ low $\eta$<br>[mA/cm <sup>2</sup> ] | Tafel slope<br>high $\eta$<br>[mV/dec] | $\alpha_c$ high $\eta$ | $i_0$ high $\eta$<br>[mA/cm <sup>2</sup> ] |
|---------|------------------------|-------------------------|---------------------------------------|-----------------------|---|--|------------------------|--|
| Fe-N-C  | 0.83                   | 0.72                    | 64.0                                  | 0.924                 | $5.14 \cdot 10^{-8}$                      | 140.8                                  | 0.420                  | $8.67 \cdot 10^{-4}$                       |
| Co-N-C  | 0.79                   | 0.71                    | 53.8                                  | 1.099                 | $1.00 \cdot 10^{-9}$                      | 143.3                                  | 0.413                  | $7.15 \cdot 10^{-4}$                       |
| Cu-N-C  | 0.68                   | 0.50                    | -                                     | -                     | -   | 123.2                                  | 0.480                  | $3.66 \cdot 10^{-6}$                       |
| Zn-N-C  | 0.50                   | 0.33                    | -                                     | -                     | -   | 131.8                                  | 0.449                  | $3.26 \cdot 10^{-7}$                       |
| H-N-C   | 0.50                   | 0.32                    | -                                     | -                     | -   | 140.1                                  | 0.422                  | $7.45 \cdot 10^{-7}$                       |
| Pt cath | 0.87                   | 0.76                    | 60.5                                  | 0.977                 | $1.41 \cdot 10^{-7}$                      | 202.2                                  | 0.292                  | $3.63 \cdot 10^{-2}$                       |
| Pt anod | 0.93                   | 0.82                    | 62.6                                  | 0.944                 | $2.30 \cdot 10^{-6}$                      | 125.7                                  | 0.470                  | $3.93 \cdot 10^{-3}$                       |

Analyzing the data shown in Table 4, we can see that the most active catalyst is Fe-N-C. It exhibits 100 mV negative shift in both  $E_{on}$  and  $E_{1/2}$  in comparison with Pt commercial catalyst (anodic scan direction). Moreover, its diffusion limiting current almost corresponds to the limiting current of the Pt catalyst. Co-N-C has a slight lower activity, but it has a lower diffusion limiting current, with a not

well-developed plateau region. Cu-N-C catalyst is considerably less active than the two previous catalysts, having about 250 mV lower  $E_{on}$  and 320 mV lower  $E_{1/2}$  than the Pt commercial catalyst. Zn-N-C and H-N-C have a very poor activity in acid medium, both showing 430 mV lower  $E_{on}$  and about 500 mV lower  $E_{1/2}$  in comparison with Pt catalyst.

It is remarkable that Zn-N-C and H-N-C catalysts exhibit almost the same ORR activity, being their polarization curves practically superimposed (see Figure 16). This suggests that even if the Zn presence leads to considerable modifications in the final catalyst chemical-physical properties (e.g. the total amount of N incorporated), this will have practically no influence on the ORR activity in acidic medium. This finding confirms the important role played by the most effective transition metals (Fe and Co) in the formation of the ORR active sites during the heat treatment. Copper also has certain effectiveness in active sites formation, but considerably lower than cobalt and iron.

In the Tafel plots (see Figure 17), for both Fe-N-C and Co-N-C two different Tafel slope zones have been identified. One at low overpotentials (approximately between 0.85 and 0.75 V vs RHE) and a second one at higher overpotentials (approximately between 0.75 and 0.60 V vs RHE). At low overpotentials the Tafel slope is lower, being approximately of 60 mV dec<sup>-1</sup>. At high overpotentials the slope becomes higher, and the linear trend is less evident, suggesting a changing in the reaction mechanism occurring in this zone [72]. However, a linearization was made also in this zone, in spite of the lower coefficient of determination ( $R^2$ ). The Tafel slopes are around 140 mV dec<sup>-1</sup>. An analogous two slope behavior can be found in the literature for C-N based NPMC in acid conditions [72].

This behavior of the Fe-N-C and Co-N-C catalysts can be compared with the Pt-based catalysts. In fact, it is widely reported in the literature that the measured Tafel slope for single crystal Pt electrodes [79], polycrystalline Pt [80] and carbon supported Pt catalysts [81] suffers a shift from about 60 mV dec<sup>-1</sup> at low overpotential to 120 mV dec<sup>-1</sup> at higher overpotential [7,82]. This effect is explained for Pt in terms of surface active site partial blocking by oxygen-containing reaction intermediates varying with the potential. It influences the reaction rate at small overpotentials even when the removal of the intermediates involves fast quasi-equilibrium steps, and if the initial electron transfer is the rate determining step (RDS) of the reaction over the whole potential range considered. In particular, the change of the Tafel slope from 60 to 120 mV dec<sup>-1</sup> at high currents at Pt surface (both Pt smooth surface and small Pt particles) was explained by the change in Temkin to Langmuir adsorption conditions (i.e., by the decrease in the surface coverage) but not to the change in rate-determining step [83–87].

The coupling of such equilibrium processes to the rate-limiting step leads to a coverage-dependent, and hence potential-dependent apparent Tafel slope [82].

When estimating ORR activity for Pt-based catalysts, usually anodic scan direction is analyzed as, in this case, activity is not affected by oxide layer which is slowly removed when potential is decreasing. Analyzing both anodic and cathodic sweep directions, a certain hysteresis is observed. This is commonly ascribed to slow removal of surface oxides which hinders ORR during negative going sweep [88].

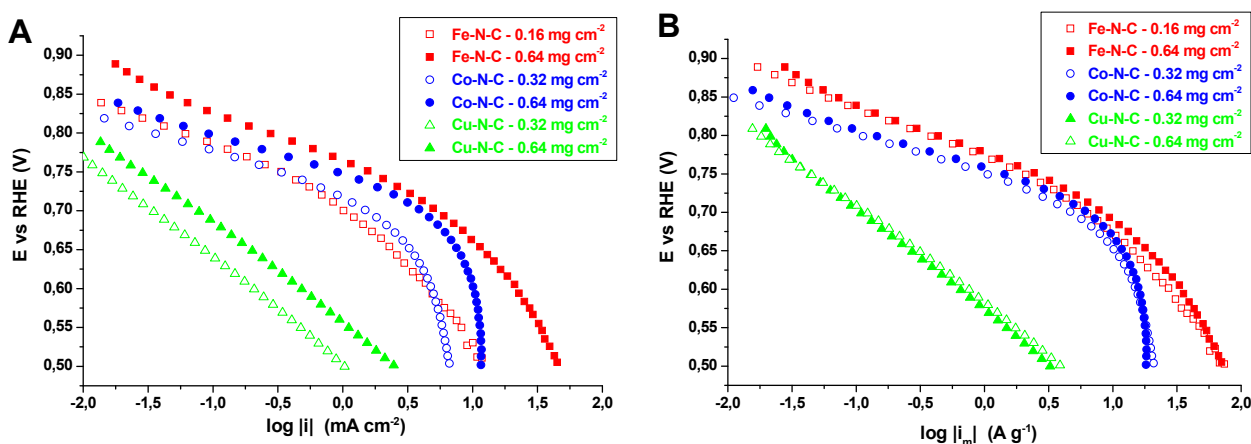
Considering the exchange current densities in the low overpotential region, Fe-N-C has an almost double  $i_0$  value than Co-N-C. These values are two orders of magnitude lower than for Pt catalyst (anodic scan direction). Comparable results can be found in the literature [89]. In the high overpotential region the  $i_0$  values for Fe-N-C and Co-N-C are closer, and still almost one order of magnitude lower than for Pt catalyst.

Otherwise, Cu-N-C catalyst does not exhibit this double-slope behavior. For this catalyst, a single linear region with a slope value of about  $123 \text{ mV dec}^{-1}$  is observed along all the potential range from 0.8 to 0.55 V vs RHE. Comparing the exchange current density of Cu-N-C with the values in the high overpotential region for Fe- and Co-N-C, the former is almost two orders of magnitude lower than the latter.

Zn-N-C and H-N-C catalysts also show a single-slope behavior in the potential range 0.5 – 0.3 V vs RHE, with a Tafel slope of 132 and  $140 \text{ mV dec}^{-1}$ , respectively. In terms of exchange current densities, their values are one order of magnitude lower than for Cu-N-C.

Since the ORR activity of Zn-N-C and H-N-C catalysts is very poor and therefore they are not interesting for being used as cathode materials in PEMFC, hereafter we will not consider these two catalysts for the investigation of the other kinetic aspects of the ORR in acid medium.

To investigate more in detail the effect of the catalyst loading on the ORR kinetic, we recorded the polarization curve in RDE at 900 rpm rotation speed with two different ink quantities deposited on the electrode for each one of Fe-, Co- and Cu-N-C catalyst. These polarization curves are shown in Figure 16 for all of the catalysts (at  $0.64 \text{ mg cm}^{-2}$  loading) and in Figure 13 A for Fe-N-C with  $0.16 \text{ mg cm}^{-2}$  loading. For Co- and Cu-N-C with  $0.32 \text{ mg cm}^{-2}$  loading the polarization curves are not reported here. The respective Tafel plots are shown in Figure 18.



**Figure 18.** ORR Tafel plots for Fe-, Co- and Cu-N-C catalysts obtained after mass transport correction. (A) Current densities referred to the electrode geometric surface area. (B) Current densities referred to the mass of catalyst deposited on the electrode.

For all of the catalysts, when the current densities are referred to the geometric area of the electrode (Figure 18 A), the apparent ORR kinetics appears to be enhanced with a higher catalyst loading. However, when the current densities are normalized per unit mass of catalyst deposited on the electrode surface (Figure 18 B), the plots with low catalyst loading undergo a vertical shifts, making them almost overlap the plots with high catalyst loading in the whole range of overvoltage. Chlistunoff also obtained similar results [72].

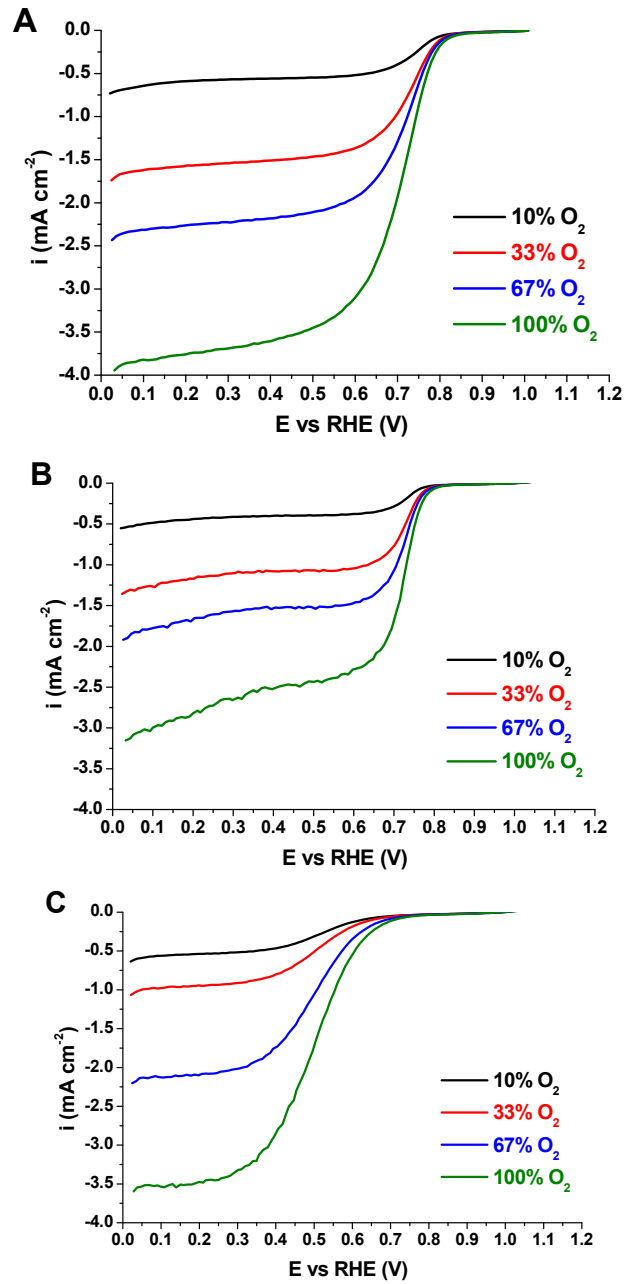
Therefore, for all the catalysts examined, we obtained a good agreement between mass specific kinetic current densities ( $\text{A g}^{-1}$ ) after the mass-transport correction for both high and low catalyst loadings. In particular, for Fe- and Co-N-C catalysts, this indicates that the curvature of the  $E$  vs  $\log|i|$  plots (with a consequent changing in the Tafel slope), does not originate from incomplete catalyst utilization in the catalytic layer [90] or uncompensated resistance [11], but it is most likely the consequence of changes in the intrinsic ORR kinetics, which is potential-dependent [72].

### 3.2.3. Reaction order for $\text{O}_2$

For the determination of the reaction order for  $\text{O}_2$ , staircase voltammetry experiments were performed in 0.5 M sulfuric acid solution saturated with  $\text{O}_2 - \text{N}_2$  mixtures in four different proportions, in order to have  $\text{O}_2$  at different partial pressures:

- 1) 10 %  $\text{O}_2 - 90$  %  $\text{N}_2$  ;
- 2) 33 %  $\text{O}_2 - 67$  %  $\text{N}_2$  ;
- 3) 67 %  $\text{O}_2 - 33$  %  $\text{N}_2$  ;
- 4) 100 %  $\text{O}_2 - 0$  %  $\text{N}_2$  .

The results for Fe-, Co-, and Cu-N-C catalysts are shown in Figure 19 A – B – C, respectively. A similar trend of results was obtained by Paulus et al. for a Pt catalyst supported on Vulcan [7] .



**Figure 19.** Staircase voltammetries (10 mV potential step, 10 s holding time) of Fe-N-C (A), Co-N-C (B), Cu-N-C (C) catalysts recorded in 0.5 M H<sub>2</sub>SO<sub>4</sub> at 900 rpm RDE rotation speed at different O<sub>2</sub> partial pressures at 25°C.

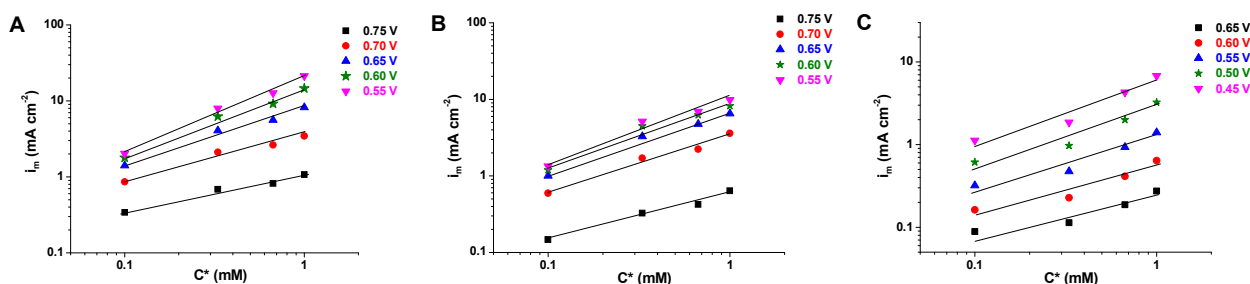
The O<sub>2</sub> solubility in moderately concentrated sulfuric acid aqueous solutions follows the Henry's law [91,92], and therefore is decreasing linearly with the O<sub>2</sub> partial pressure.

The reaction order for oxygen can be defined as follows:

$$R_{O_2} = \left( \frac{\partial \log |i_m|}{\partial \log C} \right)_{E,T,pH} \quad (3)$$

Where: R<sub>O2</sub> is the reaction order for oxygen, i<sub>m</sub> is the mass-transport corrected current density, C is the O<sub>2</sub> concentration in the electrolyte solution, E is the electrode potential, T is the temperature.

Therefore, the reaction order can be determined from the slope of a double-logarithmic plot of  $i_m$  vs.  $C^*$ , where  $C^*$  is defined as the  $O_2$  concentration normalized to the  $O_2$  saturation concentration in the electrolyte for pure  $O_2$  at 1 bar,  $C^0$  (being  $C^0 = 1.05$  mM in 0.5 M  $H_2SO_4$  aqueous solution). As shown in the plots of Figure 20 and summarized in Table 5, for all the three catalysts the reaction order for  $O_2$  seems not to be constant in the mixed kinetic-diffusion control potential range.



**Figure 20.** Double-logarithmic plots of mass transport corrected current density in function of  $O_2$  concentration in the electrolyte for Fe-N-C (A), Co-N-C (B) and Cu-N-C (C) catalysts.

In particular, for potentials more close to the onset potential, the reaction order is about 0.5. Then, as the overpotential increases, the reaction order increases as well. Considering the most active catalysts, that is Fe-N-C, the reaction order reaches 1 at 0.55 V vs RHE, where the purely diffusion limited current “plateau” starts. For Co-N-C and Cu-N-C catalysts, the reaction order increase is less marked, getting a value close to 0.8 at 0.55 and 0.45 V vs RHE, respectively.

Some studies about reaction order for oxygen have been done for Pt-based catalysts in RDE [7,93]. The reaction order values are all close to unity in all the studied potential ranges.

**Table 5.** Reaction orders for oxygen calculated at different potentials in the mixed kinetic-diffusion control zone for Fe-N-C, Co-N-C and Cu-N-C catalysts.

| E vs RHE [V] | Catalyst |        |        |
|--------------|----------|--------|--------|
|              | Fe-N-C   | Co-N-C | Cu-N-C |
| 0.75         | 0.48     | 0.61   | -      |
| 0.70         | 0.59     | 0.75   | -      |
| 0.65         | 0.75     | 0.80   | 0.47   |
| 0.60         | 0.89     | 0.83   | 0.58   |
| 0.55         | 0.99     | 0.85   | 0.63   |
| 0.50         | -        | -      | 0.71   |
| 0.45         | -        | -      | 0.78   |

Unfortunately in the literature there is a lack of studies reporting the reaction order for  $O_2$  for this type of carbon-nitrogen-transition metal based NPMC in acidic conditions. Chlistunoff reported a



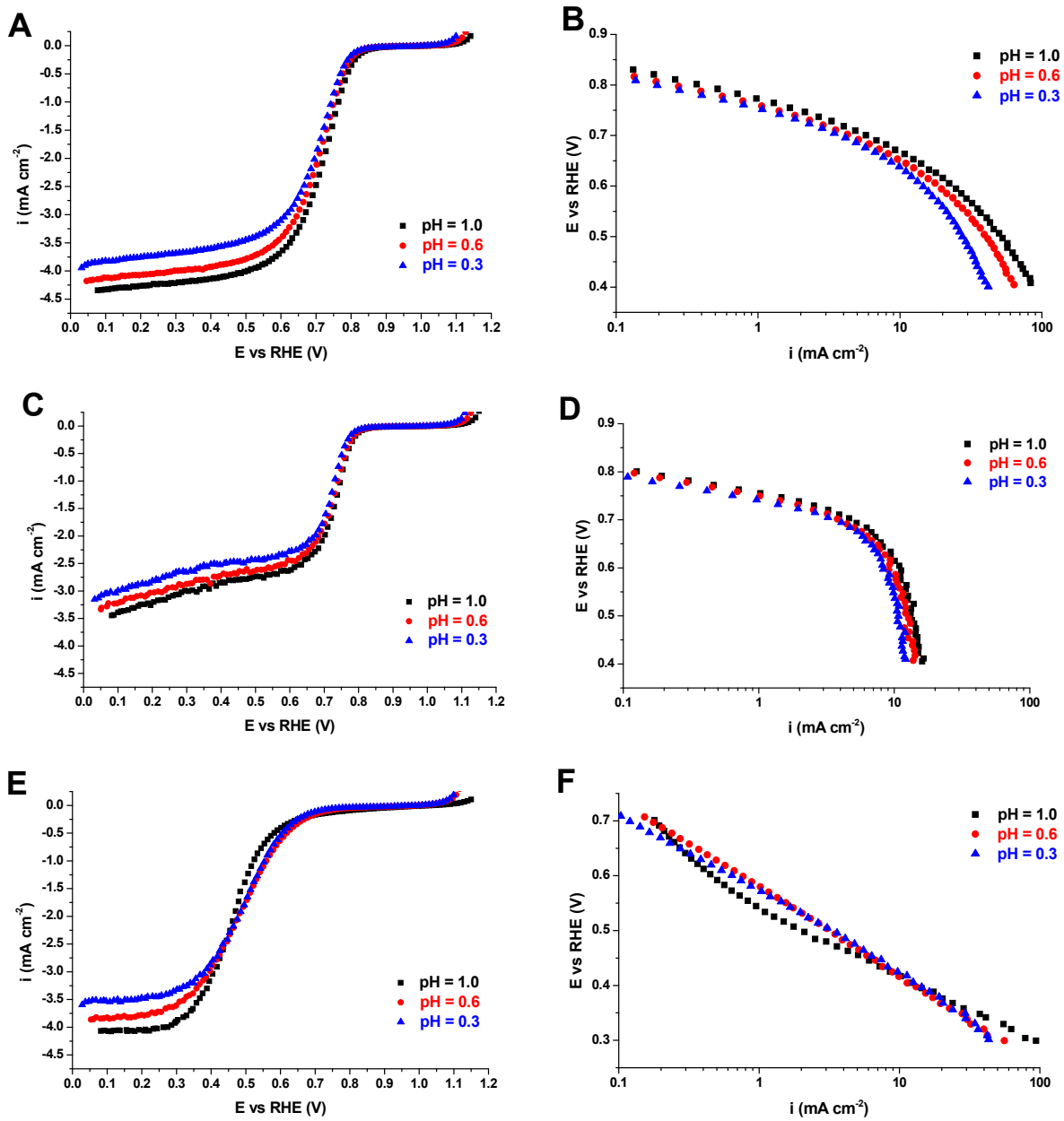
reaction order of 1 for a pyrolyzed Fe-Polyaniline catalyst which activity was tested in oxygen and air-saturated electrolyte [72].

#### 3.2.4. Reaction order for $H^+$

$H^+$  ion, in addition to  $O_2$ , is the other reactant of the ORR in acid conditions. For the determination of the reaction order for  $H^+$ , ORR activity experiments have to be performed at different  $H^+$  concentrations, that is, at different electrolyte solution pH. This is in contrast to the fact that the determination of the order of an electrochemical reaction for one of its reactants has to be performed at a constant electrode potential. In fact, if we use the RHE as potential reference scale, we have to consider that this reference varies with the electrolyte solution pH of about 60 mV per pH unit. However, the reaction order for  $H^+$  ( $R_{H^+}$ ) can be expressed by the following approximate equation [72]:

$$R_{H^+} \cong \left( \frac{\partial \log i}{\partial \log C_{H^+}} \right)_{E_{RHE}} + \left( \frac{\alpha_c F}{2.3RT} \right) \left( \frac{dE_{RHE}}{d \log C_{H^+}} \right) \quad (4)$$

where:  $i$  is the current density,  $C_{H^+}$  is the molar concentration of  $H^+$  ion,  $E_{RHE}$  is the potential measured vs RHE,  $\alpha_c$  is the cathodic transfer coefficient,  $R$  is the gas constant and  $T$  is the absolute temperature. Therefore, we recorded the polarization curves in RDE with three different  $H_2SO_4$  concentrations: 0.1, 0.25 and 0.5 M. Since the second dissociation of  $H_2SO_4$  in water at these concentrations is almost negligible, the corresponding pH values are 1, 0.6 and 0.3, respectively. The results are shown in Figure 21.



**Figure 21.** Staircase voltammetries (10 mV potential step, 10 s holding time) recorded at 900 rpm RDE rotation speed in O<sub>2</sub>-saturated sulfuric acid solutions at different pH, and the respective Tafel plots after mass-transport correction for catalysts Fe-N-C (A-B), Co-N-C (C-D) and Cu-N-C (E-F).

For Fe-N-C and Co-N-C catalysts, in the low overpotential range (between 0.8 and 0.7 V) the Tafel plot is almost linear (see Figure 21 B – C) and the slope is equal to  $\sim 60$  mV for decade of current. In addition, the plots at different pH values are almost completely overlap in this potential range. Therefore, at a certain potential in this range, we have:

$$\left( \frac{\partial \log i}{\partial \log C_{H^+}} \right)_{E_{RHE}} \cong 0$$

$$\left(\frac{\alpha_c F}{2.3RT}\right) = \frac{1}{\text{Tafel slope}} \cong \frac{1}{60 \text{ mV dec}^{-1}}$$

$$\left(\frac{dE_{\text{RHE}}}{d\log C_{\text{H}^+}}\right) \cong 60 \text{ mV dec}^{-1}$$

Therefore, the reaction order for  $\text{H}^+$  is almost equal to 1. In the same way, considering approximately no variations of the plots with pH, the reaction order for  $\text{H}^+$  suffers a decrease as the cathodic overpotential increase, due to the changes in the Tafel slope (see Table 4). As for the reaction order for  $\text{O}_2$ , also in this case the literature studies are scarce. Chlistunoff [72] performed a similar study for a pyrolyzed Fe-Polyaniline catalyst, which exhibited a similar behavior. If we look at the Tafel plots at different pH (Figure 21 B – D – F), we notice that they are not completely overlapping each other, especially at higher overpotentials. This is most likely due to the decrease of  $\text{O}_2$  solubility with decreasing pH in sulfuric acid solutions [91,94]. A correction for  $\text{O}_2$  solubility in solutions with different  $\text{H}_2\text{SO}_4$  concentrations should be necessary to eliminate this discrepancy. For Cu-N-C catalyst, the same considerations can be made. It exhibits a constant Tafel slope of about  $120 \text{ mV dec}^{-1}$  in the potential range between 0.60 and 0.40 V vs RHE. Thus, in this potential range, the reaction order for  $\text{H}^+$  is 0.5.

### 3.2.5. Activation Energy calculation for ORR

The activation energies ( $E_a$ ) are evaluated at different fixed potentials using the Arrhenius equation in a temperature range between  $10^\circ\text{C}$  and  $60^\circ\text{C}$ . In performing the RDE experiments at different temperatures two different effects must be taken into account. The first one is the enhancing effect of the temperature increase on ORR activity, and second one is the decreasing in  $\text{O}_2$  concentration with increased temperature. In particular, the  $\text{O}_2$  concentration in the electrolyte solution is reported to vary from 1.38 mM at  $20^\circ\text{C}$  to 0.61 mM at  $60^\circ\text{C}$  [95]. Thus, to take into account this effect, the current densities measured at different temperatures have been corrected according to the following equation [74]:

$$i_m^* = i_m \cdot \exp\left(\frac{1\text{mM}}{C_{\text{O}_2}}\right)^{0.79} \quad (5)$$

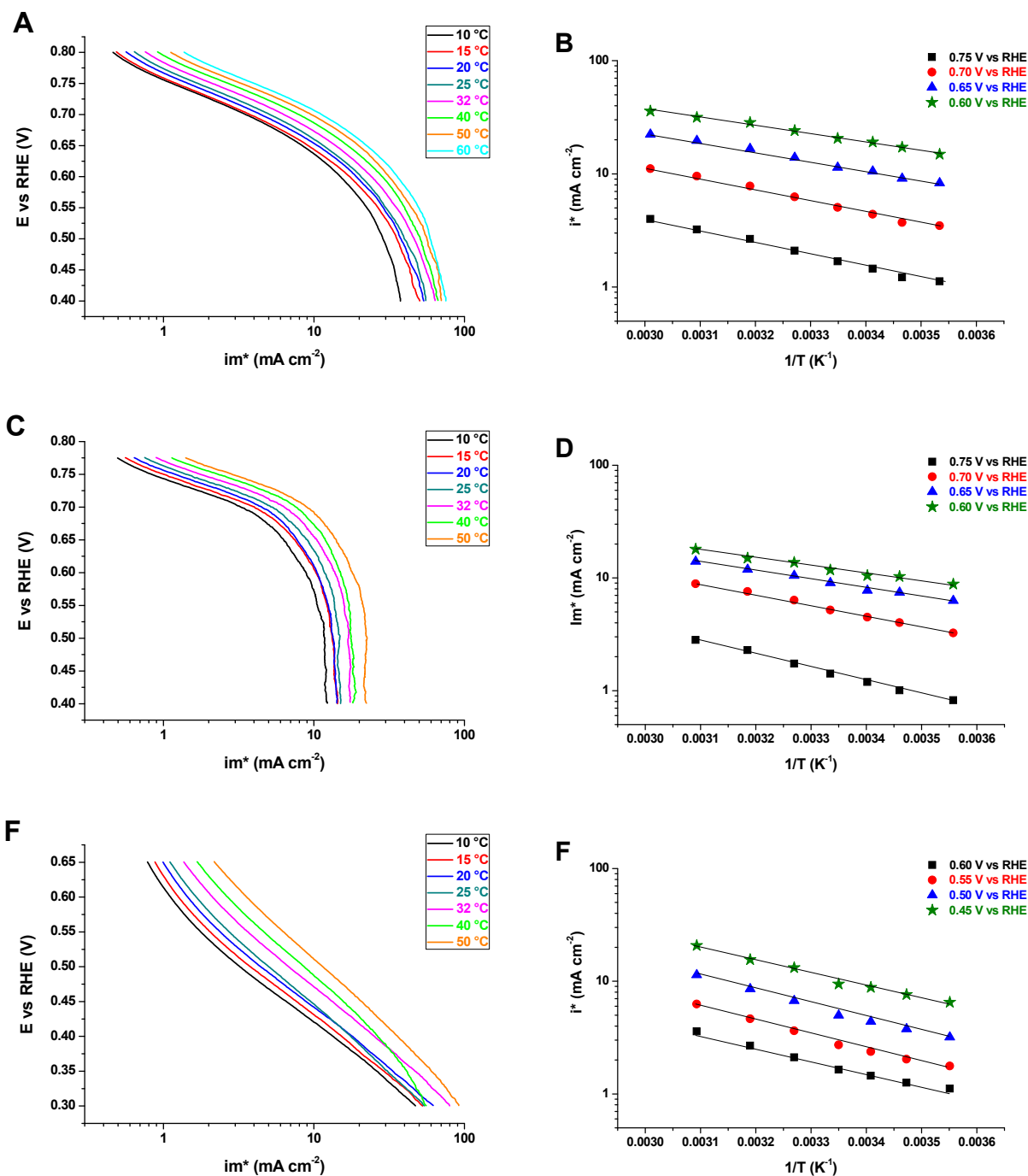
Where:  $i_m$  is the original mass-transport corrected current density,  $C_{\text{O}_2}$  is the actual oxygen concentration in the liquid electrolyte at the temperature at which the measurement was done, and  $i_m^*$  is the corresponding current density for an oxygen concentration of 1 mM. Then, Arrhenius plots (logarithm of current density vs. the inverse of the absolute temperature) can be made. The activation energy can be calculated from the linearization of the Arrhenius law:

$$i_m^*(T) = i_m^*(T_\infty) \cdot \exp\left(\frac{-E_a}{2.3RT}\right) \quad (6)$$

where T is the actual temperature at which the measure was done (in K), and  $i_m^*(T_\infty)$  is a constant value. The slope of the Arrhenius plots is equal to  $-E_a / (2.3 R)$ .

The Tafel plots at different temperatures with the aforementioned corrections are shown in Figure 22 together with their respective Arrhenius plots, for Fe-, Co- and Cu-N-C catalysts.

The Arrhenius plots were calculated at different potentials in the kinetic and mixed kinetic-diffusion control potential regions for the three different catalysts. The corresponding calculated activation energies are reported in Table 6. These values are comparable with the values found in the literature for ORR on Pt-based catalysts [7,74, 96–98]. Unfortunately, also for activation energy as well as for the reaction order for  $O_2$  and  $H^+$ , there is a lack in the literature for this type of Me-N-C electrocatalysts. Jaouen et al. calculated the activation energy at 0.9 V for a series of pyrolyzed Fe-N-C catalysts synthesized from carbon black, iron acetate and 1,10 phenanthroline. They obtained values around 9 kJ mol<sup>-1</sup> [74].



**Figure 22.** Effect of the temperature on RDE measurements of ORR activity. Tafel plot after correction for mass-transport and oxygen solubility at different temperatures, and the respective Arrhenius plots at different overpotentials for Fe-N-C (A-B), Co-N-C (C-D) and Cu-N-C (E-F). Oxygen saturated 0.5 M H<sub>2</sub>SO<sub>4</sub> electrolyte, 900 rpm RDE rotation speed.

For Fe-N-C and Co-N-C catalysts there is a decrease of activation energy with the increase of overpotential. In particular, for low overpotential region where the Tafel slope is of about 60 mV dec<sup>-1</sup>, the activation energy has values close to 20 kJ mol<sup>-1</sup>. Then, moving to the higher overpotential zone, where the Tafel slope has almost a double value, the activation energy values tend to decrease,

approaching values of 16 – 14 kJ mol<sup>-1</sup> at 0.65 V and even lower values of 13 – 12 kJ mol<sup>-1</sup> at 0.6 V. A similar trend of decreasing activation energy with increasing overpotential (simultaneously with the changing in Tafel slope) was found for Pt/C, Pt-Ni/C and Pt-Co/C catalysts in acidic conditions [98].

Unlike the two previous catalysts, for Cu-N-C the activation energy was calculated in the potential range between 0.60 and 0.45 V vs RHE, having this catalyst a 150 mV lower onset potential. The activation energy of Cu-N-C, similarly to the Tafel slope (see Figure 17), does not change with the overpotential. In fact, it oscillates between 21.3 and 23.6 kJ mol<sup>-1</sup> at all of the potential considered.

Paulus et al. also determined the activation energy for a Pt catalyst supported on carbon in the region of low Tafel slope using the Arrhenius plot method in both H<sub>2</sub>SO<sub>4</sub> and HClO<sub>4</sub> electrolytes. They obtained values of 26 – 28 kJ mol<sup>-1</sup> [7]. Similar values were obtained for low index Pt single crystal surfaces and polycrystalline Pt surfaces [79,80,96,98].

As stated in the work of Neyerlin et al. [99], this activation energy decrease with increasing overpotential is due to contributions from the Tafel slope, which also depends on temperature. As a consequence, the increase in current with temperature due to the activation energy measured at lower overpotentials is smaller than when measured at higher overpotentials. In the same work, Neyerlin et al. also reported a series of activation energy values for Pt/C catalysts measured in fuel cell. These values are in the range between 42 and 96 kJ mol<sup>-1</sup> [99]. The reason of these significantly higher activation energies in comparison with the values found in three-electrode cell configuration with liquid electrolyte, are related with the higher complexity of the complete fuel cell system, where phenomena like water flooding effects in the cathode catalyst layer may occur [7].

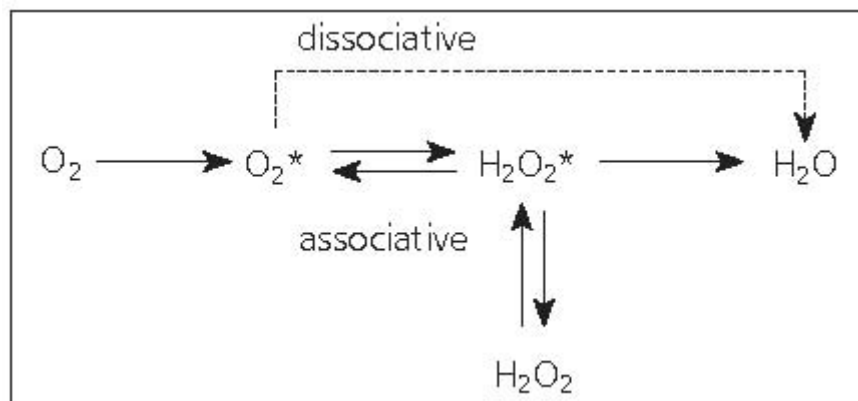
**Table 6.** Calculated activation energies as a function of the electrode potential for Fe-N-C, Co-N-C and Cu-N-C catalysts.

| E vs RHE [V] | Activation Energy [kJ mol <sup>-1</sup> ] |        |        |
|--------------|---|--------|--------|
|              | Fe-N-C                                    | Co-N-C | Cu-N-C |
| 0.75         | 20.91                                     | 22.82  | -      |
| 0.70         | 19.57                                     | 18.50  | -      |
| 0.65         | 16.34                                     | 14.56  | -      |
| 0.60         | 13.93                                     | 12.67  | 21.71  |
| 0.55         | -   | -      | 23.61  |
| 0.50         | -   | -      | 23.60  |
| 0.45         | -   | -      | 21.33  |

However, it must be considered that the calculation of activation energies at the same overpotential as it was done in this work, is only an estimation of the activation energy. Thus, E<sub>a</sub> is an “apparent” activation energy value [96]. In the case of Pt in fact, the i<sub>m</sub>\* in equation (5) is strongly dependent on

the amount of oxides on the Pt surface which, in turn, is temperature-dependent, even though the oxide coverage is considered as a preexponential term in equation (5) [96].

If one wants to make an analogy between the Pt-based catalysts and our Fe-N-C and Co-N-C catalyst, we can speculate that the reaction mechanism could be the same:



where the first step is the adsorption of  $O_2$  on the catalyst active site:  $O_2 \rightarrow O_2^*$

followed by the first electron transfer, which is the rate determining step:  $O_2^* \rightarrow O_2^{*-}$ .

Surface coverage effects have been proposed as the reason of changes in ORR kinetic behavior on Pt surfaces. These have been noted to accompany changes in the surface coverage of adsorbed oxygen-containing groups, such as OH species, which can originate from both  $H_2O$  and  $O_2$  [82]. These can control the availability of the adsorption sites for of molecular  $O_2$  [96]. A clear overlap between the onset potential of ORR and the removal of these oxygen containing species from the Pt surface is observed [82] looking at Pt CV in de-aerated solutions and in ORR experiments in RDE. In this region the Tafel slope change also occurs.

We can try to make a parallelism between the Pt-based catalysts and the NPMC. For example in Fe-N-C catalysts, the presence of a redox peak in the CV (i.e. related to the  $Fe^{2+}/Fe^{3+}$  couple) [72,100] could be compared to the Pt-oxides reduction peak in the CV of Pt surface. The onset of ORR on Pt surface is associated with the appearance of the Pt-oxides reduction peak in the CV recorded in de-aerated solution, as discussed in the literature [82]. Therefore, the onset of the ORR on these NPMC could be associated to the potential at which the redox peak starts to appear [72,100,101].

However, in our catalysts, these peaks characteristic of oxygen-containing species removal are not as evident as for Pt in de-aerated solutions (see Figure 14). In particular, their presence could be “masked” by the very high capacitive currents (e.g. in comparison with Vulcan, which is the usual carbon support for Pt-based catalysts) [100] which are due to the very high specific surface area and surface functionalization (pseudo-capacitive effects) [73] of these catalysts. However, the presence of a broad peak in the potential range between 0.8 and 0.4 V vs RHE is detected, and it could be

related to phenomena analogous to the ones occurring in Pt-based catalysts, as described before. We can state this is a way to justify the analogies between the behavior of these non-precious metal based catalysts and the Pt-based catalysts.

### 3.2.6. Koutecky-Levich analysis, RRDE test and hydrogen peroxide oxidation-reduction.

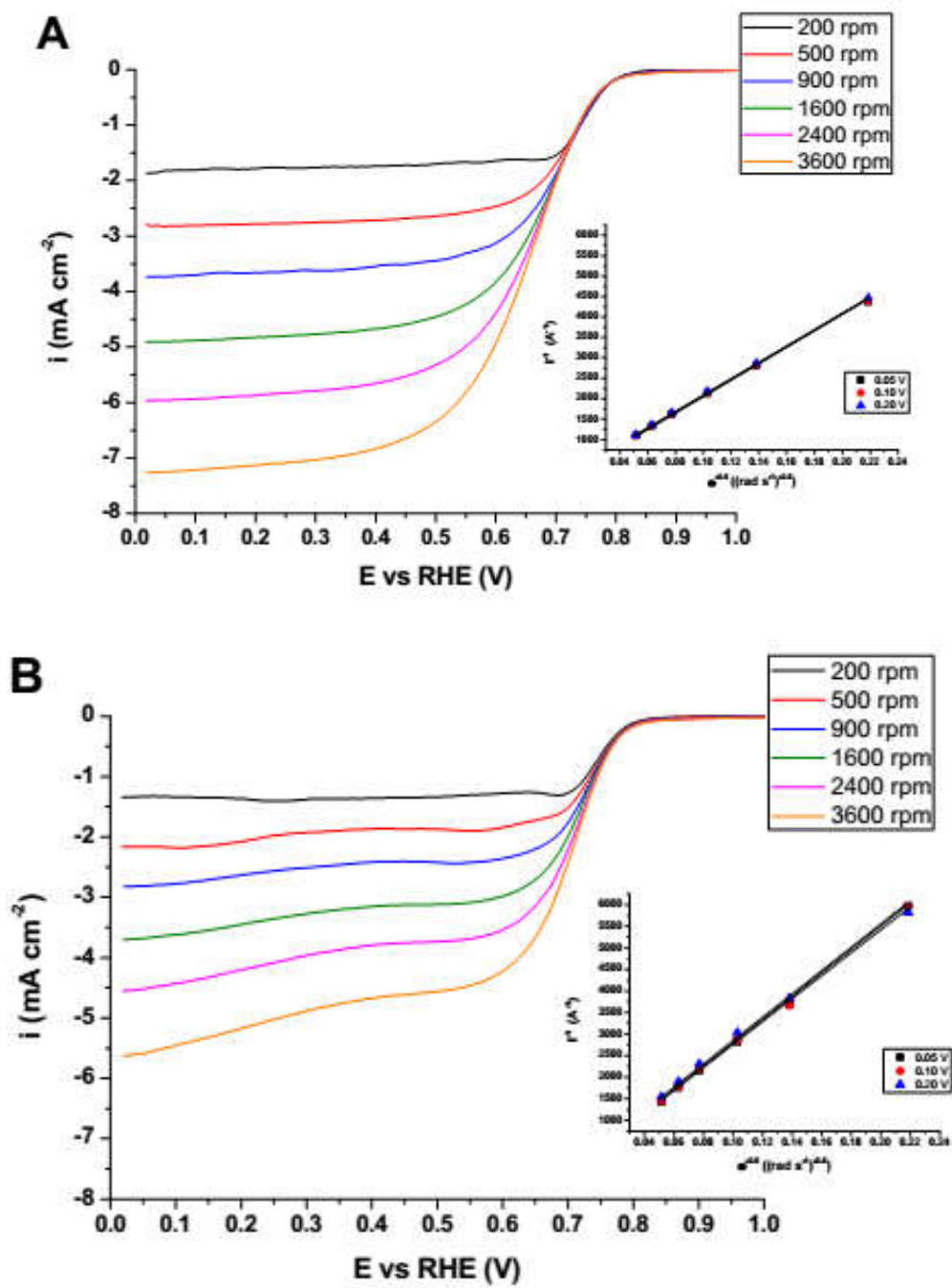
In order to have some indication about the ORR reaction pathway, i.e., if the oxygen is reduced directly to water via a direct  $4\text{ e}^-$  mechanism or via a two-step  $2\text{ e}^- + 2\text{ e}^-$  mechanism with the formation of a peroxide intermediate, or only partially to hydrogen peroxide via  $2\text{ e}^-$  mechanism, we performed a series of electrochemical tests.

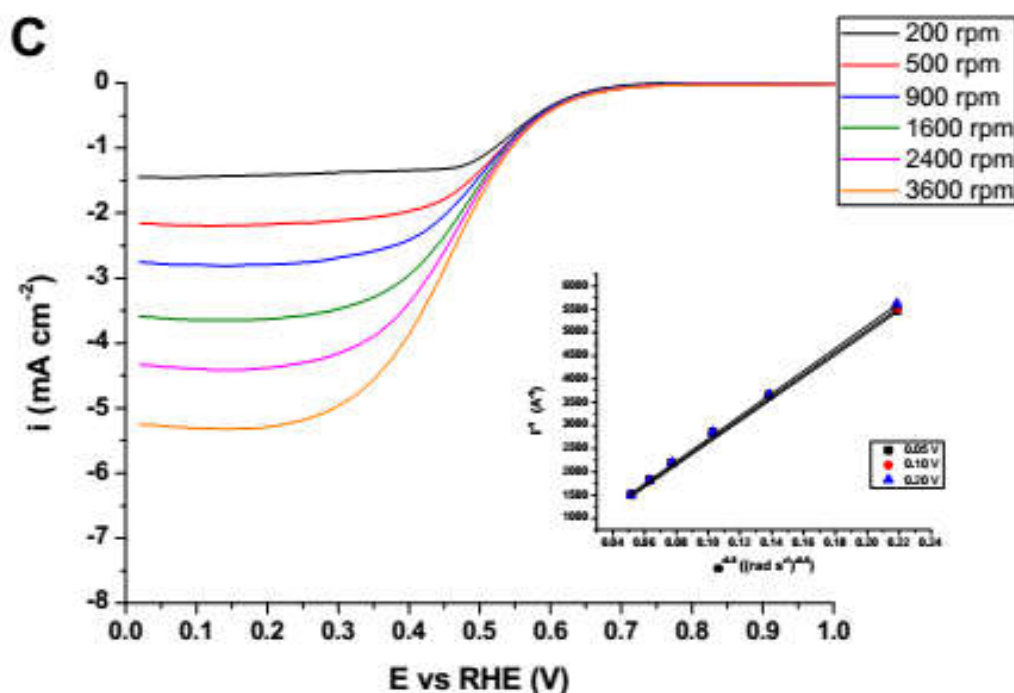
- *Koutecky-Levich analysis.*

The first test was the Koutecky-Levich analysis. LSV were recorded in  $\text{O}_2$  saturated electrolyte at different RDE rotation speed for Fe-, Co-, and Cu-N-C catalysts. The results are shown in Figure 23. Looking at the LSV at different rotation speeds, for all the three catalysts the limiting current densities are lower than those predicted by the Levich equation [102]. The variation of the current density with the rotation speed is a direct means to investigate if the reaction occurring is under mass-transport control of reactants diffusing from the bulk solution or under kinetic control [102]. As expected, for all of the catalysts, there is a noticeable increase of the diffusion-limited current density with the RDE speed. However, no one of the catalysts exhibits a perfect “plateau” in the diffusion-limited region at high overpotentials. This effect is more evident for Co-N-C catalyst. However, a straight line trend was obtained for the Koutecky-Levich plots of all of the catalysts, with an almost parallel slope at different potentials [39]. Therefore we calculated the number of electrons involved in the ORR for these catalysts. The values are summarized in Table 7.

First of all, it must be taken into account that the Koutecky-Levich theory was developed for a smooth electrode surface [100]. However, when the catalyst loading is on the order of hundred micrograms per  $\text{cm}^2$  geometric area of the electrode (as typically used in the literature for NPMC and also in our tests), we cannot affirm that the catalyst film deposited on the electrode is so thin to be under the hypothesis of validity of the K-L theory [72,103]. Therefore, some correction should be made to consider the roughness and the thickness shortcomings of the catalyst film on the RDE [104].







**Figure 23.** LSV recorded at different rotation speeds and  $5 \text{ mV s}^{-1}$  scan rate in  $\text{O}_2$ -saturated  $0.5 \text{ M H}_2\text{SO}_4$  after background capacitive current subtraction for Fe-N-C (A), Co-N-C (B) and Cu-N-C (C) catalysts. The insets show the corresponding Koutecky–Levich plots at different potentials in the diffusion-limited region.

Looking at the results in Table 7, Fe-N-C seems to be the catalyst with the better performance in terms of selectivity towards a complete  $4 \text{ e}^-$  oxygen reduction, exhibiting a hydrogen peroxide generation of about 15 molar %. Co-N-C catalyst, despite having an onset potential very close to the Fe-N-C one, has a considerably lower selectivity, generating about 60% of  $\text{H}_2\text{O}_2$ . Slight lower peroxide amounts (about 50%) are obtained for Cu-N-C, but this catalyst has a remarkably lower onset potential in comparison to the previous two.

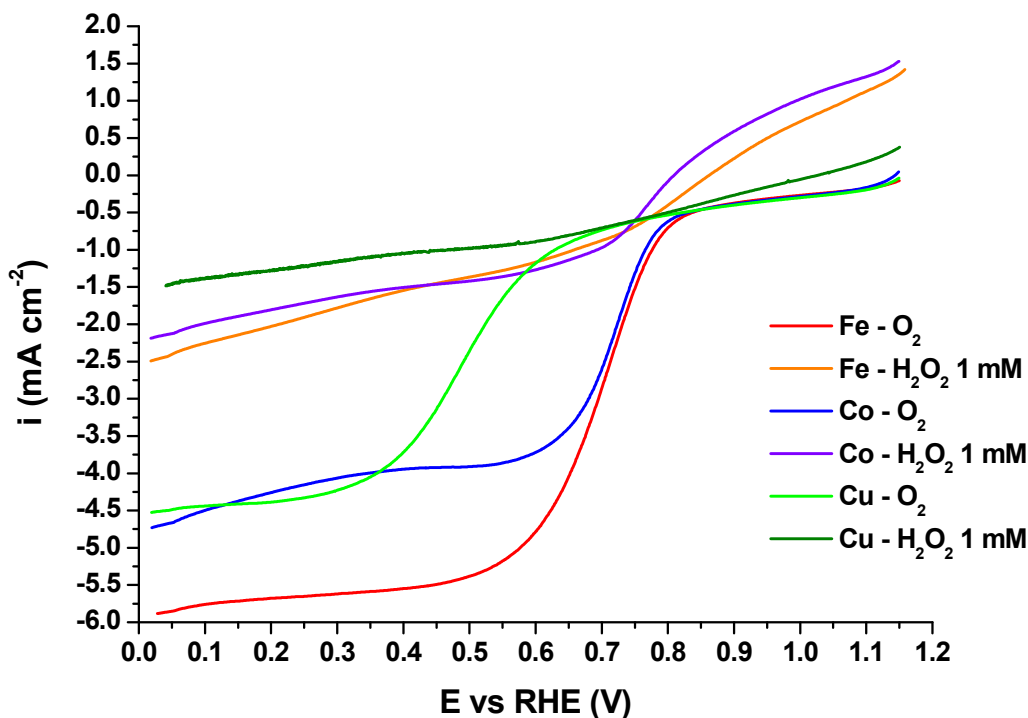
**Table 7.** Total number of electrons involved in the ORR and corresponding hydrogen peroxide generation (molar % of the reduced oxygen) for Fe-, Co- and Cu-N-C catalysts resulting from the Koutecky–Levich analysis in Figure 23.

| Sample | 0.05 V vs RHE      |                          | 0.1 V vs RHE       |                          | 0.2 V vs RHE       |                          |
|--------|--------------------|--------------------------|--------------------|--------------------------|--------------------|--------------------------|
|        | N° of $\text{e}^-$ | % $\text{H}_2\text{O}_2$ | N° of $\text{e}^-$ | % $\text{H}_2\text{O}_2$ | N° of $\text{e}^-$ | % $\text{H}_2\text{O}_2$ |
| Fe-N-C | 3.73               | 13.4                     | 3.70               | 14.8                     | 3.64               | 17.9                     |
| Co-N-C | 2.71               | 64.6                     | 2.75               | 62.5                     | 2.87               | 56.4                     |
| Cu-N-C | 3.09               | 45.4                     | 3.05               | 47.3                     | 2.97               | 51.3                     |

- *H<sub>2</sub>O<sub>2</sub> oxidation-reduction.*

To investigate more in detail which is the predominant reaction pathway for ORR in these catalysts, their activity toward the electroreduction of H<sub>2</sub>O<sub>2</sub> in absence of O<sub>2</sub> was assessed. LSV were performed in deaerated electrolyte solution after the addition of hydrogen peroxide in a concentration of 1 mM, which is very close to the concentration of O<sub>2</sub> in saturated 0.5 M H<sub>2</sub>SO<sub>4</sub> solution (about 1.05 mM [94]). Moreover, this concentration is about the maximum H<sub>2</sub>O<sub>2</sub> concentration that can be found during ORR experiments in RDE [105].

As shown in Figure 24, in spite of almost the same concentration of hydrogen peroxide than that of oxygen, the currents due to oxygen reduction are almost 3 times higher for Fe-N-C and Cu-N-C and almost 2 times higher for Co-N-C in comparison to those resulting from hydrogen peroxide reduction. The increase in H<sub>2</sub>O<sub>2</sub> reduction current with cathodic potential is almost linear, and the maximum reduction current is smaller than the diffusion limited currents expected for 1 mM H<sub>2</sub>O<sub>2</sub> from the Levich equation. Similar results have been reported in the literature [72,102,106] for heat-treated Fe-N-C ORR catalysts. This suggests that H<sub>2</sub>O<sub>2</sub> reduction is under kinetic control within all the scanned potential range. In comparison with the ORR, the kinetics of H<sub>2</sub>O<sub>2</sub> reduction is sluggish, since it is never fast enough to completely reduce all the available flux of H<sub>2</sub>O<sub>2</sub>, even at high overpotentials. It has also to be considered that part of the reduction current could originate also from H<sub>2</sub>O<sub>2</sub> chemical disproportionation [102,107]. However, this possibility is most likely excluded, as explained by Jaouen and Dodelet [102,105], letting us to deduce that the observed current is most likely due to H<sub>2</sub>O<sub>2</sub> reduction.



**Figure 24.** LSV performed at  $5 \text{ mV s}^{-1}$  and 1600 rpm in  $\text{N}_2$ -saturated  $0.5 \text{ M H}_2\text{SO}_4$  with the addition of  $1 \text{ mM H}_2\text{O}_2$  for Fe-N-C, Co-N-C and Cu-N-C catalysts. LSV in  $\text{O}_2$ -saturated  $0.5 \text{ M H}_2\text{SO}_4$  in the same conditions are also shown for comparison.

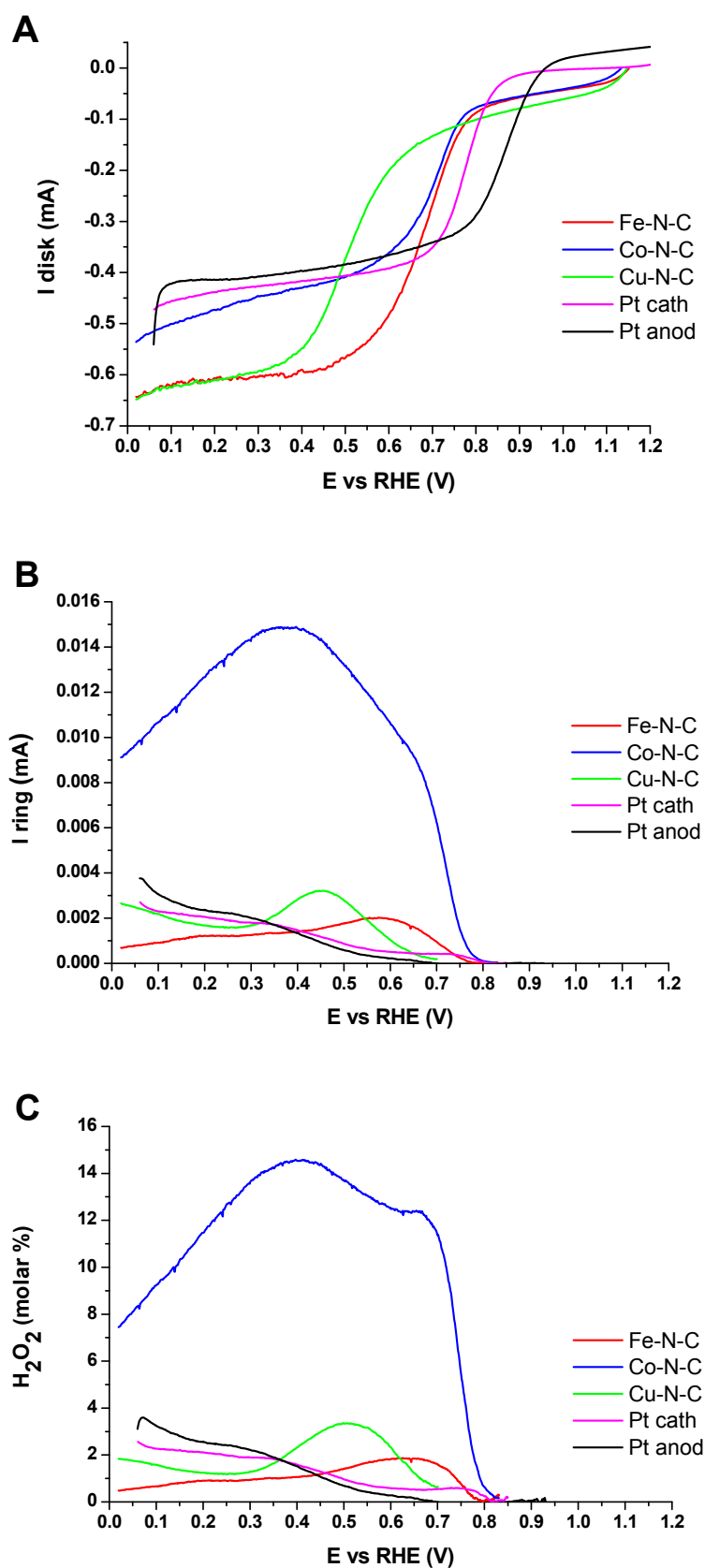
- *RRDE test.*

As a further means to better investigate the ORR path, RRDE test was performed. The results are shown in Figure 25. The following equation was used to calculate the percentage of hydrogen peroxide produced during ORR:

$$\% \text{H}_2\text{O}_2 = 100 \cdot \frac{2I_r/N}{I_d + (I_r/N)} \quad (6)$$

Where  $I_d$  is the current at the disk,  $I_r$  is the current at the ring and  $N$  is the ring collection efficiency (44%) [108].

Considering the Me-N-C catalysts, it is evident that Co-N-C is the catalysts which exhibits the higher hydrogen peroxide production, which gets a maximum molar % value of about 15 % at  $0.4 \text{ V}$  vs RHE. Cu-N-C, in spite of having a lower electroactivity in terms of onset and half-wave potentials, leads to the formation of a considerably lower amount of  $\text{H}_2\text{O}_2$ , with a maximum of 3.5 molar % at  $0.5 \text{ V}$  vs RHE. Fe-N-C is the catalysts that shows the lower formation of  $\text{H}_2\text{O}_2$  (between 0.5 and 2 molar %), confirming that it is the best catalysts not only in terms of activity but also in terms of selectivity. Values of ring currents in the same order of magnitude, and consequently of peroxide % production were measured by other groups for similar Fe-N-C pyrolyzed catalysts in acidic conditions [72,100,102].



**Figure 25.** RRDE test measurements performed in 0.5 M H<sub>2</sub>SO<sub>4</sub> for Fe-N-C, Co-N-C and Cu-N-C and in 0.1 M HClO<sub>4</sub> for Pt/C: (A) disk currents, (B) ring currents and (C) hydrogen peroxide molar proportion. Ring potential 1.2 V vs RHE, electrode rotation speed 900 rpm, disk potential scan rate 5 mV s<sup>-1</sup>.

A commercial Pt-based catalyst (Pt 20 wt. % on Vulcan) was also analyzed for comparison. For this catalyst, at lower overpotentials the peroxide generation is considerably lower than for our Me-N-C catalysts, especially in the anodic potential scan direction. In the low overpotential region (between 0.85 and 0.60 V vs RHE) the peroxide generation is higher in the cathodic scan direction, due to the presence of oxides on the Pt surface at these potentials, which hinder in some way the complete 4 e<sup>-</sup> oxygen reduction, leading to a higher peroxide production. This behavior is typical of Pt in acidic conditions [7,11,100] However, a significant increase in the ring current for Pt/C catalyst was detected when the disk potential approaches the H-underpotential deposition region [100].

The hydrogen peroxide generation results obtained with RRDE technique are considerably lower than the values calculated by the Koutecky-Levich analysis. In order to justify this discrepancy, we have to consider that the RRDE technique is a direct means of detection of H<sub>2</sub>O<sub>2</sub>, while the K-L method is an indirect one, and it is based on a number of theoretical hypotheses under which it is valid, as the smooth electrode surface. Thus, this results discrepancy is a further confirmation that most likely the conditions of validity of the K-L model are not verified in this test, as previously hypothesized.

By concluding, from the results of these three tests conducted in order to determine the ORR path, we can deduce that these Me-N-C catalysts are able to electroreduce O<sub>2</sub> to H<sub>2</sub>O and H<sub>2</sub>O<sub>2</sub>, but much less able to electroreduce H<sub>2</sub>O<sub>2</sub> to H<sub>2</sub>O. Therefore, since H<sub>2</sub>O<sub>2</sub> reduction kinetics is considerably slower than the total (4 e<sup>-</sup>) and partial (2 e<sup>-</sup>) O<sub>2</sub> reduction kinetics, we can conclude that the sequential 2e<sup>-</sup> + 2e<sup>-</sup> reduction mechanism with intermediate formation of H<sub>2</sub>O<sub>2</sub> is not the main catalytic ORR path on these catalysts. If it is occurring, it will be only marginal. If the sequential mechanism was the predominant one, the H<sub>2</sub>O<sub>2</sub> reduction kinetics should have been higher, or at least comparable to the ORR, but this is not the case, as demonstrated by the results in Figure 24. Therefore, the direct 4 e<sup>-</sup> reduction mechanism is predominant. The partial 2 e<sup>-</sup> reduction of O<sub>2</sub> to H<sub>2</sub>O<sub>2</sub> is also occurring, as demonstrated by RRDE test, and it is not negligible, especially for Co-N-C catalyst.

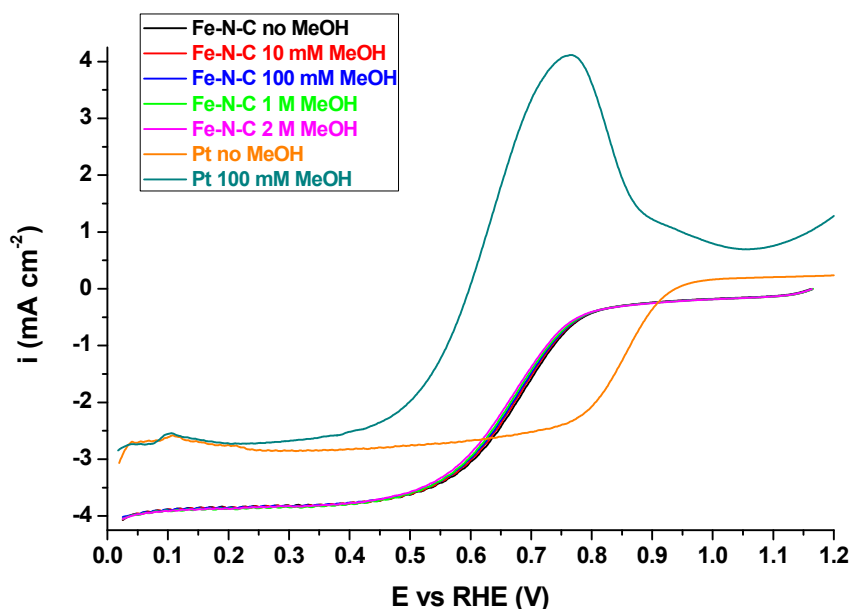
These results underline how, in order to improve the catalyst performance toward a complete reduction of oxygen to H<sub>2</sub>O, minimizing the hydrogen peroxide generation, the presence of at least one of the two following active sites is essential:

- effective H<sub>2</sub>O<sub>2</sub> reduction active sites, in order to enhance at maximum the reduction of the peroxide generated by the partial 2 e<sup>-</sup> mechanism, via the sequential 2e<sup>-</sup> + 2e<sup>-</sup> mechanism.
- dimeric active sites that simultaneously bind both oxygen atoms in order to stabilize the H<sub>2</sub>O<sub>2</sub> intermediate in acidic media, to favor the direct 4 e<sup>-</sup> pathway [100].

### 3.2.7. Methanol tolerance test.

For DMFC application, one of the most important characteristic of an ORR electrocatalyst is to be tolerant to the presence of methanol. As a matter of fact, the permeation of fuel from the anode to the cathode through the Nafion proton-conducting membranes (crossover effect), is one of the major impediments to the wide-scale commercialization of DMFC devices [109]. If a Pt-based catalyst is used at the cathode, and a relevant methanol crossover effect is present, an important decrease in the DMFC performance is observed. This is due to the high activity of Pt towards methanol oxidation reaction (MOR), which can easily occur at the high potentials usually present at the cathode of the fuel cell. This causes a considerable decrease of the cell open circuit potential and poisoning of the cathodic catalyst, due the poisoning effect of Pt catalyst by the MOR intermediates, especially CO [110–114]. As a consequence, the overall power density that the DMFC can generate remarkably decreases during operation [12,115]. The use of methanol-tolerant cathode catalysts is a good strategy to minimize this effect, and therefore increase the performance and the durability of DMFC.

As already demonstrated in the literature [68, 116–119], this type of Me-N-C NPMC do not exhibit any activity towards MOR. Therefore, we tested the ORR activity of our most active catalyst, that is Fe-N-C, in presence of various methanol concentrations. The methanol concentrations were chosen in the range from 10 mM to 2 M, that is the concentration of the methanol solution we used to feed the anode in the DMFC tests (see Paragraph 3.4). The results are shown in Figure 26. The behavior of a commercial Pt-based catalyst is also shown for comparison.



**Figure. 26.** LSV recorded in RDE at 900 rpm rotation speed and 5 mV s<sup>-1</sup> scan rate for Fe-N-C catalyst and for a commercial Pt/C catalyst (20 wt. % Pt on Vulcan). The electrolyte was O<sub>2</sub>-saturated 0.5 M H<sub>2</sub>SO<sub>4</sub> with different methanol (MeOH) concentrations, as indicated in the legend.

For the Fe-N-C catalyst, there is almost no difference between the LSV curve without presence of methanol and the curve in presence of 10 mM to 2 M methanol concentrations. This confirms the high methanol tolerance of this catalyst, and that the ORR is the predominant process at the Fe-N-C electrodes over the whole potential range. Only a very small negative shift of about 10 mV is observed in the mixed kinetic-diffusion control zone. This could be due to a slight interaction between methanol and ORR active sites [116].

Otherwise, for the Pt catalyst, the effect of the presence of methanol on the LSV curve is much more evident and severe decrease in the performance was observed. The MOR, rather than the ORR, was the preferred reaction on the Pt/C electrode.

Consequently, in spite of the almost 200 mV higher half-wave potential of the Pt catalyst in comparison with Fe-N-C in absence of methanol, with a methanol concentration of 0.1 M (that is 20 times lower than the solution fed at the anode), a big peak of methanol oxidation appears. This causes a remarkable 400 mV decrease in the  $E_{1/2}$  of the ORR, making the performance of Fe-N-C much better than the one of Pt catalyst in these conditions.

### 3.3. RDE measurements – Alkaline medium.

#### 3.3.1. Tafel analysis.

The ORR activity of the Me-N-C electrocatalysts in alkaline conditions was assessed by recording steady-state polarization curves with a potential step of 0.01 V and a holding time at each potential of 30 s in 0.1 M KOH solution, as described in Paragraph 3.2.2 for acid conditions.

In order to compare the performance of our samples with a standard commercial Pt-based catalyst, the same test was conducted for a Pt 20 wt. % supported on Vulcan. The SV polarization curves are shown in Figure 27 A. From these data, after mass-transport limitation correction, Tafel plots were made (see Figure 27 B).

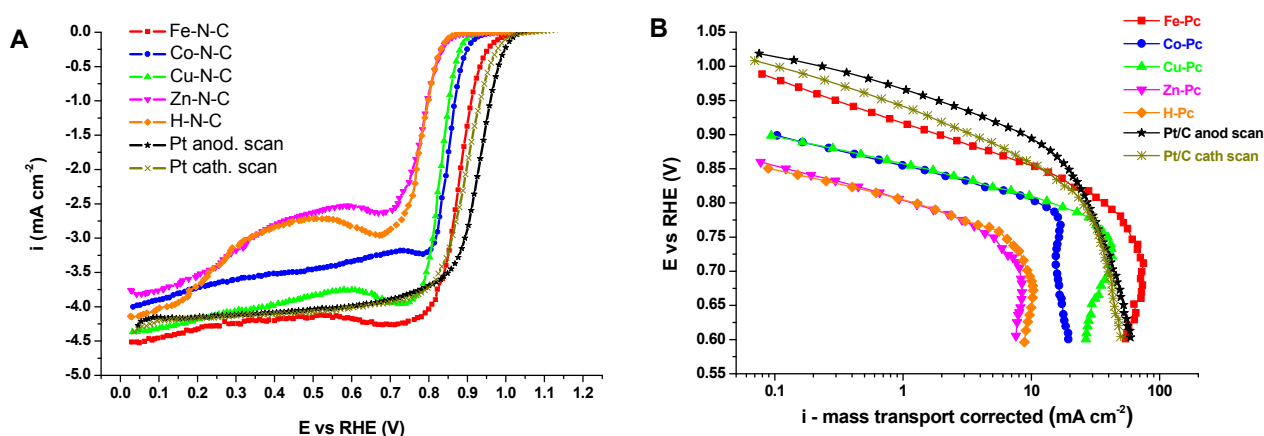
For the Me-N-C catalysts, only the zone with linear trend of potential vs mass-transport corrected current density in the low overpotential region can be clearly identified. In fact, for potentials lower than 0.85 V vs RHE for Fe-N-C, 0.80 V for Co- and Cu-N-C, and 0.75 V for Zn- and H-N-C, the change in Tafel slope with potential is too fast to allow its calculation in the high-overpotential zone (e.g. as done previously for Fe- and Co-N-C in acid conditions). For all of the Me-N-C catalysts, at high overpotentials the Tafel plots are strongly affected by the mass transport effects, as suggested by the change in concavity of the Tafel plot profiles at high overpotentials [106]. This is not the case for Pt/C catalyst, where the double Tafel slope region can be appreciated more clearly, and allow the calculation in both the low and high overpotential regions.



Starting from the data in Figure 27 B, Tafel slopes were calculated, allowing the determination of the cathodic transfer coefficients and exchange current densities of the different catalysts. The results are shown in Table 8 for all of the Me-N-C catalysts and for Pt/C catalyst in both cathodic and anodic scan directions, together with the respective onset potentials ( $E_{on}$ ) and the half-wave potentials ( $E_{1/2}$ ).

The most active catalyst Me-N-C is Fe-N-C. It only exhibits 30 - 40 mV negative shift in  $E_{on}$  and  $E_{1/2}$  respectively, in comparison with Pt commercial catalyst (anodic scan direction). Its diffusion limiting current value almost corresponds to the limiting current of the Pt catalyst, even if it is slightly higher. Co-N-C and Cu-N-C have about 100 mV lower activity in terms of  $E_{on}$  and  $E_{1/2}$  in comparison with the Pt commercial catalyst. Co-N-C has a lower diffusion limiting current, while Cu-N-C has a limiting current almost equal to the Pt/C catalyst. However, unlike the Pt/C, the “plateau” region at high overpotentials is not so well-developed.

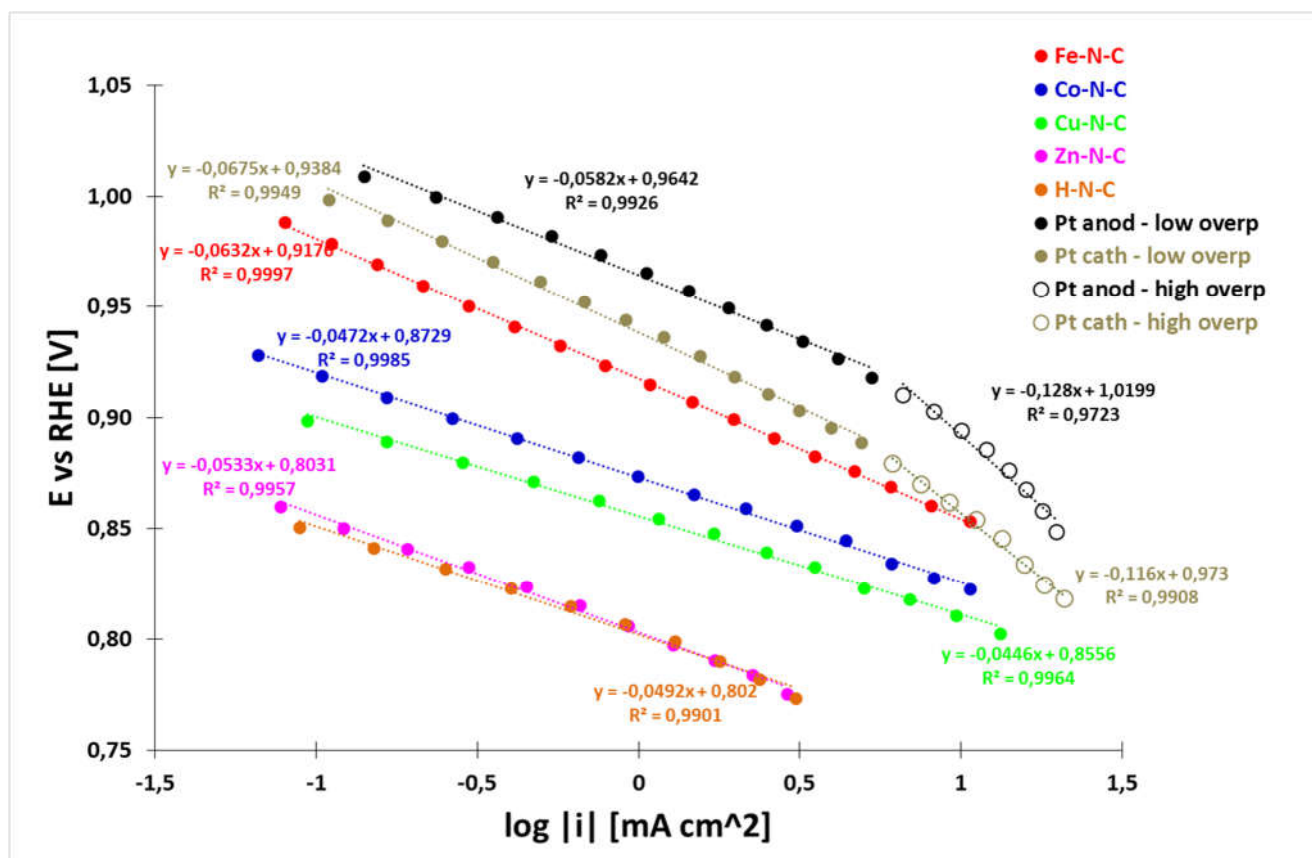
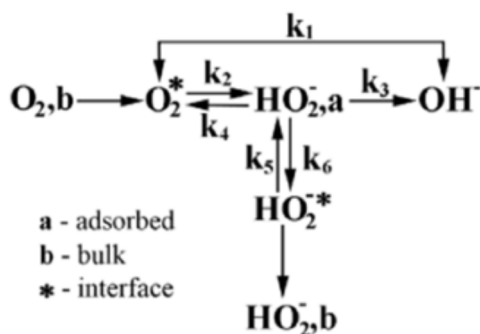
Zn-N-C and H-N-C are much less active than the previous catalysts, showing almost 150 mV negative shift in  $E_{on}$ . Like in the case of test in acidic conditions (see Paragraph 3.2.2), these two catalysts show practically the same activity, being their polarization curves almost superimposed in the whole potential range, especially in the kinetic-controlled zone. This fact confirms that even if the two catalysts have different chemical-physical properties in terms of morphology and chemical composition, these have no influence on the final electrocatalytic activity, confirming that Zn is a non-effective transition metal for the formation of ORR active sites. However, unlike in acid conditions, the Zn-N-C and H-N-C catalysts have a non negligible ORR activity in alkaline conditions, as typical for all carbonaceous materials and in particular for N-doped carbon materials [120].



**Figure 27.** (A) Staircase voltammeteries (10 mV potential step, 30 s holding time) of the Me-N-C catalysts (Me = Fe, Co, Cu, Zn, H) recorded in O<sub>2</sub>-saturated 0.1 M KOH at 900 rpm RDE rotation speed. The curve of a commercial Pt catalyst (Pt 20 wt. % on Vulcan, Quintech®) in both cathodic and anodic scan directions is also shown for comparison. (B) Tafel plots after correction for mass-transport contribution derived from the SV in (A).

Fe-N-C catalyst exhibit a slope of about 63 mV dec<sup>-1</sup> (almost the same that in acidic conditions) and an  $i_0$  value about 3 orders of magnitude higher than in acid conditions. Similar results for iron and nitrogen containing C-based catalysts can be found in the literature [121,122]. Higher Tafel slope values between 70 and 80 mV dec<sup>-1</sup> were measured in other works [123,124].

The Co- and Cu-N-C catalysts have a lower Tafel slope, of about 45 mV dec<sup>-1</sup>. Lower Tafel slopes of about 35 mV dec<sup>-1</sup> were typically observed for surface area carbon in alkaline solution [125]. These low values of Tafel slopes are explained in terms of production of peroxide ion intermediate.



**Figure 28.** Plot representing the linear zones of the potential vs logarithm of the mass-transport corrected current densities in Figure 27. Straight trend lines with their respective equations used for the calculations of  $\alpha_c$  and  $i_0$  are also shown.

These results could confirm the results of the RRDE analysis, that show a higher amount of  $\text{H}_2\text{O}_2$  production for Co- and Cu-N-C catalysts than for Fe-N-C (which exhibits almost no  $\text{H}_2\text{O}_2$ ).

For Zn- and H-N-C catalysts the Tafel slope is of about  $50 \text{ mV dec}^{-1}$ . Regarding the Pt/C catalyst it exhibit the typical behavior of the Pt polycrystalline electrodes in alkaline conditions, which shows two Tafel regions with slopes of 60 and  $120 \text{ mV dec}^{-1}$  for low and high overpotentials, respectively [126]. For Pt, as in acid conditions, the existence of these two slopes regions is explained in terms of the coverage of the electrode surface by adsorbed oxygen, which follows a Temkin isotherm at low overpotentials (where the Pt surface is highly covered by adsorbed OH) and a Langmuir isotherm at higher overpotentials (where the Pt surface is free from adsorbed OH species).

**Table 8.** ORR kinetic parameters in alkaline conditions for all of the Me-N-C catalysts and for the Pt/C commercial catalyst (for Pt/C Tafel slope,  $\alpha_c$  and  $i_0$  are calculated in low and high overpotential regions).

| Sample  | $E_{\text{on}}$<br>[V vsRHE] | $E_{1/2}$<br>[V vsRHE] | Tafel slope<br>[mV/dec] | $\alpha_c$  | $i_0$<br>[mA/cm <sup>2</sup> ]            |
|---------|------------------------------|------------------------|-------------------------|-------------|---|
| Fe-N-C  | 0.98                         | 0.87                   | 63.2                    | 0.94        | $1.14 \cdot 10^{-5}$                      |
| Co-N-C  | 0.92                         | 0.84                   | 47.2                    | 1.25        | $2.72 \cdot 10^{-8}$                      |
| Cu-N-C  | 0.89                         | 0.82                   | 44.6                    | 1.33        | $4.03 \cdot 10^{-9}$                      |
| Zn-N-C  | 0.85                         | 0.75                   | 53.3                    | 1.11        | $9.79 \cdot 10^{-9}$                      |
| H-N-C   | 0.84                         | 0.75                   | 49.2                    | 1.20        | $2.00 \cdot 10^{-9}$                      |
| Pt cath | 1.00                         | 0.89                   | 67.5 / 116              | 0.88 / 0.51 | $7.72 \cdot 10^{-4} / 6.09 \cdot 10^{-3}$ |
| Pt anod | 1.01                         | 0.92                   | 58.2 / 128              | 1.02 / 0.46 | $2.71 \cdot 10^{-5} / 5.27 \cdot 10^{-3}$ |

Fe-N-C catalyst has an exchange current density value of about 3 – 4 orders of magnitude higher than the other Me-N-C catalysts. This value is almost comparable with the one of Pt/C catalyst in the low overpotential region (in both anodic and cathodic scan directions). Therefore we can conclude that the ORR catalytic behavior of Fe-N-C catalyst in alkaline conditions is very close to the Pt/C catalyst, underlying the advantage in using these types of Me-N-C non-precious metal catalysts as cathodic catalysts for alkaline exchange membrane fuel cells.

Interestingly, it was found by Perez et al. [125] that the Tafel slope obtained on Pt/C catalysts increases from a value of  $35 \text{ mV dec}^{-1}$  for the carbon support without Pt, to a value close to  $60 \text{ mV dec}^{-1}$  for a Pt wt. % of 30 %. At the same time the number of electrons involved in the ORR changes from a value close to two to a value close to four. This behavior can be interpreted by a combined participation of the carbon and the platinum particles in the catalysis of the ORR. For the lower Pt/C ratios, the contribution of the carbon is higher and the values are closer to the typical values for pure carbon, which is a catalyst of  $\text{O}_2$  reduction to  $\text{H}_2\text{O}_2$  in alkaline conditions. Otherwise, for higher Pt contents, the contribution of Pt, and therefore the complete reduction to  $\text{H}_2\text{O}$  is

predominant [87]. Comparing the results obtained in alkaline and acid conditions, we can observe that the most active catalyst, that is Fe-N-C, shows almost 150 mV lower  $E_{on}$  in alkaline media. As consequence, the mixed kinetic-diffusion region is less well-defined in acid than in alkaline solution, suggesting that in acid conditions the reaction is under kinetic control even at high overpotentials. Comparing the  $i_0$  value of Fe-N-C in the low overpotential region, (see Table 4 and Table 8), it is almost 3 orders of magnitude higher in 0.1 M KOH than in 0.5 M  $H_2SO_4$ . Concerning the Tafel slopes, they are almost the same in both pH conditions, suggesting that the rate determining step is the same in both cases.

### 3.3.2. RRDE analysis

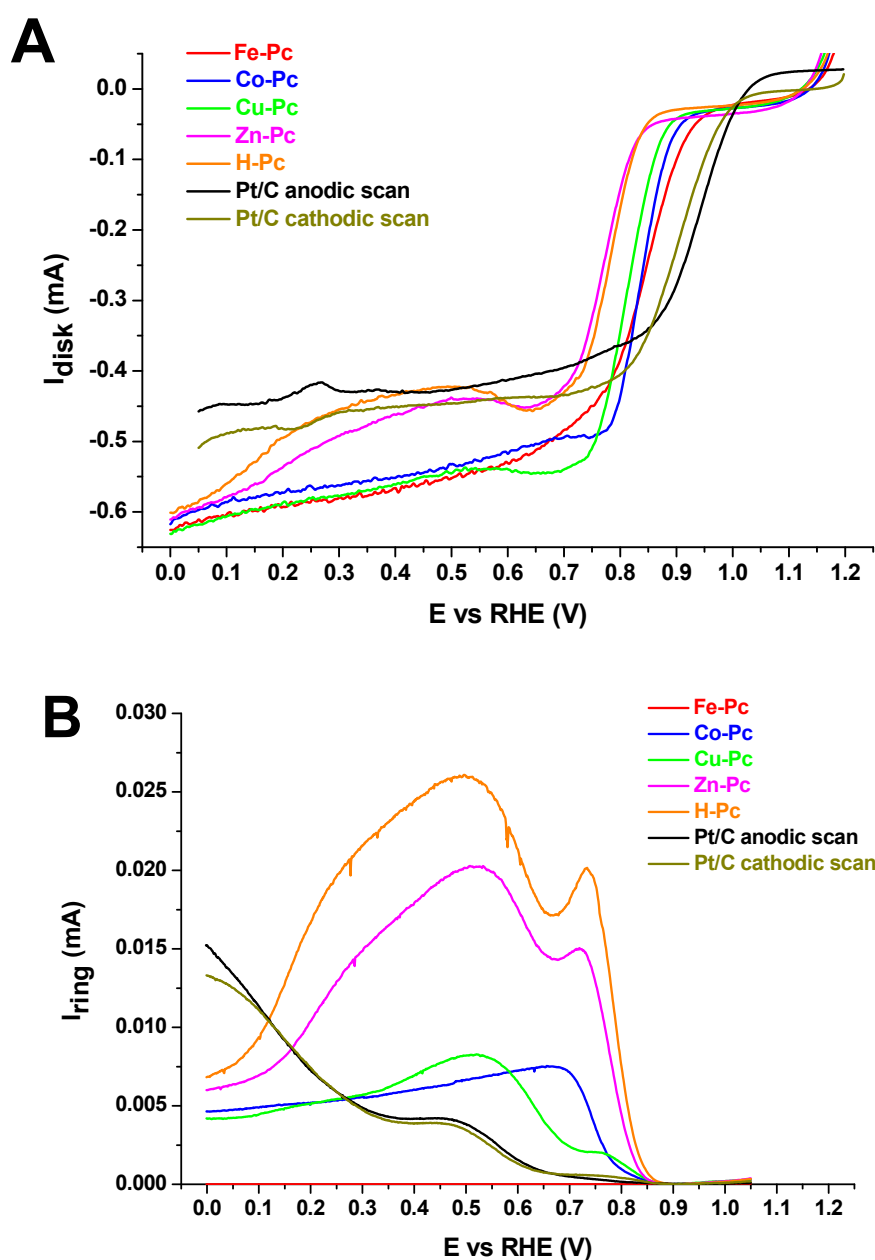
In order to explain these differences (and analogies) between the catalyst behavior in the two different electrolytes, we further analyze the ORR by performing a RRDE test also in alkaline conditions. The results are shown in Figure 29. For Fe-N-C the measured ring current is surprisingly almost zero over the whole disk scanned potential range, suggesting that no  $H_2O_2$  is generated by this catalyst in alkaline conditions. A very low hydrogen peroxide generation for Fe-N/C catalyst was reported by Ramaswamy and Mukerjee [101] and by Chung et al. [124] in 0.1 M NaOH solution. This low hydrogen peroxide generation at lower overpotentials is a noteworthy result in comparison with what obtained for other NPMC, and also with Pt-based catalysts in alkaline conditions. It could be explained by the fact that this catalyst is not supported on C material but it is “self-supported” (no external source of carbon other than C atoms contained in the Fe-phthalocyanine molecule precursor was added during the synthesis). Therefore the additional hydrogen peroxide generation contribution due to C support is not present, or, however, it is lower in comparison with other Me-N/C catalysts reported in the literature. In alkaline conditions, for NPMC in which the onset potential of complete ORR to  $H_2O$  and  $H_2O_2$  coincide, the total  $H_2O_2$  generation could seem higher. In this case, the ORR onset potential is much higher than the usual onset potential for  $H_2O_2$  generation in alkaline conditions ( $\sim 0.8$  V vs RHE) [120]. Thus, due to the enhanced stability of  $HO_2^-$  ion on the Fe-N-C catalyst active sites in alkaline conditions as reported by Mukerjee [100,101], the generated peroxide could be faster reduced to  $H_2O$  without being desorbed in the bulk of the electrolyte solution.

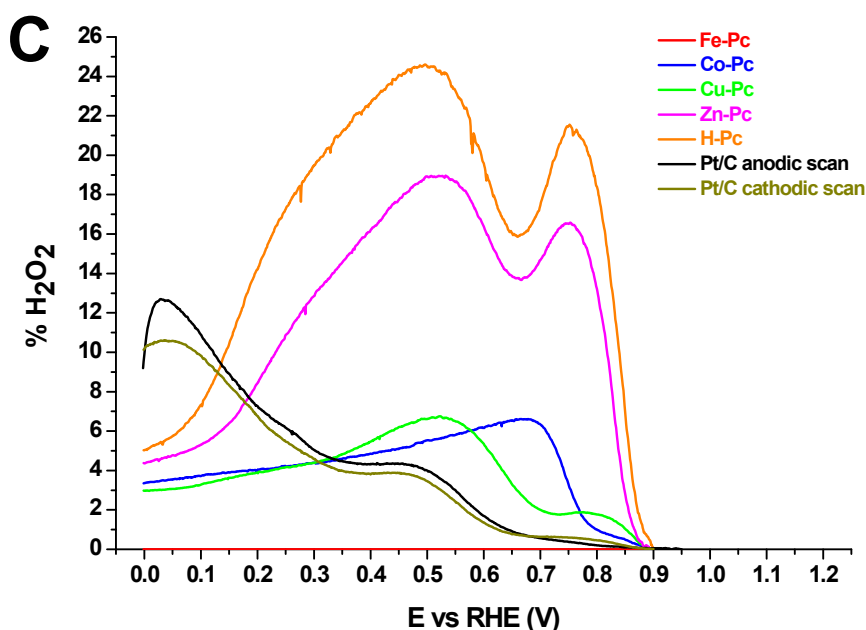
Co- and Cu-N-C catalysts lead to higher generation of  $H_2O_2$ , showing a peak of about 7 % at the potential of 0.7 and 0.525 V vs RHE, respectively. Then, as the disk electrode potential decrease, the peroxide generation decreases, reaching values around 3 – 4 %. Similar values can be found in the literature for Me-N-C catalysts [124]. Zn- and H-N-C catalysts generate considerably higher quantities of  $H_2O_2$ , showing the same trend with disk potential. They have a first peak around 0.75 V vs RHE, and a second peak (higher than the previous one) at 0.5 V vs RHE. For Zn-N-C catalyst the

two peaks are of 17 and 19 H<sub>2</sub>O<sub>2</sub> % respectively. The values for H-N-C are even higher, being of 21 and 25 H<sub>2</sub>O<sub>2</sub> % respectively.

These peaks in ring current at 0.50 V are most likely due to the carbonaceous structure of the catalysts. At higher overpotentials the ORR process becomes more efficient and consequently the peroxide production decreases.

Comparing the RRDE tests results in acid and alkaline conditions (Figure 25 C and 29 C, respectively), we can noticed than the most active Me-N-C catalysts, that is Fe-N-C and Co-N-C, exhibit a much higher peroxide generation in acid than in alkaline conditions. For Pt/C catalyst exactly the opposite behavior is observed [101].





**Figure 29.** RRDE test measurements performed in 0.1 M KOH for Fe-, Co-, Cu-, Zn- and H-N-C and for a commercial Pt/C catalyst: (A) disk currents, (B) ring currents and (C) hydrogen peroxide molar proportion. Ring potential 1.2 V vs RHE, electrode rotation speed 900 rpm, disk potential scan rate 5 mV s<sup>-1</sup>.

This was explained by the fact that the onset potential of peroxide reduction is higher than the onset potential of ORR in alkaline media. Therefore the former reaction is kinetically favored such that any peroxide intermediate formed during ORR in 0.1 M KOH will be immediately reduced to water. Otherwise, in acid conditions, the peroxide reduction is a slower reaction than the ORR, (as demonstrated by the results in Figure 24) due to weak binding of H<sub>2</sub>O<sub>2</sub> on the active site, leading to its desorption into the bulk electrolyte [100,101]. This fact suggests that the higher stabilization of the peroxide intermediate on the active site is crucial for the enhanced complete 4 e<sup>-</sup> reduction in alkaline conditions. The reasons for the stability of peroxide intermediate on the active site in alkaline but not in acidic media is explained in terms of electrostatic interaction between the positive charge on the cathode surface and the anionic nature of the peroxide intermediate in alkaline media. The cationic nature of the Fe<sup>2+</sup> / Fe<sup>3+</sup> (that is one of the possible ORR active sites) also favor this electrostatic stabilization of the HO<sub>2</sub><sup>-</sup> (which is the stable form of hydrogen peroxide at pH > 12 ) species in alkaline media. This stabilization leads to the complete 4 e<sup>-</sup> ORR in alkaline media [127]. This electrostatic “advantage” is not present in acidic media due to the neutral charge on H<sub>2</sub>O<sub>2</sub>.

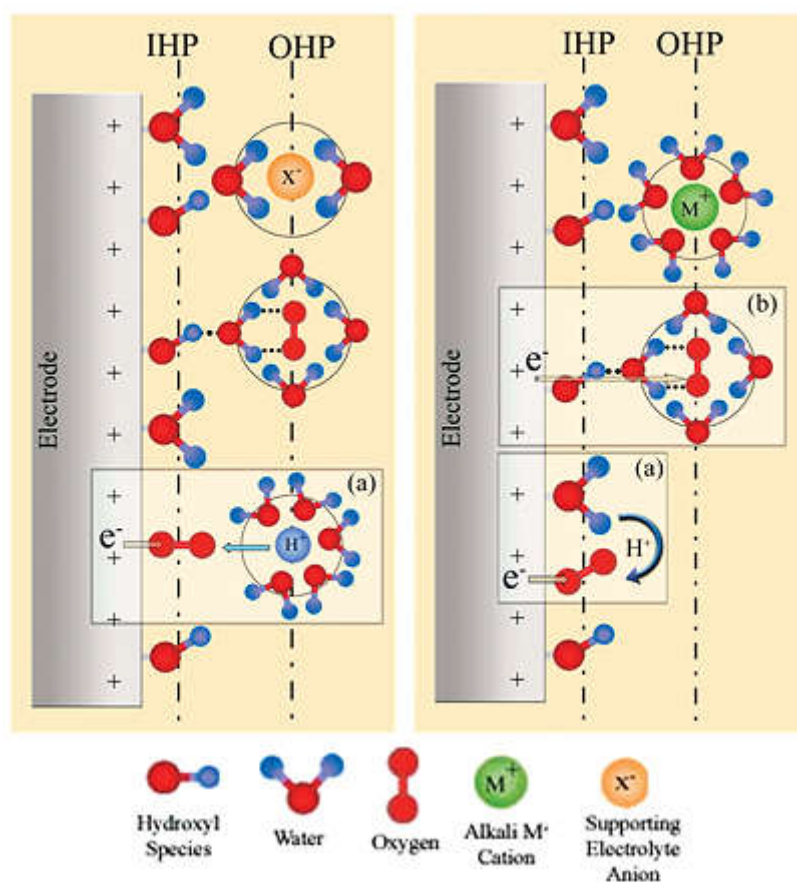
Comparing the results of RRDE tests on Pt/C catalyst in acid and alkaline media (see Figure 25 and Figure 29), higher ring currents, and consequently higher peroxide molar % generation are obtained in alkaline medium over the whole potential range. In acid conditions, as previously discussed, the ring current shows a noticeable increase only at high overpotentials, where the hydrogen

underpotential deposition phenomena start to occur. This is particularly evident in the anodic scan direction.

Otherwise, in alkaline conditions, a considerable detection of peroxide formation at the ring takes place at about 200 mV more positive potentials, considering the anodic scan. This is related to Pt-OH formation from specific adsorption of hydroxide anions, which favors the peroxide formation via the “outer-sphere” electron transfer mechanism at –OH-covered Pt sites (see Figure 30), as described in detail by Mukerjee [100].

Therefore, in alkaline media, the –OH species present on Pt surface promote the “outer-sphere” reaction mechanism, which is likely to be faster than the “inner-sphere” mechanism, which also occurs in parallel. In acid media instead, only the “inner-sphere” mechanism is occurring, limiting the peroxide formation. The presence of the similar Tafel slopes for ORR for Pt in both acid and alkaline media suggests that the rate determining step is still the first electron transfer to adsorbed O<sub>2</sub> via the inner-sphere mechanism at an oxide-free Pt site (being the “outer-sphere mechanism” faster). In their comprehensive review, Ramaswamy and Mukerjee state that on Fe-N-C catalysts the direct adsorption of molecular O<sub>2</sub> on the Fe<sup>2+</sup> active site is facilitated, because the specifically adsorbed OH<sup>–</sup> species on the Fe<sup>2+</sup> site acts as a labile ligand, which can be easily displaced by the molecular O<sub>2</sub>. This causes the successful 4 e<sup>–</sup> reduction of O<sub>2</sub> with a minimal occurrence of the “outer-sphere” electron transfer mechanism, as confirmed by the almost-zero ring current detected in our RRDE experiment with the Fe-N-C catalyst.

For the other Me-N-C catalysts, where the Fe<sup>2+</sup> active center is not present, the higher ring currents detected are primarily originated from the 2 e<sup>–</sup> reduction of O<sub>2</sub> to HO<sub>2</sub><sup>–</sup> promoted by the carbon support [128]. Carbon support promotes the outer-sphere electron transfer via mediation by the quinone/hydroquinone surface functional groups, which act similarly to the surface hydroxide species on Pt.



**Figure 30.** Schematic of the double-layer structure during ORR in acidic (left) and alkaline (right) conditions. Insets (a) and (b) respectively illustrate the “inner-sphere” and “outer-sphere” electron transfer processes occurring in the two different pH conditions [101].

### 3.4. Single cell measurements.

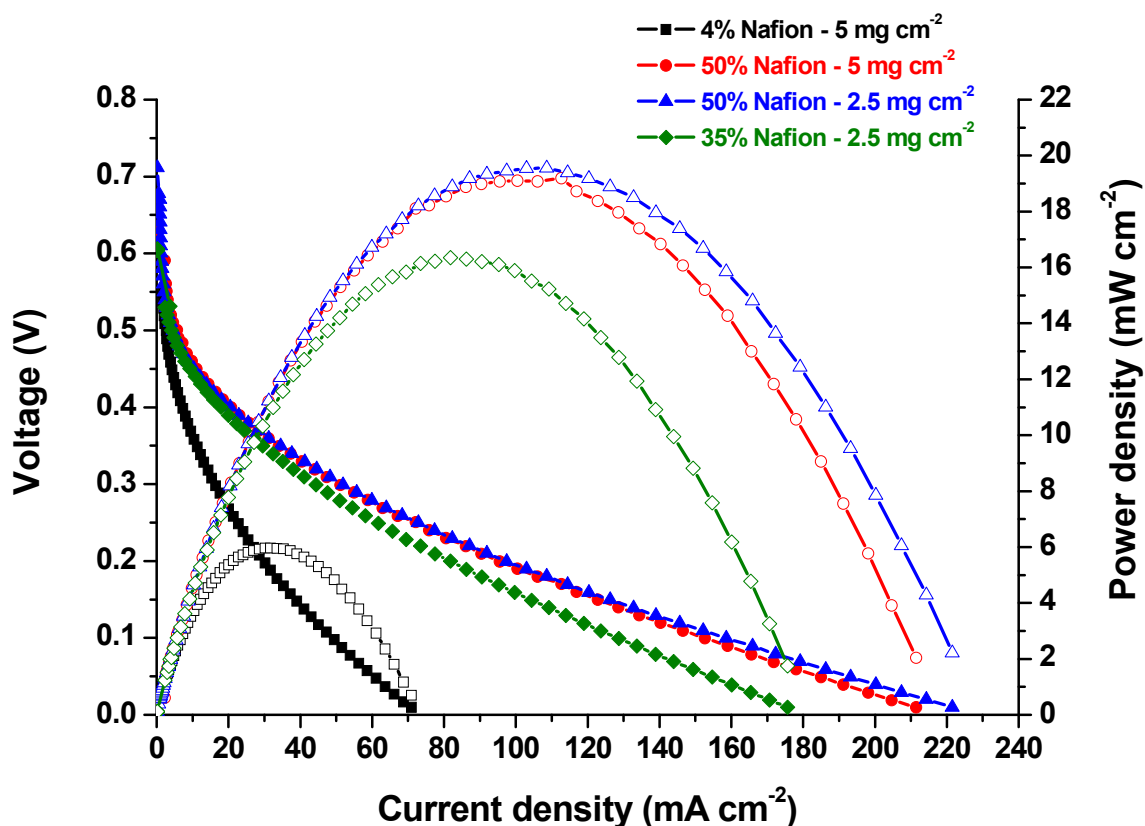
As discussed in detail in the previous section, Fe-N-C is the catalyst that exhibits the most interesting properties in terms of activity and selectivity in both acid and alkaline media. Therefore, its performance as cathode catalyst has been evaluated in different types of exchange membrane fuel cells. With a proton conducting electrolyte membrane (acid conditions), the examined fuels were hydrogen and methanol. In alkaline conditions (OH<sup>-</sup> conducting electrolyte membrane), the cell was fed with ethanol.

#### 3.4.1. Acid DMFC test.

The performance of Fe-N-C catalyst was analyzed in a single DMFC fed with 2 M methanol and pure oxygen at 90 °C temperature. The first part of this study consisted in the optimization of the cathode catalyst layer. The parameters considered for the optimization were: the Nafion ionomer content in the dry catalytic layer, the total catalyst loading and the Vulcan carbon black quantity mixed with Fe-N-C catalyst before deposition on the GDL.



First, some tests were done using pure Fe-N-C catalyst (without mixing with Vulcan) with different loadings and amounts of Nafion. The results are shown in Figure 31. The fuel cell performance is low with the smaller amount of Nafion (4 wt. %). This was the same amount used for the anode catalyst layer preparation [115]. Increasing the amount of Nafion to quantities more similar to the typical used in the literature for similar Fe-N/C NPMC (i.e. 35 and 50 wt. %) the performances increase considerably. In particular, comparing the results obtained with the same catalyst loading ( $2.5 \text{ mg cm}^{-2}$ ), the performances are better with the higher Nafion content (50 wt. %). With this Nafion amount, two tests were made with different catalyst loadings ( $2.5$  and  $5 \text{ mg cm}^{-2}$ ), showing almost the same performance. Even better, a slightly better performance was obtained with the lower catalyst loading, showing that using higher loadings of catalyst is not useful for increasing the DMFC performance. This suggests that the catalyst layer is affected by mass transport limitations. Possibly, in presence of a thicker catalyst layer, the tortuosity of the electrons, protons and oxygen path increased too much, making the presence of more catalyst totally useless. Such type of mass transport problematics were typically found in the literature for NMPC synthesized with a silica template method [17].

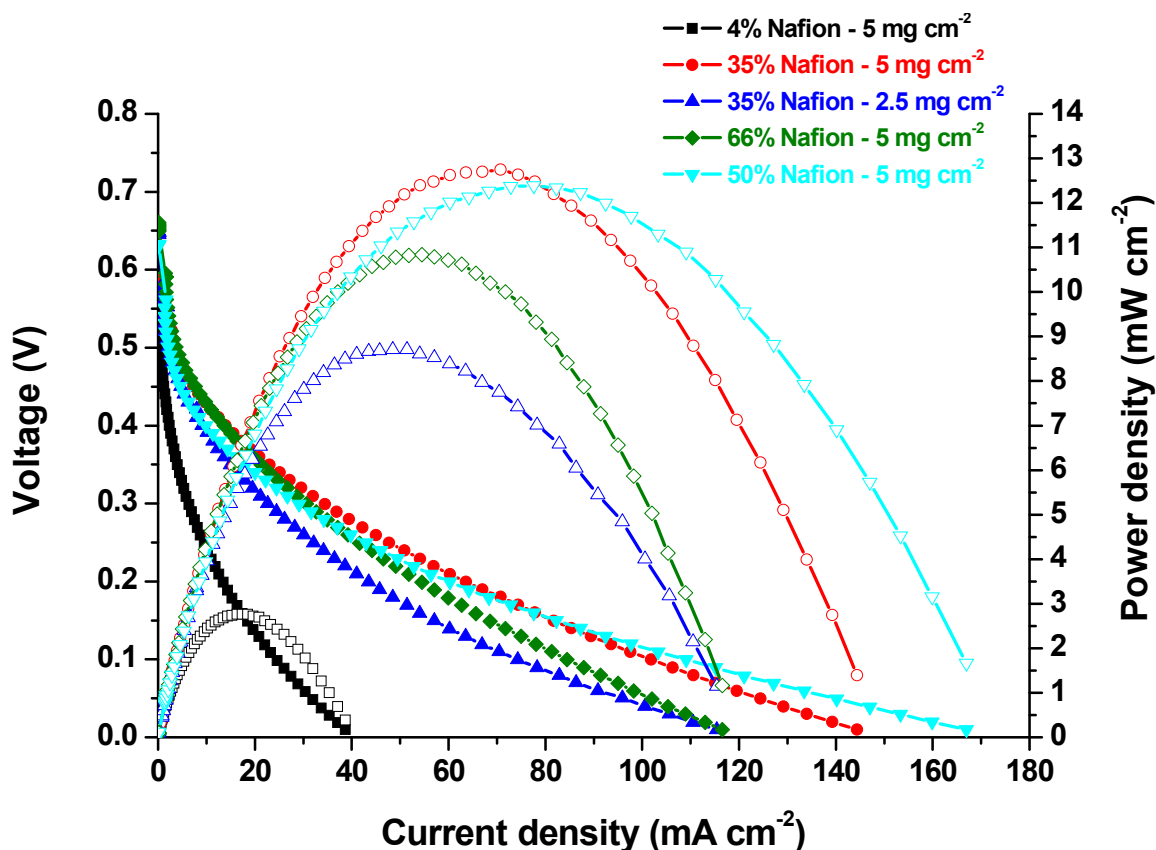


**Figure 31.** DMFC performances at 90 °C with different loadings of Fe-N-C and different Nafion wt. % contents on the dry cathode. Polarization curves (open symbols) and power density curves (closed symbols).

In parallel, we also tested the DMFC using the Fe-N-C catalysts mixed in 1:1 wt. proportion with Vulcan. These tests were done to investigate the cathode behavior in presence of additional carbon.

In facts, some studies have been published in the literature with both Pt-based and non-precious-based catalysts showing an improvement in fuel cell performance with the addition of carbon in different proportions to the catalytic layer [129–131]. These improvements in performance could be due to the changes the hydrophobicity of the catalyst layer, affecting water transport properties [131,132]. Another reason could be ascribed to the increasing in the electronic conductivity provided by the additional carbon. In fact, the better performances for MEA prepared using NPMC as cathodic catalysts have been obtained with Nafion ionomer contents between 25 and 75 wt. % [116,131]. Such high ionomer contents could cause separation of the catalyst particles, breaking the electronic pathway leading to loss of electronic conductivity. One way of compensation is to add conductive material, such as carbon, to the catalyst before deposition onto the GDL. Carbon can act as a bridge, interconnecting catalyst particles and reestablishing a continuous electronic pathway.

Comparing the results of these tests (see Figure 32), with the results obtained without the addition of Vulcan (Figure 31), we can see that there is no any improvement, suggesting that for our Fe-N-C catalyst the Vulcan addition is not useful to get better cell performances. In fact, considering the same total loading on the GDL and the same Nafion % content (Vulcan + Fe-N-C catalyst), the results obtained with the pure Fe-N-C are always better in terms of open circuit potential, power density and current density. This could be explained by the presence of more catalyst (the double quantity) on the electrode for the case of pure Fe-N-C tests.



**Figure 32.** DMFC performances at 90 °C with different loadings of Fe-N-C + Vulcan in 1:1 wt. ratio and different Nafion wt. % contents on the dry cathode. Polarization curves (open symbols) and power density curves (closed symbols).

However, also considering only the total amount of Fe-N-C catalyst on the electrode (e.g. 2.5 mg cm<sup>-2</sup> of Fe-N-C and 5 mg cm<sup>-2</sup> of Fe-N-C + Vulcan 1:1 wt. ratio), the results obtained with the pure catalyst are better, even if the total amount of catalyst in this case is the same. This could be explained in terms of mass transport limitations in this catalyst occurring especially at high current densities [17].

The results of Figure 31 and 32 are summarized in Table 9 in terms of cell open circuit potential, maximum current density and maximum power density.

**Table 9.** Performance parameters for the DMFC tests shown in Figures 31 and 32.

| Vulcan content<br>[wt. %] | Nafion content<br>[wt. %] | Catalyst layer loading<br>[mg cm <sup>-2</sup> ] | E <sub>oc</sub><br>[V] | i <sub>max</sub><br>[mA cm <sup>-2</sup> ] | P <sub>max</sub><br>[mW cm <sup>-2</sup> ] |
|---------------------------|---------------------------|--|------------------------|--|--|
| 0                         | 4                         | 5  | 0.62                   | 71   | 6.0  |
| 0                         | 35                        | 2.5  | 0.61                   | 176  | 16.3                                       |
| 0                         | 50                        | 5  | 0.63                   | 211  | 19.2                                       |
| 0                         | 50                        | 2.5  | 0.71                   | 222  | 19.6                                       |
| 50                        | 4                         | 5  | 0.60                   | 39   | 2.8  |
| 50                        | 35                        | 2.5  | 0.65                   | 115  | 9.3  |
| 50                        | 35                        | 5  | 0.59                   | 144  | 12.7                                       |
| 50                        | 50                        | 5  | 0.63                   | 167  | 12.4                                       |
| 50                        | 66                        | 5  | 0.66                   | 117  | 10.8                                       |

Therefore, the best results for the Fe-N-C catalyst as DMFC cathode are obtained with no Vulcan addition, 50 wt. % Nafion content and a catalyst loading of 2.5 mg cm<sup>2</sup>. These conditions were chosen hereafter as optimum and were used to perform the further fuel cell tests of Fe-N-C.

However, for any particular electrocatalysts, the optimal ionomer to catalyst ratio and loading have to be found, to get the best MEA test performance [131]. For example, in a recent study by Sebastián et al. [116] on a NPMC catalyst used as cathode for DMFC, two catalyst loadings were examined (2.7 and 7.4 mg cm<sup>-2</sup>) and the best performances were obtained with the highest catalyst loading. This is most likely due to the structural and morphological characteristics of the proper catalyst material. The ionomer transports H<sup>+</sup> ions to active sites and helps to remove the H<sub>2</sub>O generated from active sites. Generally, a higher ionomer content has a beneficial effect on the kinetics, due to the better ionic transport and conductivity, but it hinders the mass transport causing blocking of the pores [133]. From the results in Table 9, it can be noticed that both Nafion amount and catalyst loading influence the cell E<sub>oc</sub>. Higher Nafion contents and lower catalyst loadings result in slightly higher E<sub>oc</sub>. This could be explained by the fact that the above mentioned beneficial effect of the ionomer on the electrode kinetics. Moreover, lower catalyst loading, resulting in a thinner electrode, may favor the transport phenomena at the catalytic layer (including mass and charge transport), which may lead to slight differences in charge transfer phenomena at open circuit [17,116].

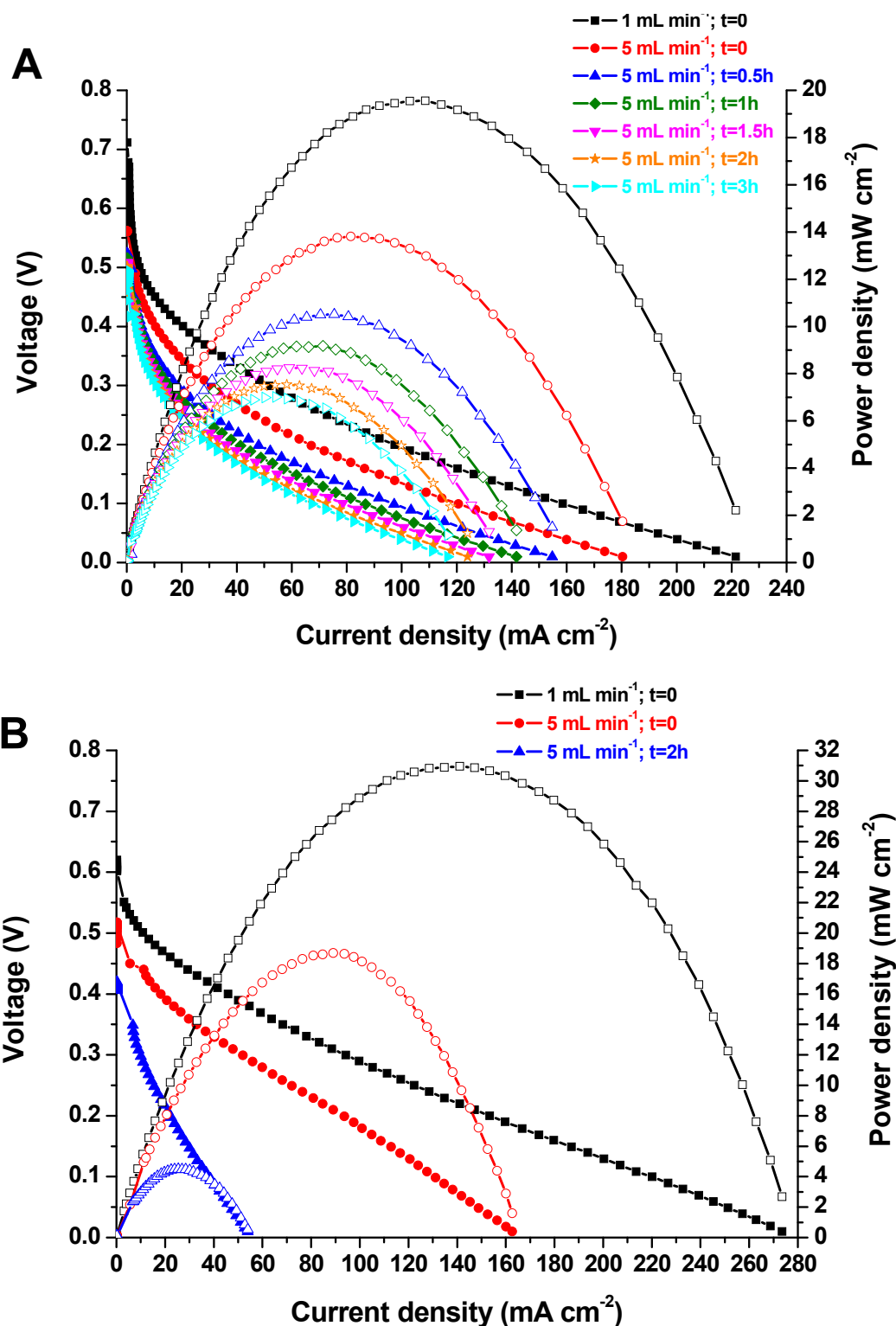
In these tests, we did not consider the effect of temperature and methanol concentration, having fixed these two parameters to 90 °C and 2 M, respectively. However, we can mention that operating with high methanol concentration has the advantage of providing higher energy density to the DMFC system, but has the drawback of suffering major losses due to crossover caused by the increased diffusion gradient of methanol through the polymeric proton conductive membrane. Working at higher temperature also increases the crossover, but at the same time, it favors the kinetics at both

anode and cathode, and the polymeric membrane ionic conductivity [116]. The operative temperature of our tests (90 °C) was sufficiently low to ensure the structural stability for the Nafion membrane. In order to assess the durability of Fe-N-C catalyst, a short-term durability test was performed on the MEA prepared with the cathode in the optimal conditions. The cell potential was kept constant to 0.4 V, and a polarization curve was recorded every 30 minutes. The methanol flow rate was set to 5 mL min<sup>-1</sup> (5 times higher than the flow rate used for the polarization curves recorded in Figure 31 and 32). The use of a higher flow rate, should generally lead to an increase of the kinetics due to a higher flux of reactants to the anodic compartment [115]. However, this also causes an increase of the water and methanol diffusion through the Nafion 117 membrane. The results of this test are shown in Figure 33-A. The curve recorded with 1 mL min<sup>-1</sup> methanol flow rate (taken from Figure 31) is also shown for comparison. The cell performance parameters at different time along the test are reported in Table 10. The cell performance show a considerable decrease at the beginning of the test (t=0) just with the increase of the methanol flow rate. The maximum power density decreases of about 30% and the open circuit potential has a negative shift of 150 mV. Even if the Fe-N-C catalyst exhibit a high methanol tolerance (see Section 3.2.7), the increase of the diffusion of both methanol and water through the membrane could cause problems of water removal from the cathode (cathode flooding), especially at high current density values, where a higher amount of water is also generated at the cathode.

After the first 30 minutes of test, a further important performance decrease is observed, with the maximum power density decreasing to 46.5 % of the initial value. However, the  $E_{oc}$  further decreases only 40 mV. Continuing along the test, the cell shows a slower performance decrease, losing about 64% of its maximum power density after 3 h of test. Interestingly, the  $E_{oc}$  remains almost constant, showing only a 60 mV negative shift between 0.5 and 2 h of tests, and remaining almost constant during the last hour. This could indicate that the fuel cell deactivation is mainly due to problems not related to the formation of a mixed potential due to the methanol oxidation occurring at the cathode, as suggested by the methanol tolerance test. As previously discussed, these deactivation is most likely due to water management problems.

In particular, the higher flow rate of methanol leads to a significant performance loss for the DMFC even if the cathode catalyst is highly methanol tolerant, probably due to a severe flooding [134] occurring in particular the catalyst micropores, where the majority of the ORR active sites are most probably located.

Sebastián et al. performed a 10 h stability test on a NPMC obtained by pyrolysis of Fe, N and C precursors, and obtained a similar trend in performance decay, detecting the major decrease within the first 3 h. Afterwards, the performance loss decelerates with time [116].



**Figure 33.** (A) Performances at 90 °C of the DMFC prepared with Fe-N-C catalyst at the cathode along the durability test (potential kept constant at 0.4 V for 3 h) with 5 mL min<sup>-1</sup> methanol flow. The polarization curve with 1 mL min<sup>-1</sup> methanol flow is also shown for comparison. (B) Performances at of the DMFC prepared with commercial Pt/C catalyst at the cathode in the same conditions of (A).

As a comparison, the same test was conducted for a MEA prepared using a standard Pt/C commercial catalyst at the cathode (Pt loading 1 mg cm<sup>-2</sup>). The results are shown in Figure 33 B. The performance

of the DMFC with Pt/C catalyst at the cathode exhibits a considerably higher performance in comparison with the MEA prepared with Fe-N-C catalyst at the beginning of the experiment with a methanol flow of 1 mL min<sup>-1</sup> (30.9 vs 19.6 mW cm<sup>-2</sup> maximum power density). However, it is worth noting that the initial E<sub>oc</sub> of the MEA with Pt/C catalyst at the cathode is about 100 mV lower than the E<sub>oc</sub> of the MEA prepared with Fe-N-C (see Table 10), despite the ORR onset potential of Pt/C catalyst in acidic conditions is considerably higher than for Fe-N-C. This confirms that the having Pt/C as cathodic catalyst, the DMFC suffers the presence of a mixed potential at the cathode due to methanol oxidation, causing an important performance decrease [135]. Simply by increasing the methanol flow rate, the performance of the Pt/C cathode-based MEA shows a decrease of about 40% in maximum power density, but remaining still better than the Fe-N-C results in the same conditions. The E<sub>oc</sub> also shows a considerably high decrease of about 110 mV, being lower than the one of the Fe-N-C based MEA in the same conditions. After 2 hours of test, the performance decrease of the DMFC with Pt/C is even more evident. The maximum power density decreased of 85% in comparison to its initial value, being well low than for the Fe-N-C. In addition, the E<sub>oc</sub> value drop down to 0.42 V, that is, 80 mV lower than for Fe-N-C.

In spite of not showing a very high stability, the performance of the DMFC single cell test with Fe-N-C is better in terms of durability than that of Pt/C. The superior tolerance to methanol crossover of Fe-N-C is clearly observed working at 5 mL min<sup>-1</sup> methanol feed rate. Even after 3 h test, the polarization and power density curves for the DMFC prepared with Fe-N-C are better than the ones of the DMFC prepared with Pt/C after only 2 h test. In particular, the drop in E<sub>oc</sub> for the DMFC based on Pt/C cathode highlights the very detrimental effect of methanol cross-over.

**Table 10.** Performance parameters for DMFC stability tests in Figures 33 A-B for Fe-N-C and Pt/C catalysts used at the cathode.

| Cathode catalyst | MeOH flow [mL min <sup>-1</sup> ] | time [h] | E <sub>oc</sub> [V] | i <sub>max</sub> [mA cm <sup>-2</sup> ] | P <sub>max</sub> [mW cm <sup>-2</sup> ] | P <sub>max</sub> per g of Pt [W g <sub>Pt</sub> <sup>-1</sup> ] | P decrease [%] |
|------------------|-----------------------------------|----------|---------------------|---|---|---|----------------|
| Fe-N-C           | 1                                 | 0        | 0.71                | 222                                     | 19.6                                    | 19.6  | -              |
| Fe-N-C           | 5                                 | 0        | 0.56                | 180                                     | 13.8                                    | 13.8  | 29.6           |
| Fe-N-C           | 5                                 | 0.5      | 0.52                | 155                                     | 10.5                                    | 10.5  | 46.5           |
| Fe-N-C           | 5                                 | 1        | 0.52                | 142                                     | 9.2                                     | 9.2   | 53.1           |
| Fe-N-C           | 5                                 | 1.5      | 0.51                | 132                                     | 8.3                                     | 8.3   | 57.7           |
| Fe-N-C           | 5                                 | 2        | 0.50                | 124                                     | 7.5                                     | 7.5   | 61.8           |
| Fe-N-C           | 5                                 | 3        | 0.50                | 117                                     | 7.0                                     | 7.0   | 64.3           |
| Pt/C             | 1                                 | 0        | 0.61                | 274                                     | 30.9                                    | 15.5  | -              |
| Pt/C             | 5                                 | 0        | 0.52                | 163                                     | 18.7                                    | 9.4   | 39.5           |
| Pt/C             | 5                                 | 2        | 0.42                | 54                                      | 4.5                                     | 2.3   | 85.5           |

The use of a NPMC at the cathode of DMFC is convenient not only in terms of durability performances, but also from the economical point of view. As suggested by the maximum power density per g of total Pt used for the MEA fabrication (see Table 10), the use Fe-N-C catalyst leads to a considerable decrease of the total MEA cost, considering that the main contribution to the total MEA cost is due to the Pt total content (Ru is about one order of magnitude cheaper than Pt, and the NPMC catalyst is about two orders of magnitude cheaper than Pt [116]). In fact, the MEA fabricated with Pt/C as cathodic catalyst contains the double amount of Pt than the MEA fabricated with Fe-N-C (2 mg of total Pt per cm<sup>2</sup> and 1 mg of total Pt per cm<sup>2</sup>, respectively).

Nevertheless, the performance of this Fe-N-C catalyst in DMFC are still lower than what expected, leaving open space for future work in performance improvement. From these results, this could be achieved improving the structural features of the catalyst, providing better mass-transport properties, which could avoid or at least limit the flooding of the micropores.

#### 3.4.2. $H_2 / O_2$ PEMFC test.

The performance of Fe-N-C catalyst was also tested in a PEMFC fed with pure  $H_2$  and  $O_2$  at anode and cathode, respectively. Otherwise than methanol, the  $H_2$  crossover through the Nafion membrane is not so high. Therefore, we used a thinner membrane (Nafion 112 instead of Nafion 117 used for DMFC) in order to minimize the ionic conduction resistance.

The polarization and power density curves resulting from these tests are shown in Figure 34, together with the results of the same test conducted on a MEA fabricated using a commercial Pt/C catalyst at the cathode. The maximum power density recorded for Fe-N-C was 105 mW cm<sup>-2</sup>, which is about 1/3 than the maximum power density obtained with the Pt/C catalyst (335 mW cm<sup>-2</sup>) in the same testing conditions.

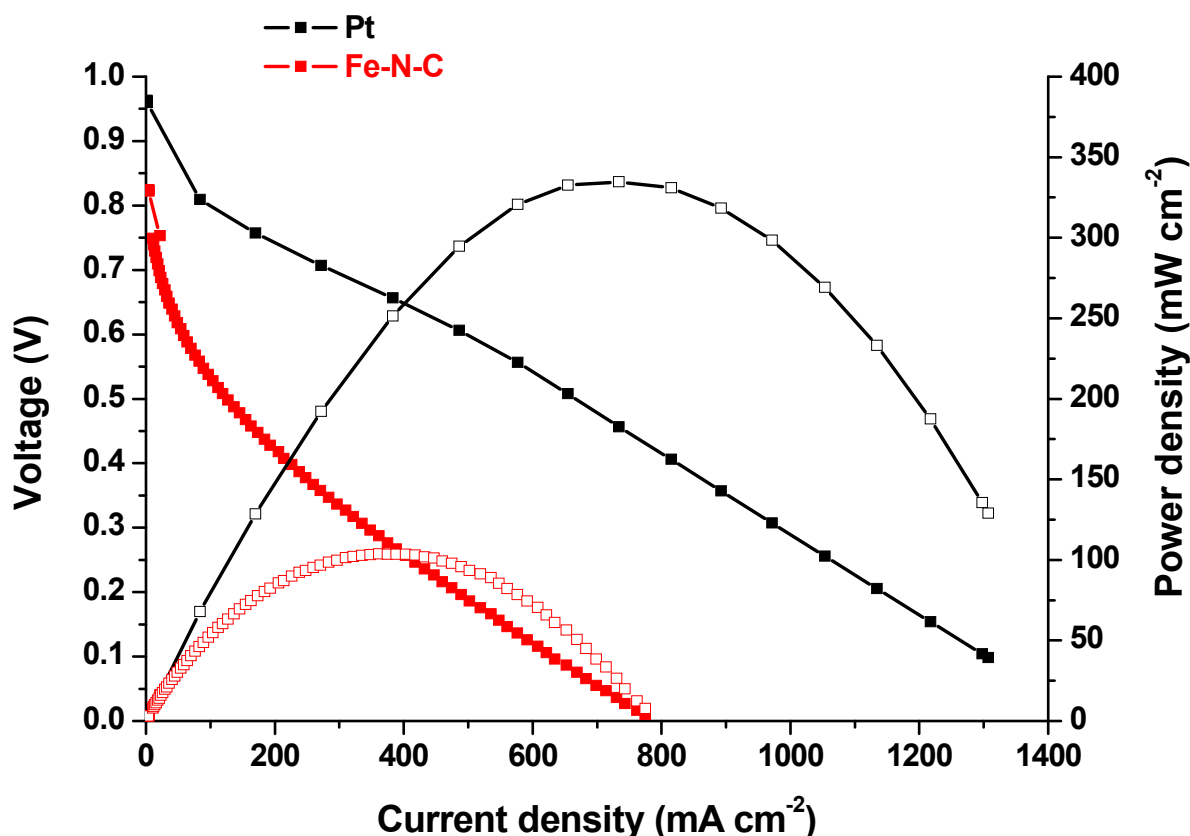
However, if we normalize the maximum power density per g of total Pt used for the MEA fabrication, with Fe-N-C catalyst at the cathode we obtain 350 W g<sub>Pt</sub><sup>-1</sup> (considering the 0.3 mg<sub>Pt</sub> cm<sup>-2</sup> used at the anode). For the MEA fabricated with Pt/C at the cathode, this value is 372 W g<sub>Pt</sub><sup>-1</sup> (considering the 0.3 mg<sub>Pt</sub> cm<sup>-2</sup> used at the anode and the 0.6 mg<sub>Pt</sub> cm<sup>-2</sup> used at the cathode).

Concerning the open circuit potential, for Pt/C catalyst it is around 0.96 V, while for our Fe-N-C catalysts its value is about 140 mV lower, being around 0.82 V. This value well matches with the ORR onset potential of 0.83 V found by the SV test in RDE (see Table 4). In fact, the anodic overpotential is very low (usually lower than 10 mV), being the kinetics of HOR on Pt/C catalyst very fast [7,17].

It is difficult to compare the performance of Fe-N-C catalyst in this test with the results reported in the literature for similar NPMC due to the non-uniformity of the experimental conditions adopted by the different work groups. For instance, we can make a comparison with the best “state of the art”



results that are reported in Table 1 in Chapter 1. There we can see how the highest power density performance values obtained for NPMC as cathodic catalysts are as high as  $700 \text{ mW cm}^{-2}$ . It is important to consider that these values were obtained at  $80 - 90^\circ\text{C}$ , while our tests were performed at  $60^\circ\text{C}$ . However, lower performing PEMFC results (around  $150 \text{ mW cm}^{-2}$ ) more similar to the ones obtained with our Fe-N-C catalyst, can also be found in the literature [17, 136–139]. The structural properties of the catalyst such as surface area and porosity appear to play important roles in promoting effective mass transfer, especially at higher current densities [140].



**Figure 34.** Polarization (filled symbols) and power density curves (open symbols) of PEMFC prepared using commercial Pt/C ( $0.6 \text{ mg}_{\text{Pt}} \text{ cm}^{-2}$ ) and Fe-N-C ( $2.5 \text{ mg cm}^{-2}$ ) as cathode catalysts. Cell temperature  $60^\circ\text{C}$ . The anode catalyst was a commercial Pt/C. Pt loadings on anode was  $0.3 \text{ mg cm}^{-2}$ .

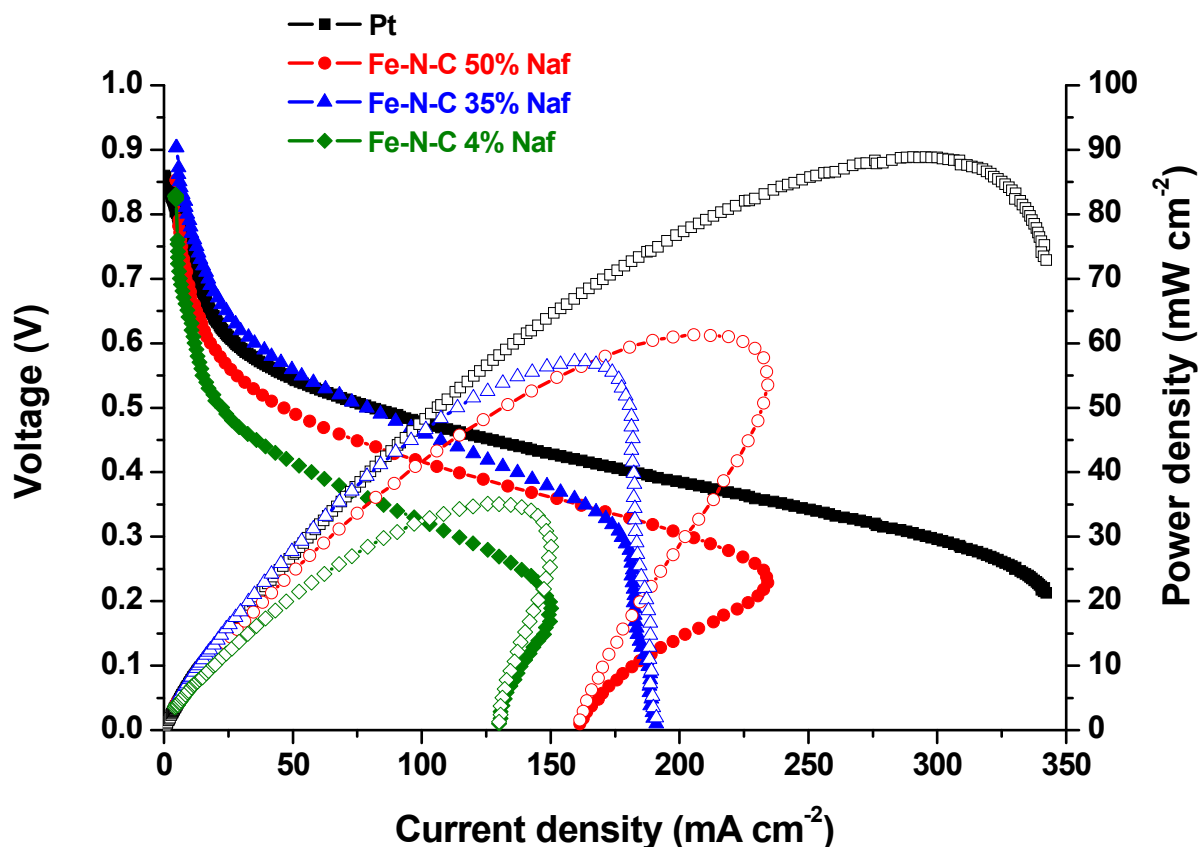
### 3.4.3. Alkaline DEFC test.

As the Fe-N-C catalyst exhibits very good activity toward ORR in alkaline conditions (see Paragraph 3.3), we performed a test in an AEMFC fueled with ethanol at the anode. To improve the cell performance, the anodic compartment must be fed with an alkaline pH solution. In particular, as mentioned in the experimental section, the solution fed at the DEFC anode was 2 M ethanol and 2 M KOH aqueous solution. As mentioned in the literature, if the ethanol is dissolved in a non-alkaline solution, the cell performance results to be considerably lower due to the ionic conductivity of the

ionomer is much lower than that of KOH solution. Therefore, providing an excess of  $\text{OH}^-$  ions in contact with the membrane helps to enhance the membrane conductivity and consequently, the reaction kinetics [141].

The results of the tests are shown in Figure 35, together with a comparative test on the same cell prepared with a standard Pt/C catalyst at the cathode. Three different cathodic layers were prepared, with different Nafion contents. Obviously, the Nafion ionomer used in the preparation of the catalytic layer of an AMEFC does not play the role of favor the ionic conductivity. However, it is commonly reported in the literature the use of a PTFE-based ionomer in the preparation of the electrodes for alkaline membrane fuel cells in wt. % on the dry electrode typically between 10 and 50% [141–144]. In the electrode, in fact, the presence of a binder is required to bind the catalyst particles together, and preserve them from progressive crumbling during the flushing of the reactants. Otherwise, without a binder, the cell performance will quickly degrade [141].

The performance of the alkaline DEFC prepared with the lower ionomer content (4 wt. %, the same used at the anode) was the worst. Increasing the Nafion content to 35 % the cell performances improve, becoming even better than for the cell with Pt/C catalyst at the cathode in the low current density region. The open circuit potential was also higher than for the Pt/C (0.90 vs 0.86 V). With a further increase of the Nafion content (50 wt. %), the performance of the cell in the low current region decreased. On the contrary, in the high currents region, the performances increased, allowing to get a maximum power density of  $62 \text{ mW cm}^{-2}$ . However, the shape of the polarization curve immediately after the maximum power density became convex, and the current density decreased with the decrease of the cell potential. This behavior suggest that the electrode was highly affected by mass transport problems, much more than in the case of 35 % Nafion content, where the polarization curve at low potentials shows a steep vertical decrease typical of the fuel cells affected by moderate-heavy mass transport limitations [132]. These mass transport limitations could be ascribed to the diffusion of the oxygen into the cathode catalyst layer, which could be hindered by the high ionomer content and by the highly microporous structure of the Fe-N-C catalyst. Similar results in terms of polarization curve shape and maximum power densities can be found in the literature for alkaline DEFC using different types of non-noble ORR electrocatalysts [143,144]. For the cell made with Pt/C catalyst these mass transport problems are much less evident, especially in the intermediate-high current density region. This characteristic of the Pt/C catalyst lead to obtain a considerably higher maximum power density (about  $90 \text{ mW cm}^{-2}$ ), in spite of almost the same  $E_{oc}$  (or even worse in the case of 35 % Nafion test).



**Figure 35.** Polarization (filled symbols) and power density (open symbols) curves for alkaline DEFC prepared using Fe-N-C as cathode catalyst with different Nafion contents in the catalytic layer. The curves for a DEFC prepared using a Pt/C commercial catalyst are also shown for comparison.

In these direct ethanol AEMFC tests, the crossover problems due to the diffusion of ethanol from anode to cathode are mitigated primarily by the lower permeability of the PBI membrane in comparison with Nafion membrane [14], and in addition by the  $\text{OH}^-$  transport direction, which is opposite than the alcohol diffusion through the membrane. This is confirmed by the remarkably high  $E_{\text{oc}}$  showed especially by the Pt/C catalyst. Therefore, the lower performances obtained by the Fe-N-C catalyst in comparison to Pt, can be mainly ascribed to its morphological-structural properties, which cause important mass transport and water removal problems (i.e. flooding).

#### 3.4.4. Concluding remarks about the fuel cell tests of Fe-N-C.

The importance of performing fuel cell test for the ORR catalysts has been clearly evidenced by the results presented in this chapter. In fact, the obtainment of good catalytic performances in RDE-RRDE tests in terms of  $E_{\text{on}}$ ,  $E_{1/2}$  and peroxide selectivity are not sufficient to define an ORR catalyst as “good” to be used to fabricate a polymer exchange membrane fuel cell stack. The “goodness” of the catalyst has to be validate by means of the obtainment of good performances in fuel cell test in terms of both activity and durability.

One of the main problems that have limited until now the use of the Me-N-C NPMC in these types of fuel cells are the mass transport problems. In particular, the catalysts fabricated with a hard templating method (i.e. using a silica as template) were found to be more affected by these problems, as well as those that show large particles or flake-like morphology. On the contrary, the catalysts synthesized starting from a carbon support with the addition of an external nitrogen and transition metal source, and the ones larger pore diameters and finest particle size usually exhibit better mass transport properties [17]. Our Fe-N-C catalyst belongs to the first group, and its structure is highly microporous (see Table 1). Moreover, as shown by the pore size distribution plot in Figure 2B, a big quantity of the micropores have a diameter between 0.6 and 0.9 nm, and between 1 and 2 nm. These values are almost 2 – 6 times the diameter of the water and oxygen molecules (about 0.3 nm) [145,146]. As demonstrated in previous studies [17,147], these are the dimensions where the majority of the ORR active sites in NPMC synthesized without a preexisting C support are hosted.

It is evident how, if these pores are becoming completely filled by the water due to the flooding phenomena, their accessibility to the ORR reactants, especially O<sub>2</sub>, becomes very difficult. Therefore, the dominant microporous structure of the support resulting in a serious water flooding, will lead to an irreversible damage of the cathode catalyst layer, as also reported in the literature [72,148].

In conclusion, from all the results obtained in this chapter, we got important indications and confirmations. Having a catalyst with a very high surface area and microporosity is essential to have a ORR electroactivity in RDE, especially in acidic conditions. In alkaline conditions, these properties have more influence on the selectivity toward a complete 4 e<sup>-</sup> oxygen reduction to water.

However, when operating in a polymer exchange membranes fuel cell, this high microporosity may result in serious mass transport and water flooding problems.

Therefore, the surface area, pore size distribution and microporosity properties of a Me-N-C electrocatalyst for ORR, have to be accurately tuned in order to obtain the better performances in fuel cell in terms of both activity and durability. This could be achieved during the catalyst synthesis operating on different parameters, such as the structure of template (in the case of hard templating synthesis method) [19,149], the use of expansion agents [17,150,151] or variables of the pyrolysis heat treatment (time, heating ramp speed, temperature, pressure, type of gas used).

#### 4. Conclusions.

Using Me(II)phthalocyanines (Me = Fe, Co, Cu, Zn) as single Me, C and N precursors, and SBA-15 silica as template, we produced a series of Me-N-C electrocatalysts for ORR with extremely high specific surface area and high microporosity.

The presence of the different transition metals ions coordinated with N atoms in the phthalocyanine macrocycle center influences the morphology, the chemical composition and the ORR behavior in terms of catalytic activity and selectivity towards a complete  $4\text{e}^-$   $\text{O}_2$  electroreduction to  $\text{H}_2\text{O}$ .

These properties are related with different trends of the weight loss and with the formation of gaseous products in different amounts and at different temperatures during the pyrolysis, as evidenced by the TGA-mass spectroscopy analysis.

Fe-N-C is the catalyst with higher activity and selectivity toward a complete  $4\text{e}^-$  ORR pathway. We speculate that this behavior in terms of weight loss and gaseous products during the pyrolysis is a key factor towards the synthesis of more active non-precious metal based catalysts.

However, further investigation is necessary with other catalysts precursors, in order to corroborate this hypothesis.

As evidenced by the electrochemical tests performed at different temperatures, the catalyst showing a higher activity, that is Fe-N-C, exhibits certain analogies with the standard Pt-based catalysts in acid conditions, in terms of activation energy values, and their variation with overpotential.

The performance of Fe-N-C catalyst in alkaline conditions is very close to Pt/C catalyst in terms of onset potential, and considerably better in terms of selectivity (almost null peroxide production), due to the good stabilization of the peroxide anion intermediate on the active site in alkaline conditions. These results underline the advantages in the use of such types of Fe-N-C catalysts for alkaline fuel cells applications.

The results of the tests of Fe-N-C catalyst in single fuel cell with both acidic (DMFC and  $\text{H}_2/\text{O}_2$ ) and alkaline (DEFC) membrane electrolyte evidenced how this catalyst, in spite of showing a good ORR activity, is highly affected by deactivation mainly ascribed to the flooding of the micropores, which could lead to irreversible loss of catalytic activity.

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## **CHAPTER 7. Fe-N-C electrocatalysts for oxygen reduction reaction derived from the impregnation of Fe – 1,10-phenanthroline complex on different carbon supports.**

### **1. Introduction.**

1,10-phenanthroline is a nitrogen-containing organic molecule which in water solution is capable to form complexes with Fe ion [1,2]. Due to the fact that they contain Fe, N and C, with nitrogen atoms coordinating the metal, these iron-phenanthroline complexes have been used as precursors for the synthesis of heat treated non-precious metal based Fe-N-C electrocatalysts for ORR since many years [3–5]. Recently, the use of Fe-phenanthroline complexes has aroused again the interest of researchers in the field of ORR catalysts alternative to Pt-based ones [6–9].

The importance of the different carbon support in getting a good ORR activity was underlined by several works [10–12].

In this work, four different carbon supports have been used for the impregnation of the Fe-phenanthroline complex.

1 – A mesoporous carbon (MPC) synthesized in our laboratory via a hard-templating method of a commercial mesoporous silica.

2 – A carbon (CNS) synthesized in our laboratory via a hard-templating method of a commercial silica nanopowder with homogeneous particle size of 12 nm.

3 – Commercial multi-walled carbon nanotubes (MWCNT).

4 – Commercial Shawinigan AB50 acetylene black (SHAW).

After impregnation with the Fe-phenanthroline complex, the four different samples were pyrolyzed in inert atmosphere at 800 °C. Their electroactivity toward ORR was tested in RDE in acidic and alkaline conditions. The catalyst synthesized starting from the MPC support was found to have the better activity in both acid and alkaline conditions. Therefore, to further improve its activity, it was submitted to a second pyrolysis at 800°C in inert atmosphere (in the same conditions used for the first heat treatment). In fact, performing a second heat treatment was found to have a positive influence in improving the ORR activity of such this type of Fe-N-C catalysts [4,13–15] as also demonstrated in Chapter 3 and Chapter 4.

The structural properties of the five catalysts were characterized by nitrogen physisorption analysis. An XPS analysis was performed to determine the surface elemental composition of the catalysts, particularly regarding the N and Fe contents.

Finally, the performances of the catalysts were tested in H<sub>2</sub> and methanol fueled PEMFC, and in an ethanol fueled alkaline membrane fuel cell.

## 2. Experimental.

### 2.1. Chemicals.

Commercial multi-walled carbon nanotubes (MWCNT, average length 5  $\mu$ m, outer diameter 6–9 nm, > 95% carbon) were purchased from Sigma-Aldrich. Shawinigan AB50 acetylene black (SHAW) was purchased from Chevron Phillips Chemical Company.

Silica mesoporous nanoparticles (200 nm particle size, 4 nm pore size) and silica nanopowder (12 nm primary particle size) were purchased by Sigma-Aldrich.

Hydrochloric acid (HCl, 37 wt. %), Sulfuric acid (H<sub>2</sub>SO<sub>4</sub>, 98 wt. %), Hydrofluoric acid (HF,  $\geq$  40 wt. %), Potassium Hydroxide (KOH, 99.0% purity), Sucrose ( $\geq$  99.0% purity), Ethanol ( $\geq$  99.8% purity), Acetone ( $\geq$  99.8% purity), Isopropanol ( $\geq$  99.7% purity), Nafion® 5 wt. % hydroalcoholic solution, 1,10-Phenanthroline C<sub>12</sub>H<sub>8</sub>N<sub>2</sub> (Phen,  $\geq$ 99 % purity), Iron(III) chloride (FeCl<sub>3</sub>,  $\geq$ 97 % purity) were purchased from Sigma-Aldrich. Nitrogen and oxygen gases were supplied in cylinders by SIAD with 99.999% purity. All aqueous solutions were prepared using ultrapure deionized water obtained from a Millipore Milli-Q system with resistivity  $>18 \text{ M}\Omega \text{ cm}^{-1}$ .

### 2.2. Synthesis.

#### 2.2.1. Synthesis of the MPC and CNS carbon supports.

MPC mesoporous carbon and CNS carbon were synthesized via hard templating method [16]. The templates used were the commercial silica mesoporous nanoparticles and the silica nanopowder, respectively. The synthesis method consists on impregnating the silica with a solution containing sucrose (used as the carbon source) and sulphuric acid. More in detail, a solution containing 10 mL of deionized water, 0.152 mL of H<sub>2</sub>SO<sub>4</sub> and 2.5 g of sucrose was pipetted drop by drop onto 2 g of silica. Then the temperature was increased at 100°C on a hot plate, and kept constant for 6 hours. Subsequently the temperature was increased to 160 °C and kept constant for 6 hours more. This two-steps heating procedure is repeated after pipetting drop by drop a solution containing 10 mL of deionized water, 0.098 mL of H<sub>2</sub>SO<sub>4</sub> and 1.6 g of sucrose. Then, after becoming completely dry, the carbon-silica mixture was heat-treated in a quartz-tube reactor at 830 °C for 6 hours under nitrogen atmosphere. To completely remove the silica template, the mixture was put in 110 mL of 5 % wt. HF

solution. Finally, the as obtained MPC and CNS were filtered under vacuum, washed with abundant deionized water and acetone, and dried in air.

#### 2.2.2. *Synthesis of the Fe-N/C catalysts.*

Before their use, all of the C-supports (MPC, CNS, MWCNT and SHAW) were washed with 1 M HCl solution for 3 h under stirring, filtered under vacuum, washed with abundant deionized water and dried at room temperature. Four different catalysts were obtained from these different C-supports, exactly following the same synthesis procedure, as described below.

Typically, for 120 mg of C-support, 130 mg of 1,10-phenanthroline (Phen) ligand molecule, used as a nitrogen source, was dissolved in 80 mL of ethanol – deionized water solution (70 mL ethanol + 10 mL deionized water), leaving under stirring until complete dissolution of Phen (about 2 h). Then, 35 mg of FeCl<sub>3</sub> was added to the solution, with the immediate formation of a reddish-orange complex (see Figure 1). According to these quantities, Fe:C-support mass ratio was set to 1:10, and the Fe:Phen molar ratio was of 1:3.35. Since each Fe ion coordinates with 3 Phen molecules [1,2], the slightly greater quantity of Phen used in the synthesis should assure a stoichiometric excess of ligand molecule to favor the chemical equilibrium of the Fe ion complexation. Moreover, this excess of Phen (and therefore of N atoms) may help to get a higher doping level of the C-support surface with N atoms, favoring the formation of active sites. The solution was left stirring at room temperature for 3 hours and afterwards the C-support was added to it. This dispersion was put in an ultrasonic bath for 30 minutes (130 W, Soltec 2200 M 3S sonicator) for allowing a better dispersion of the C-support. Then, it was left under stirring overnight and therefore the solvent was evaporated by heating on a hot plate, and the recovered powder was grinded in a mortar. Therefore, it was pyrolyzed in a tubular quartz furnace under nitrogen atmosphere (N<sub>2</sub> gas flux set at 150 N mL min<sup>-1</sup> with a mass flow controller from Bronkhorst, ELFLOW series) at 800 °C. The heating rate was set to 10 °C min<sup>-1</sup>. The temperature was kept constant for 1 hours at 800 °C, and then the furnace was switched-off leaving the apparatus cooling down naturally to room temperature. The 4 catalysts obtained from the different C-supports (SHAW, MWCNT, CNS and MPC) were named Fe-N/SHAW, Fe-N/MWCNT, Fe-N/CNS and Fe-N/MPC1, respectively. For the Fe-N/MPC1 catalyst, the pyrolysis was repeated one more time in the same conditions, starting again from room temperature, and the final catalyst was named Fe-N/MPC2.

Before testing, all of the catalysts were washed in 1 M HCl solution for 3 hours at 60 °C under reflux, to remove any instable or unbounded acid-soluble Fe, or Fe oxide moiety [13,17,18]. Afterwards the powders were filtered, washed with abundant deionized water until neutral pH, and dried overnight at room temperature.

### 2.3. Physico-chemical characterization.

#### 2.3.1. XPS analysis.

The X-ray photoelectron spectra (XPS) of the samples were acquired with a VG Escalab 200R spectrometer fitted with a Mg K $\alpha$  ( $h\nu = 1253.6$  eV) 120 W X-ray source. Samples were placed in a pretreatment chamber, and degassed at  $10^{-5}$  mbar at room temperature and for 1 hour prior to be transferred to the analysis chamber. Residual pressure was maintained below  $3.0 \cdot 10^{-8}$  mbar. The 50 eV energy regions of the photoelectrons of interest were scanned a number of times to obtain an acceptable signal-to-noise ratio. Intensities were estimated by calculating the integral of each peak, determined by subtraction of the Shirley-type background and fitting of the experimental curve to a combination of Lorentzian and Gaussian lines of variable proportions. Accurate binding energies ( $\pm 0.2$  eV) were determined by referencing to the C 1s peak at 284.6 eV [19].

#### 2.3.2. $N_2$ physisorption analysis.

Nitrogen adsorption and desorption isotherms were recorded by an ASAP 2020 Instrument (Micromeritics) at  $-196$  °C. Before being analyzed all of the samples were degassed at  $150$  °C under vacuum for 24 h. The specific surface areas were calculated by the Brunauer–Emmett–Teller (BET) method within the relative pressure range  $P/P^0 = 0.05 - 0.30$  [17]. The pore size distribution was obtained with the Barrett–Joyner–Halenda (BJH) method.

### 2.4. RDE tests.

The ORR activity of the Fe-N/C was preliminary checked in 3-electrode configuration in the RDE cell apparatus. The catalysts the ink was prepared by dispersing a given mass of catalyst in a solution containing known volumes of isopropanol, deionized water and a 5% wt. Nafion ionomer hydroalcoholic solution. The complete ink preparation procedure is described in Paragraph 2.4.1 of Chapter 6. The RDE cell was equipped with a glassy carbon disk working electrode (disk diameter 4 mm), a Pt helical wire counter electrode, and a saturated calomel reference electrode (SCE). For tests in acidic conditions the electrolyte was a 0.5 M H<sub>2</sub>SO<sub>4</sub> solution. For tests in alkaline conditions the electrolyte was a 0.1 M KOH solution. Prior to start tests, the electrolytes were saturated with pure N<sub>2</sub>, and 50 cyclic voltammetry (CV) cycles at  $100 \text{ mV s}^{-1}$  scan rate were performed in the potential window 0.0 - 1.2 V vs RHE, in order to obtain an electrochemically clean and stable working electrode surface. Afterwards, the solution was saturated with pure O<sub>2</sub> and the RDE rotation speed was set at 900 rpm. Then, staircase voltammetries were recorded with a potential step of 0.01 V and a holding time at each potential of 10 s. After this time, the background capacitive current had passed, and a steady-state value of the faradaic current was measured. In this way steady-state polarization curves can be obtained [14].

## 2.5. Single fuel cell tests.

### 2.5.1. Acid-DMFC test.

The performance of Fe-N/MWCNT, Fe-N/MPC1 and Fe-N/MPC2 as ORR cathodic catalyst was evaluated in a 4 cm<sup>2</sup> active area DMFC single cell. A commercial Nafion 117 membrane (Dupont) was used as electrolyte. Before use, the membrane was cleaned as described in Paragraph 2.5.1 of Chapter 6. A commercial Pt-Ru/C catalyst (Johnson Matthey, 30 wt% Pt-Ru, Pt:Ru 1:1 atomic ratio) was used as anodic catalyst. As a purpose of comparison, the performance of a DMFC using a commercial Pt/C catalyst (Johnson Matthey, 40 wt % Pt) at the cathode was also evaluated.

The electrodes were prepared by spraying the catalyst ink onto a Teflon-treated carbon cloth (ELAT GDL-LT 1200 W) gas diffusion layer (GDL) by means of an air-brush. The inks were prepared by mixing the catalysts powder with an isopropanol/deionized water solution (2:1 vol.) and a Nafion ionomer solution (5 wt. %) under sonication until getting a homogeneous suspension. The Nafion solution amount was calculated in order to have a 50 wt. % of Nafion in the dry catalytic layer. The total catalyst loading on the electrode was 2.5 mg cm<sup>-2</sup>. These Nafion content and catalyst loading were used because they were the optimum conditions found in Chapter 6. For preparing the Pt-Ru and Pt based electrodes, the Pt loading on the electrodes was set to 1 mg cm<sup>-2</sup>, with a Nafion content of 4 wt. %. For the MEAs preparation and for the DMFC tests, we used the same procedure described in Paragraph 2.5.1 of Chapter 6, at a cell constant temperature of 80 °C, with a methanol 2 M solution at a flow rate of 1 min<sup>-1</sup>.

A short-term durability test was performed for Fe-N/MPC2 catalyst. The test consisted of a 3 hours chronoamperometric experiment at 0.4 V conducted in the same operating conditions described in Chapter 6, with a flow rate of the methanol solution at the anode of 5 mL min<sup>-1</sup> [20]. A polarization curve is recorded regularly every 30 minutes, to evaluate the performance variation with time.

### 2.5.2. Acid H<sub>2</sub> / O<sub>2</sub> PEMFC test.

Fe-N/MWCNT and Fe-N/MPC2 catalysts were also tested in PEMFC using H<sub>2</sub> as fuel. The same 4 cm<sup>2</sup> active area single cell described in section 2.5.1 was used. In this case, a commercial Nafion 112 membrane (Dupont) was used as electrolyte. The testing was done in the same conditions described in Paragraph 2.5.2 of Chapter 6. The Nafion content on the dry electrode was 50 wt. % and the catalyst loading was 2.5 mg cm<sup>-2</sup>.



### 2.5.3. Alkaline DEFC test.

Fe-N/MPC2 catalyst was also tested as ORR catalyst in a direct ethanol fuel cell (DEFC) with an alkaline electrolyte membrane, in the same conditions described in Paragraph 2.5.3 of Chapter 6 concerning the MEA preparation and the fuel cell testing parameters.

The Fe-N/MPC2 cathodes were prepared with a Nafion content on the dry electrode of 50 wt. %, and with a catalyst loading of 2.5 mg cm<sup>2</sup>.

## 3. Results and discussion.

### 3.1. BET and pore size distribution analysis.

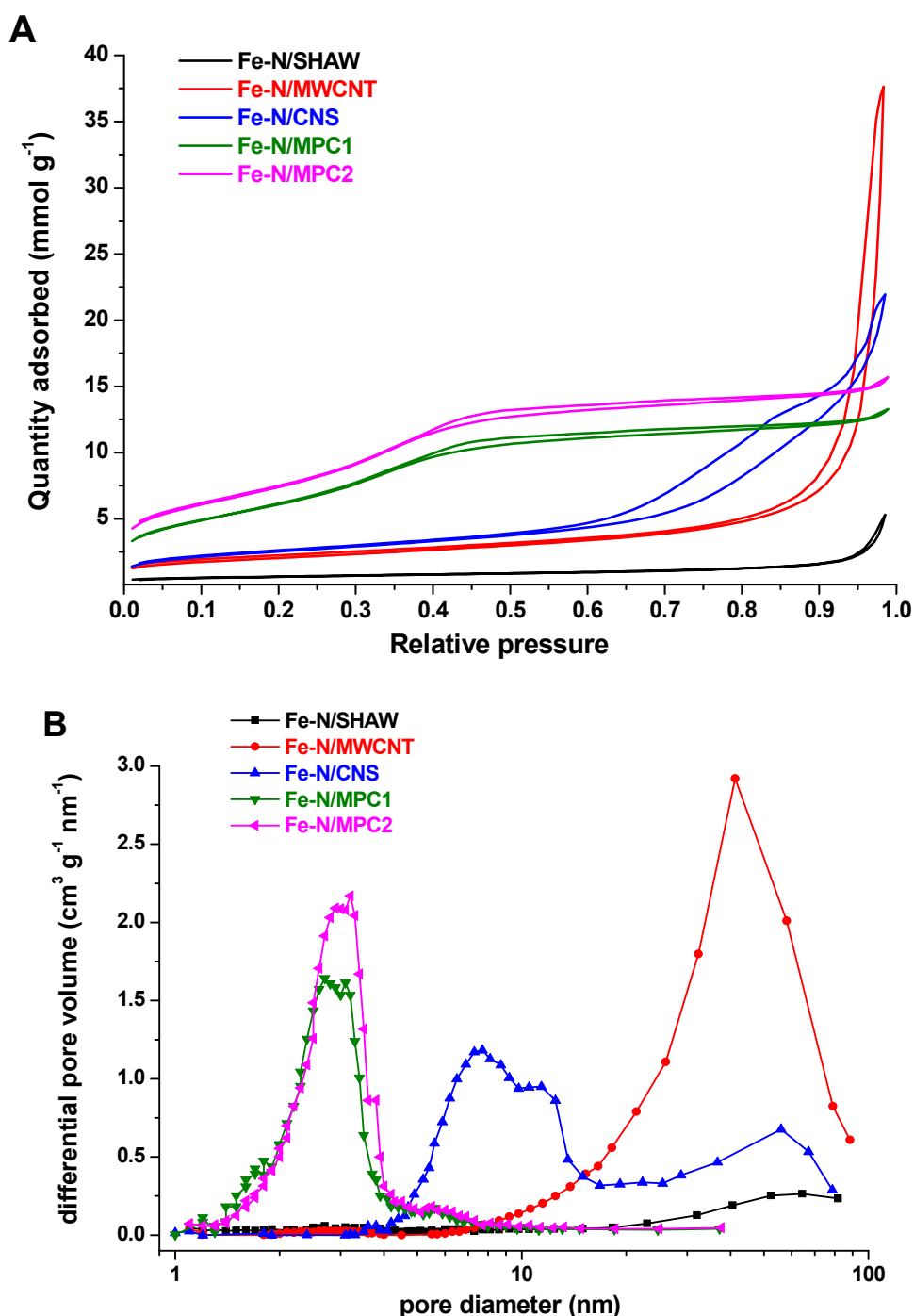
The nitrogen adsorption/desorption analysis was performed for all of the Fe-N/C catalysts. The adsorption-desorption isotherms and the BJH desorption pore-size distribution are shown in Figure 1A and 1B, respectively. The BET surface areas and the BJH total pore volume and average pore diameter are summarized in Table 1. As evident, the structure of the final catalyst strongly depends on the C-supports, which are very different from each other.

The Fe-N/SHAW and Fe-N/MWCNT catalysts have a strong macroporous character, as suggested by the shapes of their isotherms, belonging to type II – type III of the IUPAC classification [21,22]. At relative pressure values lower than 0.05, the shape of the isotherms suggest the presence of a low quantity of micropores [21,22]. For Fe-N/SHAW, almost no presence of hysteresis loop is observed. Otherwise, Fe-N/MWCNT exhibits a hysteresis loop with almost vertical adsorption and desorption branches, which are nearly parallel over an appreciable range of quantity of gas adsorbed. This hysteresis loop belongs to the H1-type of the IUPAC classification, which is typical of porous materials consisting of agglomerates [21], and can be associated with carbon nanotubes aggregated felt-like morphology [13,23].

The Fe-N/CNS isotherm shape is an intermediate between type II and type III, similarly to Fe-N/MWCNT, but with a less steep vertical increase at high relative pressures. A well-evident hysteresis loop is also present.

The Fe-N/MPC1 and Fe-N/MPC2 catalysts show identical isotherm shape, with the latter showing higher quantities of adsorbed N<sub>2</sub>, due to its higher surface area. The shape of the isotherms belongs to type IV, with the presence of type H4 hysteresis loop, which is typical of micro-mesoporous carbons. However, the hysteresis loop is not very big, indicating the presence of small width mesopores. In fact, the presence of a big hysteresis loop in type IV isotherms is usually associated with a pore width exceeding a certain critical width, which is dependent on the adsorption system and temperature (e.g., for nitrogen adsorption in cylindrical pores at 77 K, hysteresis starts to occur for

pores wider than  $\sim 4$  nm). As evident by the pore size distribution analysis in Figure 1B, the majority of the pores in the Fe-N/MPC1 and Fe-N/MPC2 catalysts are between 2 and 4 nm).



**Figure 1.** (A) N<sub>2</sub> adsorption – desorption isotherms and (B) BJH desorption pore-size distributions of the different Fe-N/C catalysts.

The results of the pore size distribution (Figure 1B) confirm the previous considerations. In fact, it is evident that the catalysts prepared using MWCNT and SHAW supports are mainly constituted by macropores and mesopores with diameter  $> 20$  nm. Fe-N/CNS catalyst exhibits the higher amount of

pores in the range of mesopores between 5 and 20 nm, having also a certain amounts of macropores. Otherwise, the catalysts supported on MPC mainly show mesopores between 2 and 4 nm width.

**Table 1.** Properties calculated from the nitrogen physisorption analysis of the different Fe-N/C catalysts and their respective C-supports materials. (\*) For SHAW the data are taken from reference [24]

| Sample     | BET surface area<br>[m <sup>2</sup> g <sup>-1</sup> ] | BJH total pore volume<br>[cm <sup>3</sup> g <sup>-1</sup> ] | BJH average pore diameter<br>[nm] |
|------------|---|---|-----------------------------------|
| SHAW*      | 80  | -   | -                                 |
| MWCNT      | 259   | 2.886   | 37.3                              |
| CNS        | 332   | -   | -                                 |
| MPC        | 865   | 0.827   | 3.3                               |
| Fe-N/SHAW  | 51  | 0.166   | 10.8                              |
| Fe-N/MWCNT | 165   | 1.287   | 31.1                              |
| Fe-N/CNS   | 208   | 0.752   | 11.7                              |
| Fe-N/MPC1  | 543   | 0.460   | 2.8                               |
| Fe-N/MPC2  | 645   | 0.549   | 2.9                               |

It is noteworthy that the surface area decrease for all of the Fe-N/C catalysts in comparison with their respective supports is almost the same. In fact, it is around 63 %, being 63.75 % - 63.71 % - 62.65 % - 62.77 % for Fe-N/SHAW, Fe-N/MWCNT, Fe-N/CNS and Fe-N/MPC1 respectively. This fact suggests that the Fe-Phen complex undergoes to a similar rate of incorporation on the C-support during the heat treatment, reducing the overall surface area, regardless of the type of C-support.

### 3.2. XPS analysis.

The XPS analysis was performed for all of the Fe-N/C catalysts after the final acid leaching in 1 M HCl, in order to determine overall surface chemical composition. The result are shown in Table 2. As expected, for all of the catalysts the main component is C, which is always detected in quantities higher than 90 atomic %. A not negligible amount of O was also detected in all of the samples. However, for Fe-N/MPC1 and Fe-N/CNS the amount of O was higher than in the other catalysts. This could be due to the not complete carbonization of the sucrose during the synthesis of MPC and CNS supports. For the Fe-N/MPC2 catalyst (that is, the Fe-N/MPC1 submitted to a second heat treatment at 800 °C in inert atmosphere), the O content was lower (3.1 at. %), suggesting that during the second heat treatment the surface of the catalyst undergoes to the loss of some oxidized functional groups. The O content in the catalysts synthesized using the commercial supports (MWCNT and SHAW) is lower.

The presence of oxygen could be also due to the incorporation of some of the O atoms of the silica templates during the CNS and MPC supports synthesis, due to the high temperatures reached during

the pyrolysis. Another reason could be the presence of some leaching in the sealing system of the tubular reactor used for the pyrolysis (in both supports and catalysts synthesis), from which atmospheric air could have entered, causing a partial oxidation of the carbonaceous material.

**Table 2.** Overall surface elemental composition of the different Fe-N/C catalysts determined by XPS analysis.

| Sample     | C [at. %] | O [at. %] | N [at. %] | Fe [at. %] | Tot [at. %] |
|------------|-----------|-----------|-----------|------------|-------------|
| Fe-N/SHAW  | 91.9      | 4.5       | 3.3       | 0.3        | 100         |
| Fe-N/MWCNT | 95.3      | 2.5       | 2.1       | 0.1        | 100         |
| Fe-N/CNS   | 91.8      | 5.2       | 2.8       | 0.2        | 100         |
| Fe-N/MPC1  | 92.6      | 5.3       | 1.8       | 0.3        | 100         |
| Fe-N/MPC2  | 95.1      | 3.1       | 1.5       | 0.3        | 100         |

A certain amount of N has been incorporated. The catalyst with the lower N content was the Fe-N/MPC2, which is the only catalyst heat treated twice. The decrease of N content detected by XPS after the second heat treatment in this types of metal-nitrogen-carbon catalysts was also found in Chapter 3 and 4. This could be associated with the release of N-containing gases, which in turn contributes to the increase of the surface area and pore volume after the second pyrolysis. Similarly, also the decrease of the O content, associated with the release of O-containing gas molecules, could contribute to the surface area increasing after the second pyrolysis.

For the catalysts heat treated once, the N at. % content varies from a minimum of 1.8 % for Fe-N/MPC1 to a maximum of 3.3 % for Fe-N/SHAW. Therefore, the overall N content is not related to the ORR electroactivity of the catalysts, as also found in Chapter 2, 3, 4 and 6, and as reported in the literature [25].

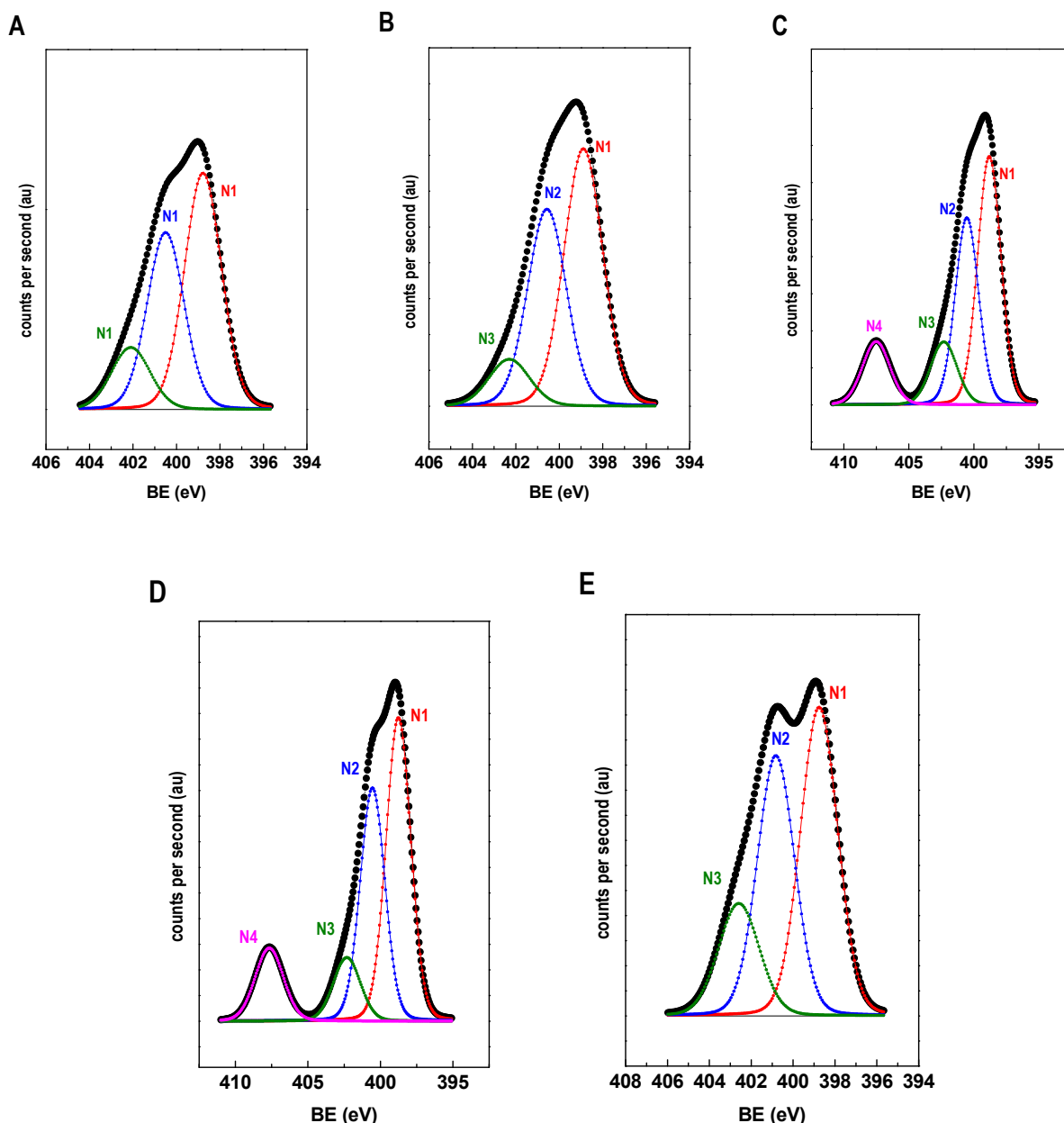
The high resolution N 1s peaks were analyzed by deconvolution. The four different components identified were pyridinic-N (N1) pyrrolic-N (N2), graphitic-N (N3) and oxidized-N (N4) [25–28]. The relative and total (referred to the overall nitrogen content of the sample, see Table 2) amounts of the different nitrogen bond types are shown in Table 3, with their respective binding energy.

In particular, the pyridinic-N type is the most abundant in all of the samples, ranging from 42 to 51 at. %. The pyrrolic-N is detected in percentages between 32 and 39 %, and the graphitic-N in lower amounts (10 – 17 %). In catalysts Fe-N/CNS and Fe-N/MPC1, a certain amount of oxidized-type N is also detected. This is in accordance to the fact that these two catalysts were also the ones where the higher amounts of O were detected. Therefore, part of the O in these catalysts should be bounded directly with N.

**Table 3.** Relative and total contents of the different N types with their respective peak binding energies resulting from the deconvolution of the high-resolution N 1s peak from XPS analysis (N1: pyridinic-N; N2: pyrrolic-N; N3: graphitic-N; N4: oxidized-N).

| <i>Binding energy [eV]</i><br><b>Relative content [atomic %]</b><br>Total content [atomic %] |                            |                            |                            |                            |
|--|----------------------------|----------------------------|----------------------------|----------------------------|
| Sample   | N1                         | N2                         | N3                         | N4                         |
| Fe-N/SHAW  | 398.8<br><b>49</b><br>1.62 | 400.5<br><b>37</b><br>1.22 | 402.1<br><b>14</b><br>0.46 | -<br>-<br>-                |
| Fe-N/MWCNT   | 398.9<br><b>51</b><br>1.07 | 400.6<br><b>39</b><br>0.82 | 402.3<br><b>10</b><br>0.21 | -<br>-<br>-                |
| Fe-N/CNS   | 398.8<br><b>42</b><br>1.18 | 400.5<br><b>32</b><br>0.90 | 402.3<br><b>12</b><br>0.34 | 407.5<br><b>14</b><br>0.39 |
| Fe-N/MPC1  | 398.8<br><b>44</b><br>0.79 | 400.5<br><b>34</b><br>0.61 | 402.3<br><b>10</b><br>0.18 | 407.7<br><b>12</b><br>0.22 |
| Fe-N/MPC2  | 398.7<br><b>45</b><br>0.68 | 400.7<br><b>38</b><br>0.57 | 402.5<br><b>17</b><br>0.25 | -<br>-<br>-                |

Trying to put in relation the different relative and total % of the different N-types with the ORR activity of the different catalysts, it is not possible to find out any direct relation. However, in many studies, the electrocatalytic activity towards ORR was attributed to pyridinic-N and pyrrolic-N [4,13,29,30]. Despite the real structure of the ORR active sites is still not clear and therefore under debate [31], many authors agree in the conclusions that the N atoms which are part of the active sites are located in the micropores [22]. Therefore, this explain the lack of existence of any direct correlation between the total or relative amount of the different N-types and the ORR activity for these catalysts. On the contrary, the electroactivity seems to be related with the surface area and the pore size distribution of the catalysts.

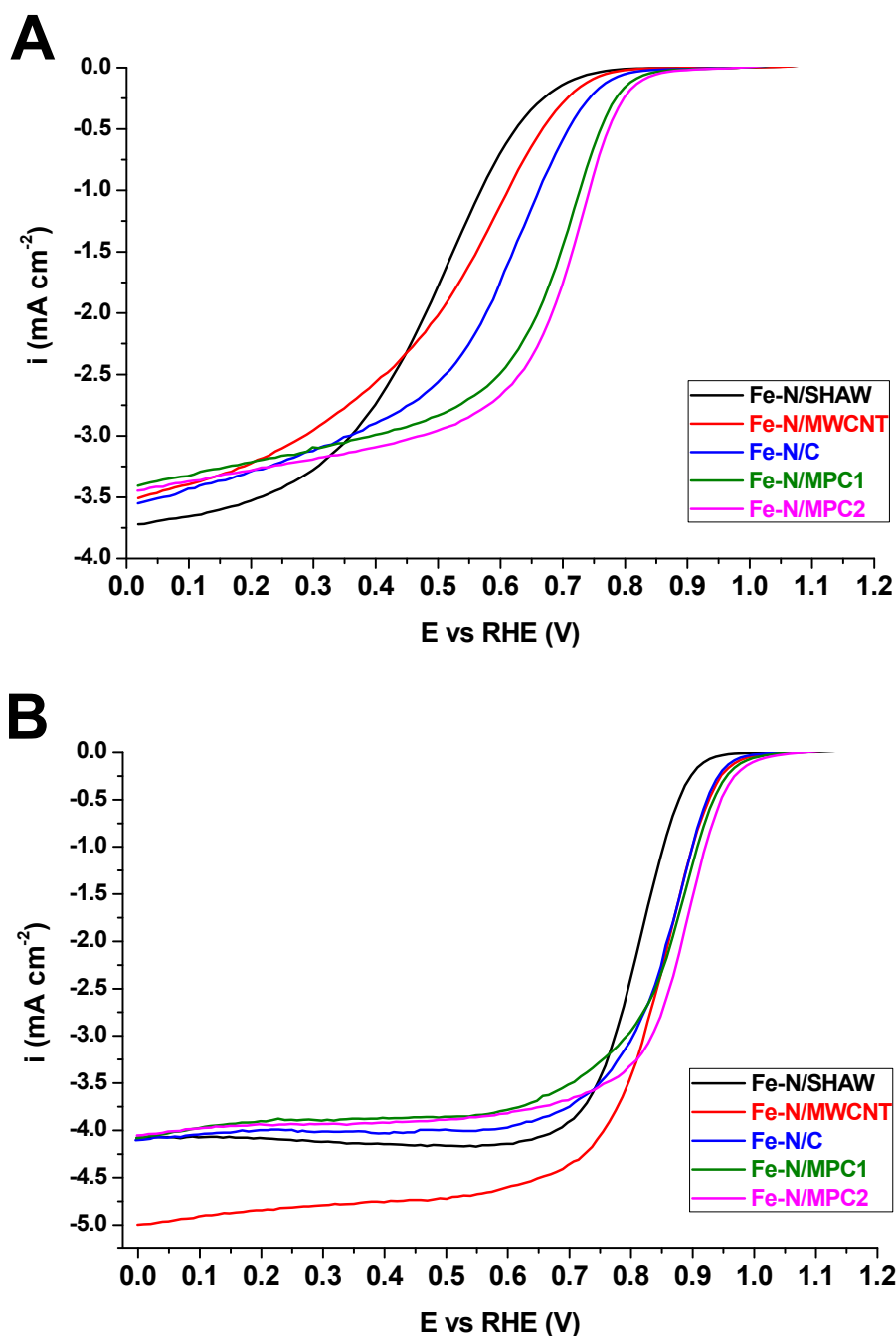


**Figure 2.** High resolution N 1s XPS spectra of the catalysts Fe-N/SHAW (A), Fe-N/MWCNT (B), Fe-N/CNS (C), Fe-N/MPC1 (D) and Fe-N/MPC2 (E) with the peak deconvolution analysis in the different N-bonding types. The black line is the overall N 1s peak. Red, blue, green and pink lines correspond to the deconvolution into pyridinic-N (N1), pyrrolic-N (N2), graphitic-N (N3) and oxidized-N (N4) peaks, respectively.

### 3.3. ORR electroactivity test in RDE.

The ORR activity of the five electrocatalysts was tested in both acidic and alkaline media by a RDE equipment, recording staircase voltammetries. The results are shown in Figure 3 A-B. The

performances of the different catalysts towards the ORR are summarized in Table 4 in terms of onset ( $E_{\text{on}}$ ) and half-wave ( $E_{1/2}$ ) potentials.  $E_{\text{on}}$  is defined as the potential required to generate a current density of  $0.1 \text{ mA cm}^{-2}$  in a steady-state RDE experiment [33] and  $E_{1/2}$  is the potential required to get half the maximum current density in the polarization curve.



**Figure 3.** Staircase voltammetries (10 mV potential step, 10 s holding time) of the different Fe-N/C catalysts recorded in RDE at 900 rpm rotation speed in  $\text{O}_2$ -saturated electrolyte: (A)  $0.5 \text{ M H}_2\text{SO}_4$  and (B)  $0.1 \text{ M KOH}$ .

In acidic medium, the activities of the catalysts pyrolyzed once are considerably different from one another. The most active is Fe-N/MPC1. It shows 100 mV higher  $E_{\text{on}}$  and 190 mV higher  $E_{1/2}$  in

comparison with the less active catalyst, that is Fe-N/SHAW. Considering that all of the catalysts were synthesized exactly in the same way, it is evident how the C-support plays a crucial role in the final ORR electroactivity. The use of a micro-mesoporous C-support, with a high specific surface area, seems to be useful to allow the formation of a higher number of active sites and to favor their accessibility to the reactants.

Concerning the effect of the second pyrolysis, comparing Fe-N/MPC1 and Fe-N/MPC2, a slight increase of 10 mV in  $E_{on}$  and of 20 mV in  $E_{1/2}$  was obtained. Probably mainly due to the increase of the catalysts surface area.

**Table 4.** Onset potentials ( $E_{on}$ ) and Half-wave potentials ( $E_{1/2}$ ) of the Fe-N/C catalysts in acid and alkaline conditions.

| Sample     | 0.5 M H <sub>2</sub> SO <sub>4</sub> |                      | 0.1 M KOH           |                      |
|------------|--------------------------------------|----------------------|---------------------|----------------------|
|            | $E_{on}$ [V vs RHE]                  | $E_{1/2}$ [V vs RHE] | $E_{on}$ [V vs RHE] | $E_{1/2}$ [V vs RHE] |
| Fe-N/SHAW  | 0.71                                 | 0.49                 | 0.92                | 0.81                 |
| Fe-N/MWCNT | 0.74                                 | 0.53                 | 0.97                | 0.84                 |
| Fe-N/CNS   | 0.77                                 | 0.60                 | 0.96                | 0.85                 |
| Fe-N/MPC1  | 0.81                                 | 0.68                 | 0.98                | 0.86                 |
| Fe-N/MPC2  | 0.82                                 | 0.70                 | 1.00                | 0.88                 |

The catalysts exhibit a much higher ORR activity in alkaline conditions than in acid conditions. In particular the onset potentials are almost 200 mV higher. This is typical for this type of transition metal-N-C catalysts.

In alkaline conditions, the differences in the catalysts electroactivities are less evident. Fe-N-/MWCNT, Fe-N/CNS and Fe-N/MPC1 exhibit practically the same activity, being their  $E_{on}$  and  $E_{1/2}$  only 10 mV different from each other. Fe-N/MWCNT catalyst shows a higher diffusion-limited current density. This could be due to the higher macroporous character of this catalysts. Its average pore diameter in fact is considerably higher than for the other catalysts, and this could favor the mass transport, allowing to get higher current density values in the mass-transport limited zone of the polarization curve. Another reason could be the fact that the Fe-N/MWCNT catalyst deposition on the RDE surface was less homogeneous, resulting in the formation of some agglomerates. This could locally enhance the turbulence in proximity of the RDE surface, increasing the mass transport of the O<sub>2</sub> and resulting in a higher limiting current value [34].

Fe-N/SHAW is the catalyst which shows the lower activity also in alkaline conditions.

The effect of the second pyrolysis on the ORR activity in alkaline conditions is similar than in acidic condition, that is, a slight increase of 20 mV in  $E_{on}$  and  $E_{1/2}$  was obtained.



The less evident differences between the activities of the different catalysts in alkaline conditions are probably partially due to the intrinsic ORR catalytic activity of the carbonaceous and nitrogen-doped carbonaceous materials, which promotes the  $2\text{e}^-$  reduction of  $\text{O}_2$  to  $\text{HO}_2^-$  in alkaline medium [35].

As described in Chapter 6, another reason could be ascribed to the fact that ORR partially occurs by the “outer-sphere” mechanism, which is promoted by the presence of the carbon support in alkaline conditions (i.e. by mediation by the quinone/hydroquinone surface functional groups).

These effects “mitigate” the differences between the activities of the different catalysts, which are more evident in acid medium.

However, to better complete these considerations, performing both a RRDE test and a  $\text{H}_2\text{O}_2$  reduction test for the different catalysts in both acid and alkaline conditions is necessary.

The performances of the best catalysts (Fe-N/MPC1 and Fe-N/MPC2) are equal to the ones of a Pt/C commercial catalyst (see Table 8 in Chapter 6), making their use in the cathode catalytic layer of an AEMFC very interesting.

### 3.4. Fuel cell tests.

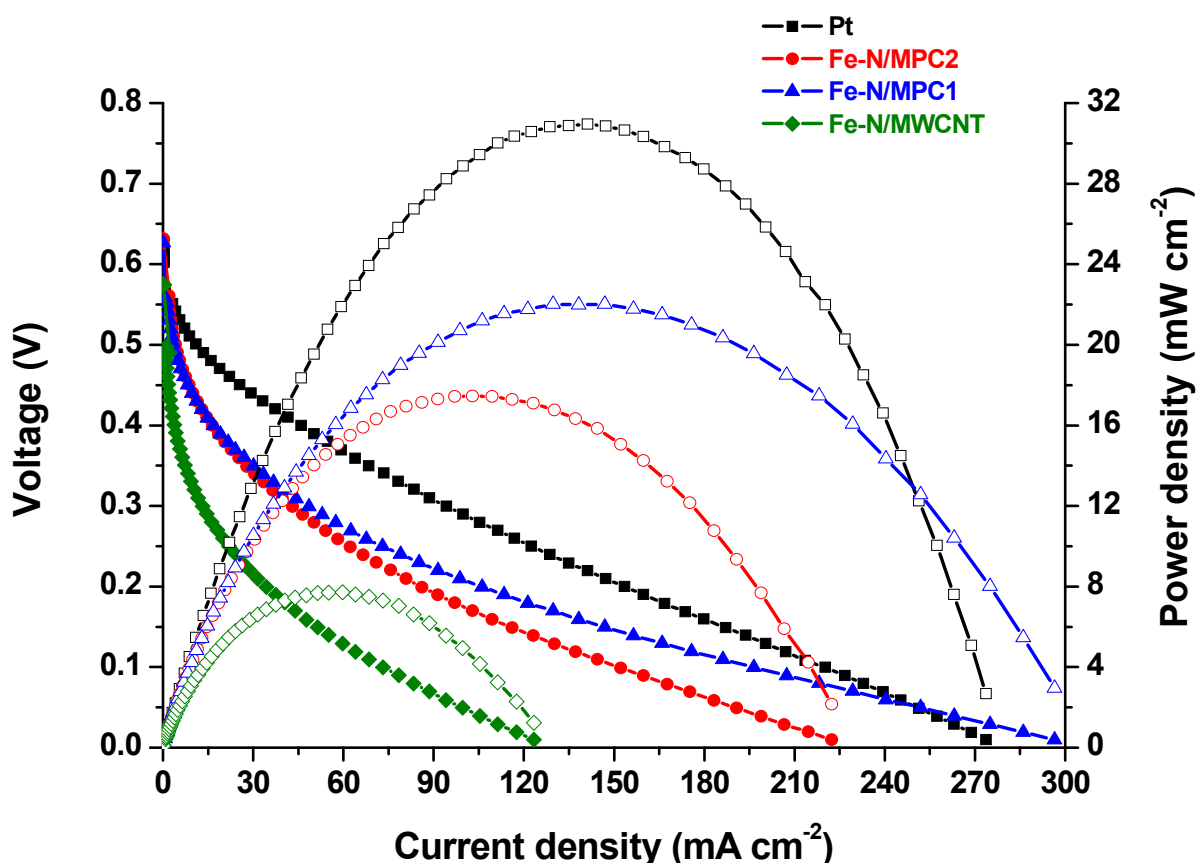
To better put in evidence the differences between the different C-supports on the characteristics of the final catalyst form a more applicative point of view, the performance of the different Fe-N/C catalysts were evaluated in different types of fuel cells. In acidic conditions, that is in a fuel cell equipped with a proton conducting membrane, we performed the test using both hydrogen and methanol as fuels. In alkaline conditions, that is, in a fuel cell equipped with an  $\text{OH}^-$  conducting membrane, ethanol was used as a fuel.

#### 3.4.1. Acid DMFC test.

The performance of Fe-N/MWCNT, Fe-N/MPC1 and Fe-N/MPC2 were tested in a DMFC. The cathodes were prepared with a catalyst loading of  $2.5\text{ mg cm}^{-2}$  and a Nafion content of 50 wt. %. The cell temperature was set to  $90^\circ\text{C}$ . The anode of the cell was fed with a 2 M methanol solution with a flow rate of  $1\text{ mL min}^{-1}$  and a backpressure of 0.33 bar. The cathodic compartment was fed with a  $200\text{ NmL min}^{-1}$  pure  $\text{O}_2$  flow preheated at  $80^\circ\text{C}$  with no humidification and a backpressure of 3 bar. The polarization curves and power density curves are shown in Figure 4, in comparison with the curves obtained for a DMFC prepared with a commercial Pt/C catalyst at the cathode (the same shown in Chapter 6). The main performance parameters are summarized in Table 5.

The most performing results in terms of power density were obtained with the Pt/C catalyst. Regarding our catalysts, unlike expected, the Fe-N/MPC1 catalyst was more performing than Fe-N/MPC2, which exhibited better performances in RDE. Considering the  $E_{\text{oc}}$ , the values of our catalysts were almost the same of the Pt/C. However, in RDE the  $E_{\text{on}}$  for ORR of Pt/C catalyst was

considerably higher than for our non-noble catalysts. This is due to the detrimental effects of methanol crossover, resulting in the presence of a mixed potential at the cathode of the DMFC, causing an important performance decrease. The most performing NPMC, that is Fe-N/MPC1, shows a maximum power density that is about 2/3 than for Pt/C. The Fe-N/MWCNT catalysts have a considerably lower performance, confirming the results of RDE test. This is probably due to its lower surface area and lower micropores content, which may result in a formation of a lower number of active sites. As future work, in order to complete the characterization, also the Fe-N/CNS and Fe-N/SHAW catalysts will be tested.



**Figure 4.** DMFC performances of Fe-N/MWCNT, Fe-N/MPC1 and Fe-N/MPC2 catalysts at 90 °C. The curve for a commercial Pt/C catalyst is shown for comparison. Polarization curves (open symbols) and power density curves (closed symbols).

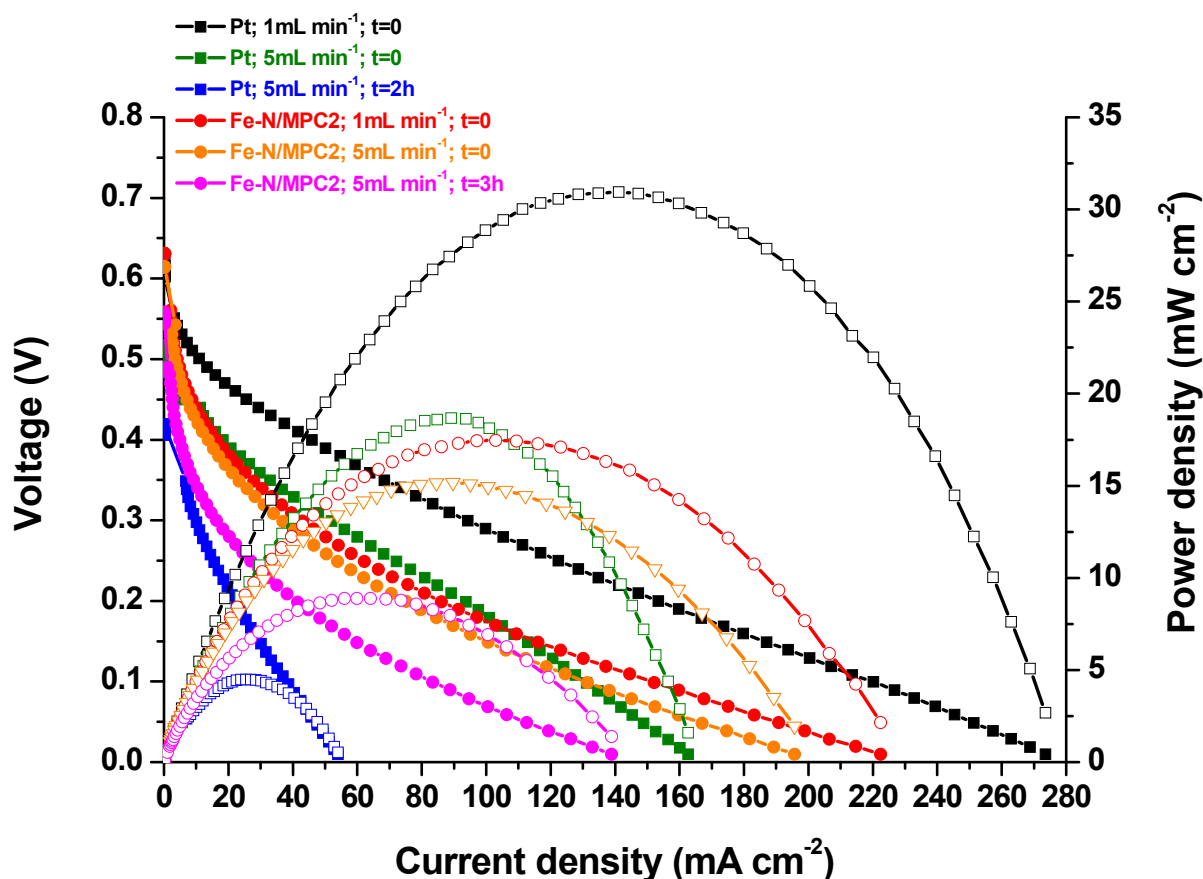
Therefore, the overall performance of our NPMC catalysts was lower than the one of Pt/C. Nevertheless, if we refer the maximum power density to the total Pt amount used to fabricate the MEA (see P max per g of Pt in Table 5), we get that using the Fe-N/MPC1 and Fe-N/MPC2 catalysts at the DMFC cathode we obtain better performance than with the Pt/C catalyst.

**Table 5.** Performance parameters for DMFC tests in Figure 4 (for Fe-N-MWCNT, Fe-N/MPC1, Fe-N/MPC2 and Pt/C) and for DMFC short-term durability test in Figure 5 (for Fe-N/MPC2 and Pt/C).

| Cathode catalyst | MeOH flow [mL min <sup>-1</sup> ] | time [h] | E <sub>oc</sub> [V] | i <sub>max</sub> [mA cm <sup>-2</sup> ] | P <sub>max</sub> [mW cm <sup>-2</sup> ] | P <sub>max</sub> per g of Pt [W g <sub>Pt</sub> <sup>-1</sup> ] | P <sub>max</sub> decrease [%] |
|------------------|-----------------------------------|----------|---------------------|---|---|---|-------------------------------|
| Fe-N/MWCNT       | 1                                 | 0        | 0.57                | 123                                     | 7.7                                     | 7.7   | -                             |
| Fe-N/MPC1        | 1                                 | 0        | 0.63                | 297                                     | 22.0                                    | 22.0  | -                             |
| Fe-N/MPC2        | 1                                 | 0        | 0.63                | 222                                     | 17.5                                    | 17.5  | -                             |
| Fe-N/MPC2        | 5                                 | 0        | 0.61                | 196                                     | 15.2                                    | 15.2  | 13.2                          |
| Fe-N/MPC2        | 5                                 | 3        | 0.56                | 139                                     | 8.9                                     | 8.9   | 49.2                          |
| Pt/C             | 1                                 | 0        | 0.62                | 274                                     | 30.9                                    | 15.5  | -                             |
| Pt/C             | 5                                 | 0        | 0.52                | 163                                     | 18.7                                    | 9.4   | 39.5                          |
| Pt/C             | 5                                 | 2        | 0.42                | 54                                      | 4.5                                     | 2.3   | 85.5                          |

A short-term durability test was performed on the DMFC containing the MEA prepared with Fe-N/MPC2 catalyst on the cathode. The durability test was performed for this catalyst because it was the one that showed better ORR activity in RDE. The same test for Fe-N/MPC1 catalyst, which has a better performance in DMFC has not been performed yet at the moment of the writing of this chapter, but it is going to be performed.

The short-term durability test was the same described in Chapter 6. Figure 5 shows the polarization and power density curves of the Fe-N/MPC2 catalyst at the beginning of the test ( $t = 0$ ) with a methanol flow rate of 1 and 5 mL min<sup>-1</sup>, and at the end of the test ( $t = 3$ h) with a flow rate of 5 mL min<sup>-1</sup>. The polarization and power density curves obtained for a Pt/C catalyst (in this case the test duration was 2 hours) are also shown for comparison. The performance parameters are also summarized in Table 5.



**Figure 5.** Comparison between the performances at 90 °C of the DMFC prepared with Fe-N/MPC2 and with commercial Pt/C as cathode catalysts at the beginning and at the end of the durability test (potential kept constant at 0.4 V for 3 h) with 5 mL min<sup>-1</sup> methanol flow. The polarization curves with 1 mL min<sup>-1</sup> methanol flow are also shown for comparison.

For the Pt/C catalyst, the cell performance suffers a remarkable decrease simply by increasing the flow rate. The  $E_{oc}$  immediately decreased by 90 mV and the maximum power density by 39.5 % from its initial value. Then, after 2 hours test, the maximum power density decreased by 85.5 % and the  $E_{oc}$  further decreased of 100 mV.

The use of a higher flow rate, should lead to an increase of the kinetics due to a higher flux of reactants to the anodic compartment [36]. However, at the same time, this also causes an increase of the water and methanol diffusion through the membrane, enhancing the methanol crossover detrimental effects on Pt/C cathodic catalyst.

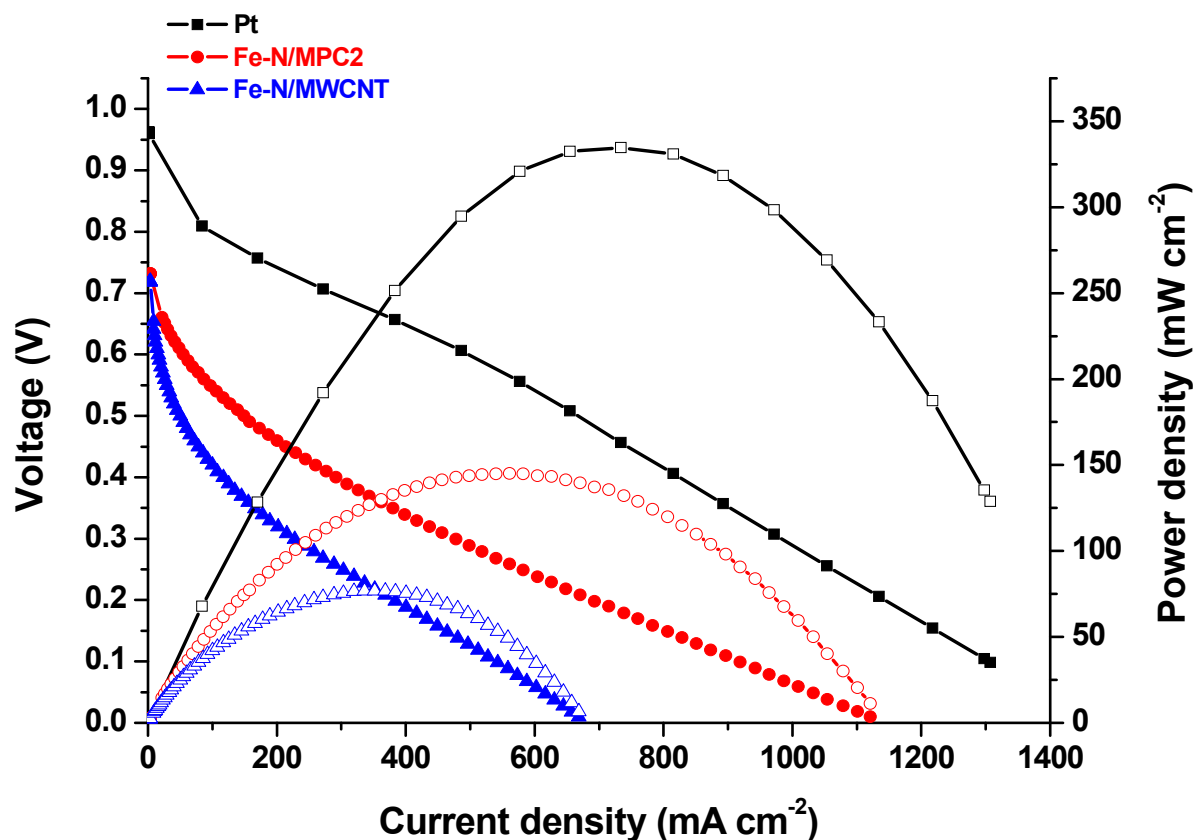
For Fe-N/MPC2 catalyst, this negative effect of the methanol flow rate increase are much less evident. In fact, the  $E_{oc}$  only suffered a 20 mV decrease and the maximum power density only decreased by 13.2 % in comparison with the test at 1 mL min<sup>-1</sup>. After 3 h test, the cell performance only decreased by 49.2 %, being the maximum power density the double than the one of the Pt/C catalyst after only 2 hours of test. If we refer the maximum power density to the total amount of Pt in the MEA, the

performance of the Fe-N/MPC2 catalyst after 3 hours test is almost 4 times higher than that of Pt/C after 2 hours test (8.9 against 2.3 W g<sub>Pt</sub><sup>-1</sup>). These results put in evidence the advantage of using this type of non-Pt based electrocatalysts for ORR in DMFC. In addition to their lower cost, they show a considerably higher stability and tolerance to the methanol crossover. Therefore, they can represent a good alternative to Pt-based catalysts, which, due to their low methanol tolerance, have been until now one of the biggest impediments to the wide commercialization of DMFC powered devices [37,38]. However, their electroactivity and mass transport properties (such as flooding resistance) have to be furtherly improved.

#### 3.4.2. Acid H<sub>2</sub> / O<sub>2</sub> PEMFC test.

The performances of Fe-N/MPC2 and Fe-N/MWCNT catalysts were tested in a PEMFC fed with pure H<sub>2</sub> and O<sub>2</sub> at anode and cathode, respectively, both with a backpressure of 3 bar(g) and preheated at 80 °C. H<sub>2</sub> flow was fed with 100% relative humidity, while O<sub>2</sub> was fed without humidification. The temperature of the cell was kept at 60 °C during the experiments. The polarization and power density curves results are shown in Figure 6, together with the results obtained in the same conditions but with a commercial Pt/C catalyst at the cathode.

The maximum power density for Fe-N/MPC2 was 145 mW cm<sup>-2</sup>, which is about 43 % of the maximum power density obtained with the Pt/C catalyst (335 mW cm<sup>-2</sup>). With Fe-N/MWCNT the cell performance is considerably lower, being almost ½ than for Fe-N/MPC2, in spite of showing practically the same E<sub>oc</sub>. This trend of results is very close to what obtained in the DMFC tests.



**Figure 6.** Polarization (filled symbols) and power density curves (open symbols) of PEMFC prepared using commercial Pt/C ( $0.6 \text{ mg}_{\text{Pt}} \text{ cm}^{-2}$ ), Fe-N/MPC2 ( $2.5 \text{ mg cm}^{-2}$ ) and Fe-N/MWCNT ( $2.5 \text{ mg cm}^{-2}$ ) as cathode catalysts. Cell temperature  $60^\circ \text{C}$ . The anode catalyst was a commercial Pt/C. Pt loadings on anode was  $0.3 \text{ mg cm}^{-2}$ .

As shown in Table 6, if we refer the maximum power density to the total mass of Pt used for the MEA fabrication, with Fe-N/MPC2 catalyst at the cathode we obtain  $483.3 \text{ W g}_{\text{Pt}}^{-1}$  (considering the  $0.3 \text{ mg}_{\text{Pt}} \text{ cm}^{-2}$  used at the anode). For the MEA fabricated with Pt/C at the cathode, we obtain a lower value of  $371.8 \text{ W g}_{\text{Pt}}^{-1}$  (considering the  $0.3 \text{ mg}_{\text{Pt}} \text{ cm}^{-2}$  used at the anode and the  $0.6 \text{ mg}_{\text{Pt}} \text{ cm}^{-2}$  used at the cathode). Concerning the open circuit potential, for Pt/C catalyst it is around  $0.96 \text{ V}$ , while for our catalysts its value is about  $230 \text{ mV}$  lower. This is the main cause of the lower fuel cell performance of our catalysts in comparison to Pt, being the kinetics of oxygen electroreduction on Pt in acidic conditions much faster, as also found in the RDE experiments.

**Table 6.** Performance parameters for PEMFC tests in Figure 6.

| Cathode catalyst | $E_{\text{oc}} [\text{V}]$ | $i_{\text{max}} [\text{mA cm}^{-2}]$ | $P_{\text{max}} [\text{mW cm}^{-2}]$ | $P_{\text{max per g of Pt}} [\text{W g}_{\text{Pt}}^{-1}]$ |
|------------------|----------------------------|--------------------------------------|--------------------------------------|--|
| Fe-N/MWCNT       | 0.72                       | 669                                  | 76.8                                 | 256.0  |
| Fe-N/MPC2        | 0.73                       | 1120                                 | 145.0                                | 483.3  |
| Pt/C             | 0.96                       | 1307                                 | 334.6                                | 371.8  |

The H<sub>2</sub> / O<sub>2</sub> PEMFC test needs to be completed with the test of the other three catalysts of the series, (Fe-N/MPC1, Fe-N/CNS and Fe-N/SHAW) in order to better understand the influence of the catalyst structure, which for these catalysts is mainly provided by the C-support, on their performance in PEMFC.

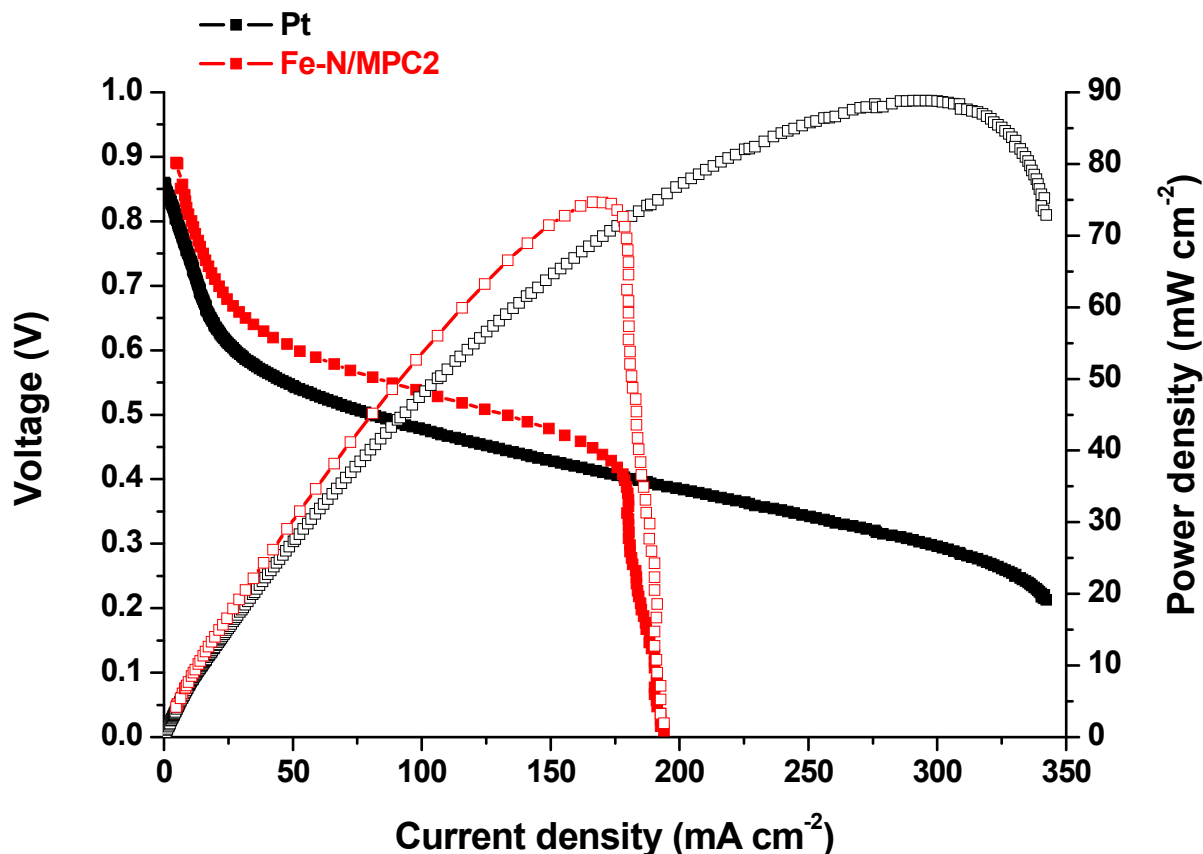
#### 3.4.3. Alkaline DEFC test.

The performance of Fe-N/MPC2 as ORR catalyst were also tested in an alkaline DEFC fed with a 2 M methanol – 2 M KOH solution preheated at 80 °C with a flow rate of 1 mL min<sup>-1</sup> and a backpressure of 0.33 bar. KOH was added to the ethanol solution to provide an excess of OH<sup>-</sup> ions in contact with the membrane. This helps to enhance both the membrane conductivity and the reaction kinetics [39]. At the DEFC cathode, a flux of 200 NmL min<sup>-1</sup> of pure O<sub>2</sub> was fed with 3 bar backpressure. The temperature of the cell was kept constant at 90 °C during the experiments.

The Fe-N/MPC2 cathode was prepared with a 2.5 mg cm<sup>-2</sup> catalyst loading, and a Nafion content on the dry electrode of 50 wt. %. The polarization and power density curves resulting from this test, together with the results of the same test on a DEFC with a Pt/C commercial catalyst at the cathode, are shown in Figure 7.

The performance of the alkaline DEFC prepared with the Fe-N/MPC2 cathode is better than the one of the Pt/C cathode in the low current density region, until about 200 mA cm<sup>-2</sup>. The E<sub>oc</sub> is also better, being 30 mV higher.

On the contrary, for current densities higher than 200 mA cm<sup>-2</sup>, the cell performances decreased very rapidly. Immediately after the attainment of the maximum power density, the polarization curve steeply decreases. This behavior suggest that the electrode was highly affected by mass transport problems [40]. These mass transport limitations could be ascribed to the diffusion of the oxygen into the cathode catalyst layer, which could be hindered by the high ionomer content and by the microporous structure of the catalyst.



**Figure 7.** Comparison between the polarization (filled symbols) and power density (open symbols) curves obtained for alkaline DEFCs prepared using Fe-N/MPC2 and a commercial Pt/C as cathode catalyst.

These results, in terms of power density and polarization curve shape are similar to the state-of-the-art that can be found in the literature for alkaline membrane DEFC with the use of NPMC at the cathode [41,42].

To complete the tests, and therefore fully understand the influence of the C-support in the real performance of this series of catalysts in alkaline DEFC, the other 4 catalysts of the series have to be tested.

Also in this case, as previously found for H<sub>2</sub> / O<sub>2</sub> PEMFC and DEFC tests in acidic conditions, referring the maximum power density to the total mass of Pt used for the MEA fabrication, the performance of Fe-N/MPC2 catalyst are better than the performance of the Pt/C catalyst. With Fe-N/MPC2 catalyst at the cathode we obtain 56.2 W g<sub>Pt</sub><sup>-1</sup> (considering the 1.33 mg<sub>Pt</sub> cm<sup>-2</sup> used at the anode). For the MEA fabricated with the commercial Pt/C catalyst at the cathode, we obtain 38.2 W g<sub>Pt</sub><sup>-1</sup> (considering 1.33 mg<sub>Pt</sub> cm<sup>-2</sup> at the anode and 1 mg<sub>Pt</sub> cm<sup>-2</sup> at the cathode).



**Table 8.** Performance parameters for PEMFC tests in Figure 6.

| Cathode catalyst | E <sub>oc</sub> [V] | i <sub>max</sub><br>[mA cm <sup>-2</sup> ] | P <sub>max</sub><br>[mW cm <sup>-2</sup> ] | P <sub>max</sub> per g of Pt<br>[W g <sub>Pt</sub> <sup>-1</sup> ] |
|------------------|---------------------|--|--|--|
| Fe-N/MPC2        | 0.89                | 193  | 74.7                                       | 56.2   |
| Pt/C             | 0.86                | 342  | 88.9                                       | 38.2   |

The performance of Fe-N/MPC2 catalyst, especially at low current densities, are very promising. However, they could likely be improved by performing an optimization of the electrode ink formulation, regarding the ionomer content and the catalyst loading. Moreover, the type of ionomer to be used instead of Nafion, i.e. an OH<sup>-</sup> conducting ionomer, preferably of the same type or at least compatible with the material of the electrolyte membrane [39].

### 3.5. Conclusions.

From the results obtained in this work, we can conclude that:

- The synthesis method we used, consisting in wet impregnation of the Fe – 1,10-phenanthroline complex on the C-support, drying and pyrolysis at 800 °C is effective in producing active ORR electrocatalysts.
- The C-support is essential to reach better ORR activity, especially in acid conditions. This means that the support morphology and structural features like the surface area and pore size distribution are key parameters in order to synthesize more active catalysts, regardless of the synthesis process.
- The previous point is much more important in acid than in alkaline conditions. In fact, at low pH, due to the slower kinetics of ORR, the distribution and accessibility of the active sites are much more important and limiting factors. This was confirmed not only by the polarization curves recorded in RDE in 0.5 M H<sub>2</sub>SO<sub>4</sub> solution, but also by the tests conducted in a single fuel cell equipped with an acidic electrolyte membrane (see Figure 4 for DMFC and Figure 6 for H<sub>2</sub> / O<sub>2</sub> PEMFC tests, respectively).
- In alkaline conditions, the enhanced ORR kinetics caused by the intrinsic properties of the carbonaceous and N-doped carbon-based materials, makes the influence of the C-support on the final ORR activity less evident.

These results evidenced how the choice of a good C-support is a much stricter parameter in the catalyst design for a fuel cell equipped with an acidic membrane than for a fuel cell equipped with an alkaline one. In acid membrane fuel cells, much care has to be put in the choice of an adequate C-support. If one only cares about the cost reduction, choosing for example a carbon black support (like SHAW), the risk of producing a catalyst with a too poor final ORR catalytic activity is high. Therefore, much attention has to be paid also in the synthesis of the C-support, i.e. using a silica template like a mesoporous silica in order to obtain the final desired structural features. Otherwise, in

alkaline fuel cells, since the difference in ORR electroactivity induced by the C-support is lower, a good choice could be using a support that assure a good activity, but at the same time does not cost too much. In this case for example the MWCNT. This fact put in evidence once more the great potentialities in the use of alkaline fuel cells, especially in terms of the reduction of the costs due to the catalytic materials.

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## CHAPTER 8. Conclusions.

### 8.1. General findings from the experimental work.

A series of interesting conclusions can be drawn from the results presented in each of the chapters of this thesis.

In Chapter 2, reduced graphene oxide was prepared in three different ways starting from graphite oxide. The influence of the synthesis method on the exfoliation and reduction degrees of rGO was evidenced. Starting from these three different rGO, three Fe-N/rGO catalysts for ORR were obtained. The final physicochemical properties of the catalysts and ORR activity in alkaline conditions depend on the initial properties of the rGO, underlying the important influence that the reduction-exfoliation process in rGO synthesis has on the final Fe-N/rGO catalyst.

In Chapter 3, a complex between Co(II) ions and the nitrogen-containing ligand molecule TPTZ and multi-walled carbon nanotubes were used as precursor for the preparation of an electrocatalyst for ORR. After a first pyrolysis, a good electroactivity in acid conditions was obtained. Then, a second pyrolysis was performed, and the catalyst performances increased in terms of both current density performance and stability. These improvements can be ascribed to the increase of the microporosity and better stabilization of the active sites induced by the second pyrolysis.

In Chapter 4, the synthesis of a Fe-N-C catalyst using pyrrole, iron acetate and mesoporous carbon as precursors was optimized. It was found that using a surfactant (polyvinylpyrrolidone) during the Fe ions impregnation and performing a preliminary heat treatment on the support before the Fe ions impregnation was not useful to obtain a higher activity. Performing a second pyrolysis lead to an activity and selectivity improvement, while the addition of further Fe amounts before this second pyrolysis does not lead to improve the ORR activity. These results provide an insight on how to synthesize a more active ORR catalyst.

The results of the physico-chemical characterization and RDE tests show that the total N and Fe contents are not the limiting factors for the ORR activity. However, the ORR activity improvement attained after the second pyrolysis is related to the higher relative amounts of pyridinic and pyrrolic nitrogen, and to the significant increase of the microporosity.

In Chapter 5, iron phthalocyanine was used as unique precursor for the synthesis of a Fe-N-C catalyst. The pyrolysis was performed at different temperature to find out an optimum. Then, two different mesoporous silica (SBA-15 and a commercial mesoporous silica) were used as hard templates to modify morphology of the final catalyst. The type of silica used as templating agent strongly influences the catalyst morphology, which in turn influences the catalyst ORR activity, depending on

the structural properties, in particular the total surface area and the micropores content. These results underline the importance of the choice of a templating agent with an adequate structure in order to produce a catalyst with good performances via the hard-templating method.

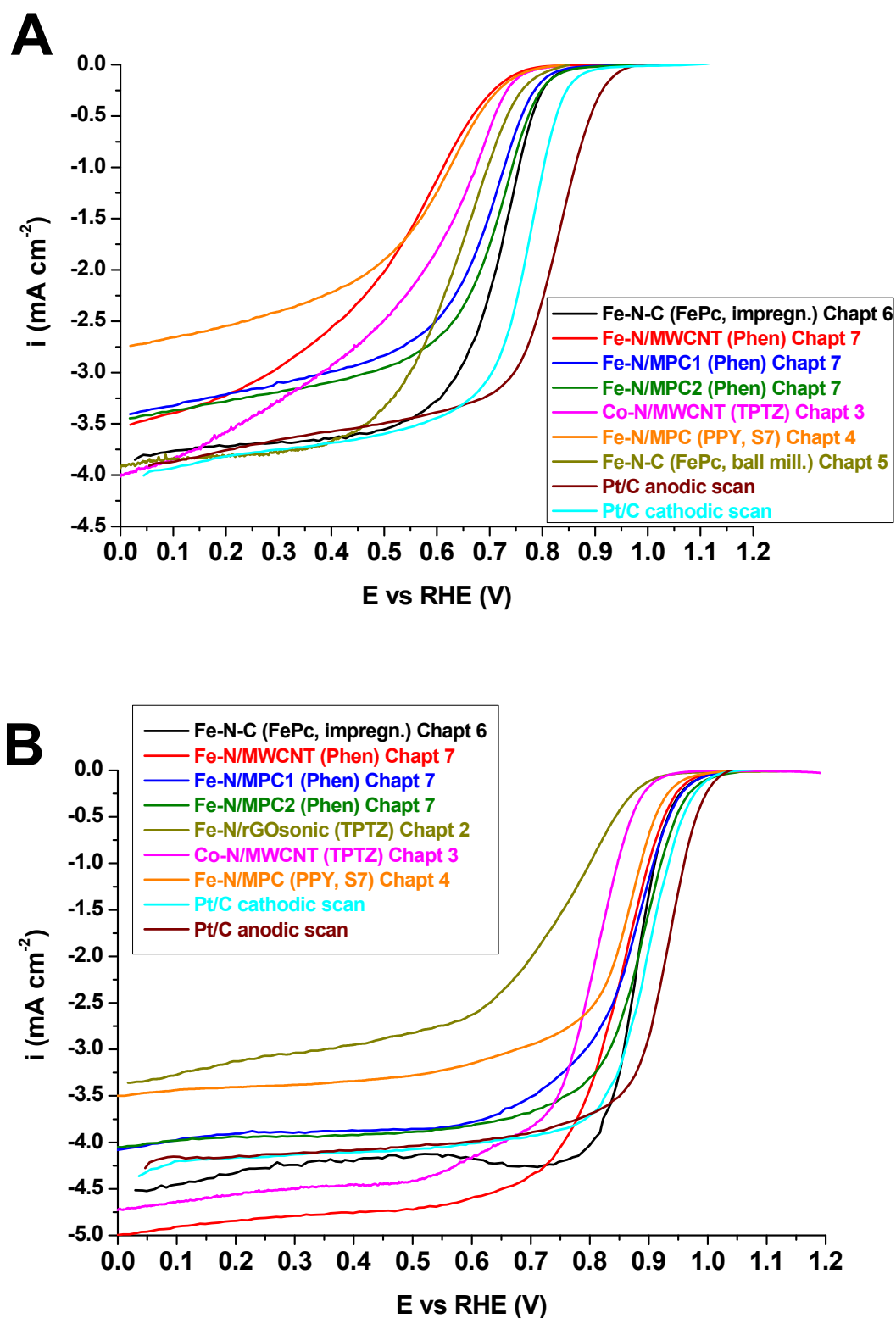
In Chapter 6, different Me(II)phthalocyanines (Me = Fe, Co, Cu, Zn) were used as unique transition metal, C and N precursor, to investigate the influence of the different metals in the final catalyst properties. A TGA coupled with a mass spectroscopy analysis evidenced how these properties are in relation with different trends of the weight loss and with the formation of gaseous products in different amounts and at different temperatures, which are induced by the different transition metals during the pyrolysis. These results show a new insight on what occurs during the pyrolysis process during the synthesis of these types of Me-N-C derived ORR. Fe-phthalocyanine is the precursor which lead to obtain the catalyst with higher activity and selectivity toward a complete  $4e^-$  ORR in both acid and alkaline conditions. In acid conditions, it exhibits interesting analogies with the standard Pt-based catalysts in terms of activation energy values, and their variation with overpotential. In alkaline conditions, this catalyst shows a performance very close to the Pt/C catalyst in terms of onset potential, and an almost null peroxide production.

The results of the different single fuel cell tests evidenced how this catalyst, in spite of its good ORR activity in RDE, is highly affected by deactivation mainly ascribed to the flooding of the micropores. This fact provides an important evidence of the importance of performing a fuel cell test for the ORR catalysts. Good catalytic performances in RDE-RRDE tests are not sufficient to define an ORR catalyst as a good candidate to be used in a fuel cell stack. The “goodness” of the catalyst has to be validated by means of the obtainment of good performances in fuel cell test in terms of both activity and durability.

In Chapter 7, different C-supports were used to obtain Fe-N/C catalysts using Fe – 1,10-phenanthroline complex as precursor. The results evidence the importance of the C-support characteristics in order to obtain a good catalyst performance. This is especially important in acid conditions, where the slower kinetics of ORR renders the distribution and accessibility of the active sites to be very limiting factors. In alkaline conditions the enhanced ORR kinetics due to the intrinsic properties of the Fe-N-C materials, makes the C-support structure itself a less strict parameter.

## **8.2. Resume of catalysts activities measured in RDE in both acid and alkaline conditions.**

To give an overall idea of the results obtained, the RDE performances of the most active catalyst developed in each of the chapters of this thesis are shown in Figure 1. It is evident that activity improvements were obtained throughout the experimental work performed during the development of the thesis.

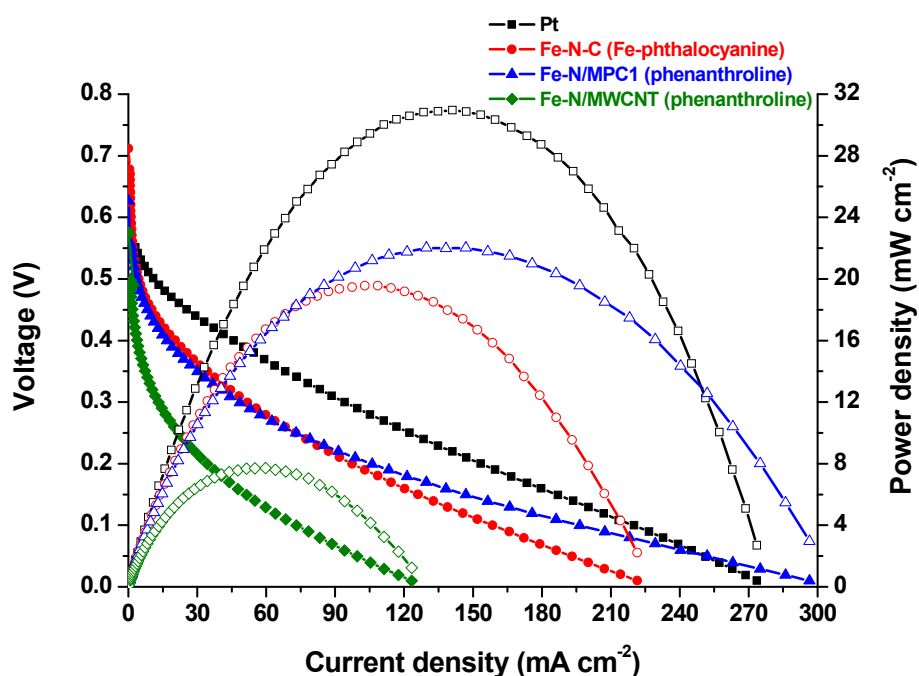


**Figure 1.** Polarization curves recorded in RDE at 900 rpm in acid (A) and alkaline (B) conditions for the most significant catalysts developed in this thesis. For each catalyst are indicated a reference to the composition, the nitrogen precursor molecule and the chapter of the thesis where it is presented.



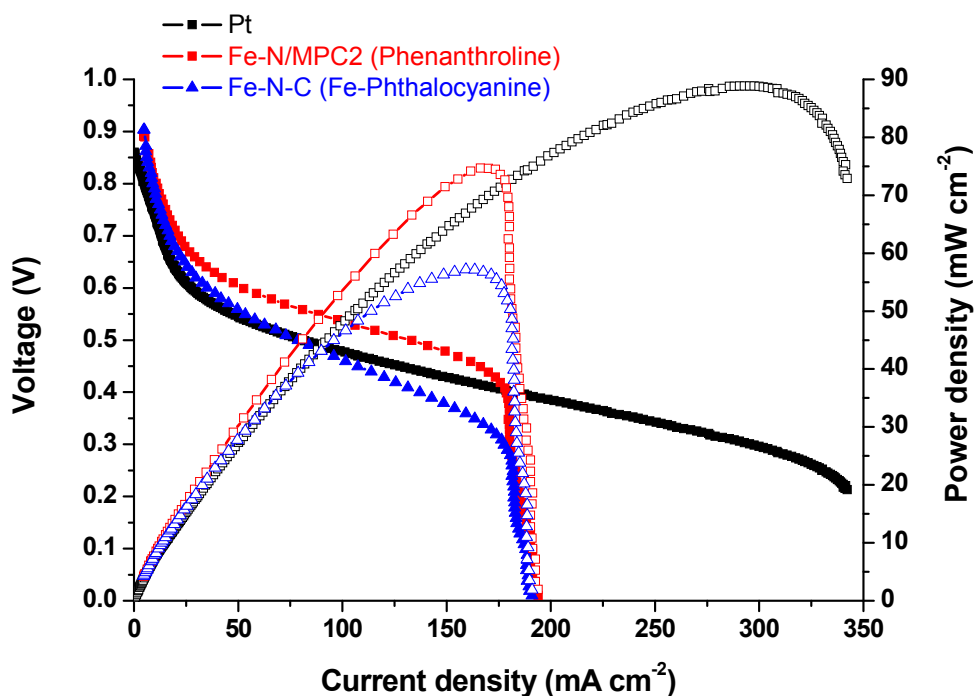
### 8.3. Overall performances obtained in single fuel cell and economic considerations.

The results of the acid membrane direct methanol fuel cell tests evidenced how much the choice of the cathodic catalyst influences the performance of the fuel cell. The best result obtained by one of our catalyst in terms of maximum power density is about 70 % of the commercial Pt/C catalyst. In terms of durability, our non-precious metal-based catalysts have shown considerably better performances than the Pt. This make them good candidates for Pt replacement at the cathode of DMFC. However, improvements in terms of electrocativity in acid conditions and durability have to be achieved. In particular, durability and stability issues in this type of catalysts seem to be caused by the flooding of the micropores, where most of the active sites are located. Therefore, the structural characteristics of the catalysts have to be investigated more in detail and improved.



**Figure 2.** Comparison of the most significant results obtained in the single DMFC tests.

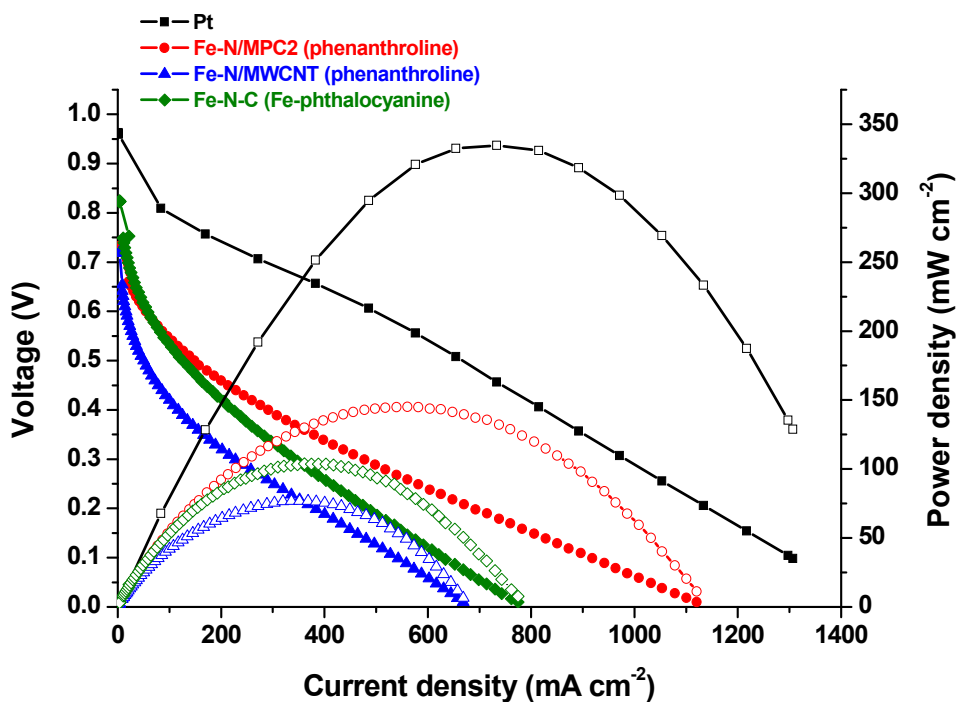
The performance obtained in direct ethanol alkaline fuel cell tests are very encouraging in terms of maximum power density, being the value for the better performing non-precious metal catalyst about 84 % than maximum power density obtained with the commercial Pt/C catalyst. However, some improvements can still be obtained in the mass transport limited region at high current densities, by optimization of the catalyst ink formulation and the catalyst structure and morphology.



**Figure 3.** Comparison of the most significant results obtained in the single alkaline DEFC tests.

Therefore, we demonstrated how the non-precious metal catalysts for ORR developed in this thesis are potential candidates for application as cathodic catalysts for direct alcohol fuel cells, in both acid and alkaline conditions. Nevertheless, so far, the commercialization of these technologies is still not widely developed. Comprehensive studies about the impact of the replacement of the standard Pt-based catalysts with this type of non-noble metal catalysts on the final cost of direct alcohol fuel cell devices are not available in the literature. However, one can state that the replacement of Pt with such a this type of catalysts will provide undoubted advantages in terms of decreasing the dependence on Pt (noble metal with high cost, price volatility and scarcity of reserves), without affecting too much the performances (especially in alkaline conditions), and also in terms of durability, especially in DMFC, due to the better resistance to methanol crossover.

Concerning the application in a PEMFC fueled with  $H_2$ , the performance of the best electrocatalyst developed and tested in this thesis, reaches a value close to 43 % of the maximum power density obtained with a commercial Pt/C catalyst at cathode in the comparative test. The use of this technology is more widely-developed, especially in the automotive sector, and some cost analyses can be found in the literature. In particular, different research centers and companies, and between them the U.S. Department of Energy have published some studies [1,2,3].



**Figure 4.** Comparison of the most significant results obtained in the single H<sub>2</sub> / O<sub>2</sub> PEMFC tests.

For example, the Los Alamos National Laboratory calculated the cost of the catalyst per kW of power generated by a 80 kW fuel cell stack based on a non-precious metal cathodic catalyst able to generate a maximum power density of 370 mW cm<sup>-2</sup>. The value varies with the number of stacks (and therefore of fuel cell powered vehicles) produced per year. For a minimum value of 1000 stacks per year, the cost of the catalyst was esteemed to be 0.62 U.S.\$ kW<sup>-1</sup>. Under the hypothesis of the maximum number of stacks production considered (500,000 stacks per year), the cost decreases to 0.35 U.S.\$ kW<sup>-1</sup> [1]. Under these hypotheses, considering a non-noble metal catalyst loading of 4 mg cm<sup>-2</sup> and the cost of the other components of the stack, they calculated a total cost of the non-precious metal based stack of 30 U.S.\$ kW<sup>-1</sup>.

The same calculation made for a Pt-based stack by the U.S. Department of Energy [2] lead to a cost of 55 U.S.\$ kW<sup>-1</sup>, considering a total Pt loading in the MEA of 0.153 mg cm<sup>-2</sup>, a maximum power density of 692 mW cm<sup>-2</sup> and an average Pt price of 1500 U.S.\$ per troy ounce.

However, we cannot provide such a this type of calculation on the basis of the cost of production of our more performing catalyst. In fact we could only base our calculation on the prices of the reagents that we can purchase at laboratory scale (order of magnitude of few grams), and this could lead to meaningless results. Moreover, the scale-up of the synthesis process from lab-scale to industrial scale is not trivial.

On the basis of the Los Alamos National Laboratory calculations [1], more than one stack has to be mounted on the vehicle to assure an adequate power if the maximum power density achieved is lower than  $600 \text{ mW cm}^{-2}$ . The presence of more than one stack causes a remarkable cost rising, in addition to problems of space on board and of total weight of the vehicle.

Therefore, the remaining major challenges and barriers to be overcome in order to make the non-precious metal-based ORR electrocatalysts for PEMFC powered vehicles a viable technology are:

- ORR activity of non-PGM catalysts (required to lower cost of stack components).
- Long-term stability and performance durability of non-PGM catalysts.
- Understanding of the active-site and reaction mechanism to help the catalyst design.
- Electrode integration optimization to allow sufficient ionic and electronic conductivity in thick catalytic layers and efficient mass transport of reactants / products to / from the active reaction sites.
- Scale-up of non-PGM catalyst synthesis.
- Water management at high current densities.
- Optimization of ionomer distribution in the electrode layer.
- MEA design, optimization, fabrication, and scale-up.
- Integration with existing automotive fuel cell stack and system technology.

#### **8.4. Suggestions for future work.**

From the results presented in this thesis, new possibilities and ideas for a future work can be suggested.

- The kinetic studies performed in RDE for the Me-N-C catalysts in acid conditions and presented in Chapter 6 could be conducted also in alkaline conditions: electrode ink and loading optimization in RDE, calculation of the reaction orders for oxygen and  $\text{OH}^-$ , calculation of the activation energy, hydrogen peroxide reduction test.
- The importance of the use of a templating agent able to give to the C-support or directly to the catalyst certain structural features was evidenced, especially in acid conditions. However, the cost of structured templating agents, such as a mesoporous silica, is still high at the present state of the art, and this could result in a too much high cost of the final non-precious metal catalyst. Therefore, the use of other methods for increasing the porosity and the surface area, especially for the self-supported catalysts (which do not make use of a C-support during the synthesis) could be considered for a future work. For example, the addition of foaming and expansion agents before the pyrolysis.
- Completion of the single fuel cell tests the catalyst presented in Chapter 7.

- Further tests in single fuel cell to find out the optimum catalyst ink formulation in order to obtain better performances.
- Further investigation via the TGA coupled with mass spectroscopy on catalysts prepared starting from different precursors, in order to compare the role played by the different transition metals during the pyrolysis process, as done in Chapter 6.

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## List of Publications

**L. Osmieri**, A.H.A. Monteverde Videla, S. Specchia. *Activity of Co–N multi walled carbon nanotubes electrocatalysts for oxygen reduction reaction in acid conditions*. Journal of Power Sources 278 (2015) 299–307.

DOI: 10.1016/j.jpowsour.2014.12.080

A.H.A. Monteverde Videla , **L. Osmieri**, M. Armandi, S. Specchia. *Varying the morphology of Fe–N–C electrocatalysts by templating Iron Phthalocyanine precursor with different porous SiO<sub>2</sub> to promote the Oxygen Reduction Reaction*. Electrochimica Acta 177 (2015) 43–50.

DOI: 10.1016/j.electacta.2015.01.165

A.H.A. Monteverde Videla, **L. Osmieri**, R. Alipour Moghadam Esfahani, J. Zeng, C. Francia. S. Specchia. *The Use of C–MnO<sub>2</sub> as Hybrid Precursor Support for a Pt/C–Mn<sub>x</sub>O<sub>1+x</sub> Catalyst with Enhanced Activity for the Methanol Oxidation Reaction (MOR)*. Catalysts 5 (2015) 1399–1416.

DOI: 10.3390/catal5031399

**L. Osmieri**, A.H.A. Monteverde Videla, S. Specchia. *Optimization of a Fe–N–C electrocatalyst supported on mesoporous carbon functionalized with polypyrrole for oxygen reduction reaction under both alkaline and acidic conditions*. Submitted to: International Journal of Hydrogen Energy (manuscript number: HE\_2016\_137) – Under revision.

Alessandro H. A. Monteverde Videla, **Luigi Osmieri**, Stefania Specchia. *Non-noble metal (NNM) catalysts for Fuel Cells: tuning the activity by a rational step by step single variable evolution*. Book Chapter in: Fethi Bedioui, Jose H. Zagal (Editors). *Electrochemistry of N4 Macrocyclic Metal Complexes, Volume1: Energy*. Springer International Publishing AG, Cham. – In Press  
ISBN 978-3-319-31170-8.

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**Osmieri L.**, Monteverde Videla A.H.A., Armandi M., Specchia S. (2015). A micro-silica reactor ( $\mu\text{SiO}_2\text{-R}$ ) able to produce highly porous non-noble catalysts for oxygen reduction reaction under alkaline conditions. In: *EFCD2015 – Challenges Towards Zero Pt for Oxygen Reduction*, La Grande Motte (France), 13/09/2015 – 16/09/2015. → **attended (poster presentation)**.

**Osmieri L.**, Alipour Moghadam Esfahani R., Monteverde Videla A.H.A., Vasile N.S., Specchia S. (2015). Kinetic analysis of oxygen reduction reaction on different self-supported C-N-Me (Me = Fe, Co, Cu) catalysts in acidic medium. In: *ECS Conference on Electrochemical Energy Conversion & Storage with SOFC-XIV*, Glasgow (United Kingdom), 26/07/2015 - 31/07/2015. # C-0622.

Monteverde Videla A.H.A., **Osmieri L.**, Ercolino G., Stelmachowski P., Kotarba A., Specchia S. (2015). “Mesoporous Cobalt Oxide for Oxygen Evolution Reaction under alkaline conditions: a comparative study of three synthesis methods”. In: *International Conference on Electrochemical Energy Science and Technology EEST2015*, Vancouver (BC, Canada), 16/08/2015 – 22/08/2015.

**Osmieri L.**, Monteverde Videla A.H.A., Alipour Moghadam Esfahani R., Vankova S., Armandi M., Specchia S. (2015). Zinc(II)-phtalocyanine as precursor for preparation of extremely high surface area N-doped carbon for potential applications in electrochemical devices. In: *II Italian Meeting on Porphyrins and Phtalocyanines*, Roma (Italy), 06/07/2015 - 08/07/2015. → **attended (poster presentation)**

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**Osmieri L.**, Monteverde Videla A.H.A., Spinelli P., Specchia S. (2014). Activity of Co-N<sub>x</sub>-multi-walled carbon nanotubes electrocatalysts for oxygen reduction reaction in acid conditions: a comparison between tests in rotating disk electrode and in gas-diffusion electrode half-cell. In: *14<sup>th</sup> Ulm ElectroChemical Talks 14-UECT*, Ulm (Germany), 24/06/2014 - 26/06/2014. → **attended (poster presentation).**

Monteverde Videla A.H.A., **Osmieri L.**, Specchia S. (2014). The use of different types of reduced graphene oxide (rGO) on the reduction oxygen reaction (ORR) under alkaline conditions. In: *6<sup>th</sup> Forum on New Materials - CIMTEC2014*, Montecatini Terme (Italy), 15/06/2014 - 19/06/2014. → **attended (oral presentation).**